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9th Avenue East Class Environmental Assessment

City of Owen Sound

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File: Prepared by: Prepared for:

121387 Tatham Engineering Limited City of Owen Sound

115 Sandford Fleming Drive, Suite 200 808 2nd Avenue East
Date: Owen Sound, Ontario N4K 2H4

January **T** 705-444-2565 9, 2024 tathameng.com

Authored by:	Reviewed by:
M. J. FIGUEROA EN 100543417 JAN 9, 2024 ONNOE OF ONTRE	M. J. CHALLE SEE STONAL CONTRIBUTION OF ONTAINS ON CE OF ONTAINS OF OUT AND CONTRIBUTION OF CONTRIBUTION OF OUT AND CONTRIBUTION OF OUT AND CONTRIBUTION OF CONTRIBUTION OF OUT AND CONTRIBUTION OF OUT AND CONTRIBUTION OF CONTRIBUTION OF OUT AND CONTRIBUTION OF OUT AND CONTRIBUTION OF CONTRIBUTION OF OUT AND CONTRIBUTION OF OUT AND CONTRIBUTION OF CONTRIBUTION OF OUT AND CONTRIBUTION OF CONTRIBU
Mark Figueroa, B.Eng. & Mgmt., P.Eng. Engineer	Michael Cullip, B.Eng. & Mgmt., M.Eng., P.Eng. Vice President

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1	January 9, 2024	Final Report

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1 Introduction

1.1 PROJECT AREA

The City of Owen Sound has identified several infrastructure needs and deficiencies in an area of the City involving the 9^{th} Avenue East (Highway 6/10) corridor which is a MTO Connecting Link. The project area, as identified in Figure 1, can generally be described as 9^{th} Avenue East from Superior Street to 9^{th} Street East (approximately 1,250 metres) including the block to the east extending to the terminuses of 6^{th} Street East and 7^{th} Street East.

1.2 IDENTIFIED NEEDS

There are concerns with the water distribution system which has dead ends on Superior Street, 6th Street East and 7th Street East. Furthermore, the 9th Avenue East watermain services several commercial and institutional properties such as hotels/motels, a courthouse, places of worship and long term care facilities. Given the pressure zone boundaries in the City and the aforementioned dead ends, there is no ability to back feed 9th Avenue East in the event of a watermain break leading to prolonged water outages.

The watermain, storm sewer and sanitary sewer systems date back to the 1960s and are deteriorated. The surface infrastructure (asphalt, curbs, guiderail, etc.) are also aged and in need of replacement.

1.3 REPORT STRUCTURE

This report is structured to follow the process of a Schedule B Class Environmental Assessment (Class EA) and includes the following:

- the problem/opportunity the project aims to address;
- a confirmation of the appropriate Class EA schedule;
- a summary of background reports and studies undertaken to inventory the applicable project area environments;
- the alternative solutions;
- a summary of stakeholder consultation activities; and
- the recommended solution.



2 Problem/Opportunity

The City of Owen Sound has initiated a Municipal Class EA to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. In consideration of the aforementioned background and in context of the City's objective to provide safe and reliable infrastructure, road and sidewalk systems, the following Problem Statement has been defined to set the framework for the completion of the Class EA study.

That existing infrastructure, road and sidewalk needs and deficiencies within the subject length of 9th Avenue East (100 metres south of Superior Street to 100 metres north of 9th Street East) be addressed in an environmentally sound manner, in consideration of City standards and policies, infrastructure requirements and active transportation opportunities, with the objective of providing safe and reliable service to the people of Owen Sound.

The Problem Statement was formally issued in a Notice of Study Commencement dated June 23, 2022, a copy of which is provided in Appendix A. Further discussions with respect to the notice and associated stakeholder consultation is provided in Chapter 7.



3 Municipal Class EA Process

All infrastructure and road improvement projects in Ontario are subject to the Environmental Assessment Act. The Act allows the use of Class Environmental Assessments, such as the Municipal Class Environmental Assessment process¹ (amended 2023). Applying to all municipal infrastructure and road improvement projects, a number of study categories and schedules have been established recognizing the range of environmental impacts. These are briefly described below.

3.1.1 Class EA Schedule

Exempt Projects

These projects generally include normal or emergency operational and maintenance activities, rehabilitation works, minor reconstruction or replacement of existing facilities, and new facilities that are limited in scope. As the environmental effects of these activities are usually minimal, these projects are exempt from the Environmental Assessment Act and hence there are no requirements under the Class EA framework.

Schedule B Projects

Schedule B projects generally include improvements and minor expansions to existing facilities or smaller new projects. As there is the potential for some adverse environmental impacts, the proponent is required to conduct a screening process whereby members of the public and review agencies are informed of the project and given the opportunity to provide comment (warranting completion of Phases 1 and 2 of the Class EA process). Documentation of the planning and design process is required under a Schedule B study. As these studies are generally straightforward and do not require detailed technical investigations to arrive at the preferred solution, a comprehensive report is not required. Rather, a Project File shall be prepared to demonstrate that the appropriate steps have been followed. The Project File is to be submitted for review by the public and review agencies for comment and input. Once this is complete, the project can proceed to implementation (Phase 5).

Schedule C Projects

Schedule C projects generally include the construction of new facilities and major expansions to existing facilities. As they have the potential for significant environmental impacts, they must

¹ Municipal Class Environmental Assessment. Municipal Engineers Association, October 2000, as amended in 2007, 2011, and 2015.



proceed under the full planning and documentation procedures specified by the *Municipal Class EA* document (Phase 1 to 5). Schedule C projects require that an Environmental Study Report be prepared and appropriately filed for review by the public and review agencies.

3.1.2 Class EA Terminology

Prior to determining the appropriate Class EA schedule, an understanding of the defining terminology is required as noted below:

Localized Operational Improvements

Refers to structural changes to an existing roadway at specific locations, and may include turning lanes at an intersection, storage lanes, U-turn lanes, bus bays, median changes, changing the curb radii, etc.

Road Capacity

Means capacity defined in terms of the number of travelled lanes and does not differentiate between various lane widths to accommodate differing traffic volumes.

Same Purpose, Use, Capacity & Location

Refers to the replacement or upgrading of a structure or facility or its performance, where the objective and application remain unchanged, and the volume, size and capability do not exceed the minimum municipal standard, or the existing rated capacity, and there is no substantial change in location. Works carried out within an existing road allowance such that no land acquisition is required are considered to be in the same location. Conversely, it is thus inferred that should improvements extend beyond the existing road allowance and additional property is required, the location is considered to have changed.

3.1.3 Selected Class EA Schedule

The Municipal Class EA document details a number of infrastructure and road improvement projects and defines the corresponding Class EA schedule to be applied based on the result of a screening process.

Exempt Projects

- Road resurfacing with no change to the horizontal alignment.
- Reconstruction where the reconstructed road will be for the same purpose, use, capacity and at the same location.



- Establish, extend or enlarge a water distribution system and all works necessary to connect the system to an existing system or water source, provided all such facilities are either in an existing road allowance or an existing utility corridor including the use of Trenchless Technology for water crossings.
- Establish, extend, or enlarge a sewage collection system and all necessary works to connect the system to an existing sewage or natural drainage outlet, provided all such facilities are in either an existing road allowance or an existing utility corridor, including the use of Trenchless Technology for water crossings.

Schedule B

- Reconstruction or widening where the reconstructed road will not be for the same purpose, use, capacity or at the same location (e.g. additional motor vehicle lanes, continuous centre turn lane that requires property, i.e. not at the same location), provided the construction value is less than \$3 M (otherwise a Schedule C undertaking would apply).
- Establish, extend or enlarge a water distribution system and all works necessary to connect the system to an existing system or water source, where such facilities are not in either an existing road allowance or an existing utility corridor.
- Establish, extend or enlarge a sewage collection system and all works necessary to connect the system to an existing sewage outlet where such facilities are not located in an existing road allowance, or existing utility corridor.

Applicable Schedule

In consideration of the above, a Schedule B undertaking has been selected. The requirements of such would be to complete Phase 1 and Phase 2 of the overall Class EA process (refer to Appendix B for the Municipal Class EA Planning and Design Process), which involves identifying the problem, developing alternative solutions and selecting a preferred solution prior to proceeding to Phase 5: Implementation (i.e. design and construction).



4 Alternative Solutions

In consideration of the noted system deficiencies, City standards and guidelines, and the project area, alternative improvement solutions were considered, as detailed below.

4.1 ROADS

The City's scope of work for road infrastructure includes resurfacing the existing asphalt pavement, replacing deteriorated concrete curbs and replacing deficient steel beam guiderail on 9th Avenue East. Localized sidewalk replacements and extensions may also be included in the reconstruction program. Given that the intent is simply to replace that which is aged and requires replacement, the road will remain in its current location and maintain its current configuration. As such, there is no need for alternative solutions for the road improvements.

4.2 STORM SEWER

A closed-circuit television (CCTV) investigation of all storm sewers and structures on 9th Avenue East within the project area was completed, and several deficiencies were identified including sagging, cracked and collapsed pipes. Given these deficiencies, coupled with the overall age of the system, full replacement of the storm sewer system within the project area is recommended, maintaining its existing location. In this regard, there are no alternative solutions pertaining to the storm sewer system.

4.3 SANITARY SEWER

The City has determined that the sanitary sewers in the project area are generally in good condition and are not in need of replacement. During the reconstruction of 9th Avenue East, all existing sanitary services will be replaced as a proactive maintenance activity. In this regard, there are no alternative solutions pertaining to the sanitary sewer system.

4.4 WATERMAIN

4.4.1 9th Avenue East

There are two watermains on 9th Avenue East within the project area:

- a 400 millimetre diameter trunk watermain from 8th Street East to the north project limit; and
- a 150 millimetre diameter distribution watermain along the entire length, providing individual water services to all properties fronting the road and providing service to fire hydrants.



Through the City's water model, the size of the trunk watermain is confirmed as appropriate. City operations staff have also confirmed the trunk watermain is in satisfactory condition and thus replacement is not required, albeit there are several valves which will be replaced.

With respect to the distribution watermain, as noted previously, there are significant risks in the distribution system when breaks result in outages to several critical properties. The existing distribution watermain ranges in size from 150 to 200 millimetres in diameter and has sections of cast iron and ductile iron. Based on numerous modelling scenarios undertaken for this study, it is recommended that the existing distribution watermain will be replaced with a 200 millimetre diameter watermain; the modelling report and summary is included in Appendix C Replacement of the distribution watermain is an exempt activity under the MEA Class EA framework and thus alternative solutions are not required.

4.4.2 Looping Watermain

To mitigate the risks previously alluded to, a second distribution watermain in the area is required to provide redundancy and looping to increase system reliability during both normal operations and watermain repairs. When determining alternative solutions for the looping watermain alignment, the following sections were considered:

- 6th Street East to 8th Street East; and
- Superior Street to 6th Street East.

6th Street East to 8th Street East

From 6th Street East to 8th Street East, there is a City-owned utility corridor parallel to 9th Avenue East which intersects the dead ends of 6th Street East and 7th Street East. The City and Tatham concluded the most appropriate alignment for the looping watermain would be in this utility corridor, and as it is City owned, the undertaking is classified as an exempt activity. Construction of this first phase of the looping watermain was completed in 2023. The location of the looping watermain from 6th Street East to 8th Street East is illustrated in Figure 2.

Superior Street to 6th Street East

The second segment of the looping watermain has only one City owned road allowance or utility corridor, 9th Avenue East. Installing a twin watermain on 9th Avenue East from Superior Street to 6th Street East was not considered in detail for the following reasons:

- does not provide benefit to properties on Superior Street;
- if twin watermains are too close together, one cannot be safely worked on without shutting down/depressurizing the other; and



• existing utilities, sewers and watermain limit the available space to fit a second watermain.

In consideration of the discussion above, the looping watermain from Superior Street to 6th Street East was assumed to be "established, extended or enlarged" outside of a road allowance or utility corridor (as identified in Figure 3), and as such, a Schedule B Class EA was initiated to review and select an appropriate alignment. Five alternative solutions were explored, in addition to a "do nothing" scenario, as detailed in Table 1 and illustrated in Figure 4 through Figure 8.

Table 1: Looping Watermain Alternatives

ALTERNATIVE	DESCRIPTION
Do Nothing	 existing watermain system remains in its current arrangement with no looping south of 6th Street East
Alternative 1	 watermain installed in easements to be created on the 595 9th Avenue East (Grey County) and 425 9th Avenue East (E.C. King) properties connects to existing watermains on Superior Street and 6th Street East outside of existing sanitary sewer easements (shown in green) on 595 9th Avenue East and 1010 Superior Street properties considerable tree removals required on 425 9th Avenue East (E.C. King) property
Alternative 2	 generally parallel to existing sanitary sewer easements (shown in green) on 595 9th Avenue East (Grey County) and 1010 Superior Street properties existing sanitary sewer easements are not wide enough to accommodate the watermain; existing easements would need to be widened connects to existing watermains on Superior Street and 6th Street East
Alternative 3	 parallel to existing sanitary sewer easements (shown in green) on 595 9th Avenue East (Grey County) and 1010 Superior Street properties existing sanitary sewer easements are not wide enough to accommodate the watermain; existing easements would need to be widened connects to existing watermains on Superior Street and 6th Street East existing building on Grey County property would need to be relocated
Alternative 4	 watermain installed in easements to be created on the 595 9th Avenue East (Grey County), 1010 Superior Street, 1000 Superior Street and 1150 Superior Street properties connects to existing watermains on Superior Street and 6th Street East
Alternative 5	 watermain installed in easements to be created on the1305 8th Street East, 1650 Superior Street (Hydro One) and 1150 Superior Street properties connects to existing watermains on Superior Street and 6th Street East



5 Background Reports & Studies

To inform the evaluation of alternative solutions, several background reports and studies were completed to consider various environments within the project area, the findings of which are summarized below.

5.1 SCOPED ENVIRONMENTAL IMPACT STUDY

Azimuth Environmental was retained to conduct a Scoped Environmental Impact Study (EIS) within the area (provided in Appendix D). The purpose of the EIS is to identify Natural Heritage Features and Functions (NHFFs) and evaluate potential impacts of the proposed alternatives. The Scoped EIS considers any negative environmental impacts from each of the proposed alternatives, and recommendations are provided to assist in determining the optimal alternative.

5.1.1 Study Approach

To develop the Scoped EIS report, Azimuth completed the following:

- collected and reviewed background information through Grey County, Ministry of Natural Resources and Forestry, and Ministry of the Environment, Conservation and Parks records;
- conducted the following field surveys:
 - 2 vascular plant inventories (spring and summer 2022); and
 - 2 dawn breeding bird surveys;
- completed a Species at Risk (SAR) habitat assessment through background information and fieldwork to identify the presence of SAR/SAR habitat in the study area;
- recorded wildlife observations and assessed potential for Significant Wildlife Habitat (SWH)
 function according to provincial criteria;
- evaluated the alignment alternatives with regard for the identified NHFFs; and
- assessed the potential direct and indirect impacts of the project on NHFFs in the study area.

5.1.2 Habitat for Threatened or Endangered Species

The following Threatened or Endangered species were determined to have the potential to occur in or adjacent to the study area:

- Eastern Meadowlark:
- Little Brown Myotis (potential);



- Northern Myotis (potential); and
- Tri-colored Bat (potential).

Eastern Meadowlark

Eastern Meadowlark activity was detected in the area of Alternative 5, as well as the lands adjacent to this area. It was determined that this alternative would likely disrupt the habitat of the Eastern Meadowlark. However, the works proposed in Alternatives 1 through 4 would not impact the habitat, and it was deemed the Eastern Meadowlark would likely continue to be present post-construction.

Little Brown Myotis, Northern Myotis and Tri-colored Bat

Through field investigations, approximately 20 candidate bat snag trees were found in the woodland corridor between 405 9th Avenue East and 1010 Superior Street. Alternatives 1 through 3 would encroach into potential SAR bat habitat (Alternative 1 would have the greatest impact), and the proposed works would represent removal of a small number of snag trees with potential to provide habitat for SAR bats (if present).

Based on the MECP Bat Survey Standards Note, and provided only a small number of potential bat habitat snags would be removed outside of the active bat season (April 1 to September 30 in Southern Ontario), additional bat surveys or MECP consultation would not be required. It was found that the potential for indirect impacts to SAR bat habitat would be considered mitigable, provided that the mitigation measures outlined in the Scoped EIS report Section 8 are followed.

5.1.3 Other Wetlands

It was identified that Alternatives 4 and 5 would both directly and indirectly impact three small, isolated wetlands, located in the field east of 1025 6th Street East. Alternatives 1 through 3 would not encroach into wetland, and therefore would not represent a direct impact to wetlands.

5.1.4 **Candidate Significant Woodlands**

One Candidate Significant Woodland feature was identified in the study area, located west and south of 1000 6th Street East. It was determined Alternative 5 would not encroach upon this feature, while Alternatives 1 through 4 would. In Azimuth's opinion however, Alternatives 3 and 4 would not compromise the overall form or ecological function of the feature since construction would be along the eastern-most edge of the Woodland. Alternatives 1 and 2 may have adverse effects as they would fragment part of the Candidate Significant Woodland and possibly increase forest "edge effects", which results in potentially increased risk of predation on bird nests and exposure to nest parasitism.



5.1.5 Candidate Significant Wildlife Habitat

Azimuth identified certain potential Significant Wildlife Habitat features, and noted anticipated impacts due to construction in their report:

Bat Maternity Colonies

Potential bat maternity roosting habitat was identified in the study area of Alternatives 1 through 4, however it was determined that the scale of tree removals would be relatively small, especially with Alternatives 3 and 4. It is expected that the potential habitat for roosting bats will not be impacted post construction.

Special Concern and Rare Wildlife Species

During the study period, Azimuth detected Eastern Wood-pewee (Special Concern species) on adjacent lands, but not within the study area. The conclusion was that this species and its habitat would not be impacted by the proposed works.

Azimuth also identified potential habitat for the Monarch Butterfly but did not observe any Monarch and deemed the habitat quality as low. More suitable habitat locations were located outside of the study area; thus, it was determined that the impact on Monarch habitat within the study area would be negligible.

5.1.6 Recommendations

Based on findings from field surveys and background information, it was determined that Alternative 3 would be the least impactful. This alternative would avoid wetlands areas and have minimal encroachment on Candidate Significant Woodlands, while avoiding the habitat of Eastern Meadowlark and minimizing impacts on habitat of other significant wildlife. Given the similar alignment of Alternative 2 to Alternative 3, Alternative 2 similarly has a low impact.

5.2 GEOTECHNICAL INVESTIGATION

GEI Consultants completed a comprehensive geotechnical investigation of the entire project area (report is provided in Appendix E). Boreholes 17, 19, 20 and 21 are within the Schedule B Class EA study area which generally revealed the following subsurface conditions (drilling completed February 13, 2023):

- native fill comprised of clay;
- a layer of glacial till with cobbles and boulders below the fill layer;
- auger refusal at 2.3 to 3.5 metre depth; and
- groundwater at drilling from 1.2 metres below ground surface to dry.



The watermain will generally be installed with a 2.0 metre depth to invert. Therefore, there may be a need for dewatering due to the groundwater levels, and localized rock excavation.

5.3 **HYDROGEOLOGICAL ASSESSMENT**

Following the geotechnical investigation, which revealed groundwater levels above the watermain invert, a hydrogeological assessment was completed (refer to Appendix F). This assessment will support future construction dewatering permit applications with the MECP.

5.4 WATER MODELLING

As noted previously, several scenarios were analyzed in the City's water model to determine the appropriate size of the distribution watermain on 9th Avenue East and the looping watermain (results of the modelling are provided in Appendix C). The modelling determined a 200 millimetre watermain was appropriate for both watermains.



Evaluation of Alternative Solutions 6

This section will discuss the evaluation of the alternative solutions as previously described. The evaluation of results at this stage is considered preliminary given the need to solicit agency and public input. The evaluation is descriptive or qualitative in nature allowing for a comparative evaluation of the positives and negatives associated with each alternative solution.

EVALUATION CRITERIA 6.1

In completing the evaluation, a number of criteria were considered as outlined below.

Technical (Water Operations)

- water system needs
- alignment and configuration

Natural Environment

- vegetation impacts
- wildlife/terrestrial impacts
- fisheries/aquatic impacts

Social Environment

future impacts on adjacent property

Cultural/Heritage Environment

- archaeological impacts
- built heritage impacts

Economic Environment

construction and operating costs

6.2 **ENVIRONMENTAL IMPACTS**

The potential impacts associated with each alternative are noted in the following sections.

6.2.1 Do Nothing

Criteria	Comments	Score
Technical (Water Operations)	Operational needs not addressed	0
Social Environment	 No easements required Watermain break results in detrimental impacts to commercial and institutional properties 	1
Natural Environment	No adverse impacts	5
Cultural / Heritage Environment	 No adverse impacts 	5
Economic Environment	 No capital cost Maintenance costs remain (flushing, fixing breaks) 	2
	TOTAL:	13



6.2.2 Alternative 1

Criteria	Comments	Score
Technical (Water Operations)	Operational needs addressedRelatively straight alignment	5
Social Environment	 New easements required on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 	3
Natural Environment	 Fragments woodland in south half Encroaches on potential SAR bat habitat 	1
Cultural / Heritage Environment	No adverse impactsPreviously disturbed area in north half	5
Economic Environment	Lowest capital cost (shortest length)Reduces maintenance costs (flushing, fixing breaks)	5
	TOTAL:	19

6.2.3 Alternative 2

Criteria	Comments	Score
Technical (Water Operations)	Operational needs addressedRelatively straight alignment	5
Social Environment	 New easement required on 1 property Widen existing easement on 1 property Significantly reduces impacts of watermain breaks (less customers affected) 	4
Natural Environment	Minimal impacts (limited tree removals)	4
Cultural / Heritage Environment	No adverse impactsAll areas previously disturbed	5
Economic Environment	Lowest capital cost (shortest length)Reduces maintenance costs (flushing, fixing breaks)	5
	TOTAL:	23



6.2.4 Alternative 3

Criteria	Comments	Score
Technical (Water Operations)	Operational needs addressedStraight alignment	5
Social Environment	 Widen existing easements on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 	4
Natural Environment	Minimal impacts (limited tree removals)	4
Cultural / Heritage Environment	No adverse impactsAll areas previously disturbed	5
Economic Environment	 Lowest watermain capital cost (shortest length) but must relocate building on Grey County property Reduces maintenance costs (flushing, fixing breaks) 	1
	TOTAL:	19

6.2.5 Alternative 4

Criteria	Comments	Score
Technical (Water Operations)	Operational needs addressedSeveral bends in alignment, longer length	4
Social Environment	 Widen existing easements on 2 properties New easements required on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 	3
Natural Environment	Limited tree removalsWill encroach into wetlands	2
Cultural / Heritage Environment	No adverse impactsAll areas previously disturbed	5
Economic Environment	 Largest watermain capital cost (longest length) Reduces maintenance costs (flushing, fixing breaks) 	1
	TOTAL:	15



6.2.6 Alternative 5

Criteria	Comments	Score
Technical (Water Operations)	Operational needs addressedSeveral bends in alignment, longer length	4
Social Environment	 New easements required on 3 properties Hydro One won't allow infrastructure or easements through high voltage area Significantly reduces impacts of watermain breaks 	0
Natural Environment	Limited tree removalsWill encroach into wetlands	2
Cultural / Heritage Environment	No adverse impactsAll areas previously disturbed	5
Economic Environment	 Largest watermain capital cost (longest length) Reduces maintenance costs (flushing, fixing breaks) 	1
	TOTAL:	12

6.3 **RECOMMENDED SOLUTION**

A comparative summary of the evaluation scores is provided in Table 2. In consideration of the advantages and disadvantages of each alternative and their respective scoring, and the overall project objectives, Alternative 2 is recommended.

Table 2: Looping Watermain Alternatives - Evaluation Summary

CRITERIA	ALTERNATIVE					
	Do Nothing	1	2	3	4	5
Technical (Operations)	0	5	5	5	4	4
Social Environment	1	3	4	4	3	0
Natural Environment	5	1	4	4	2	2
Cultural/Heritage Environment	5	5	5	5	5	5
Economic Environment	2	5	5	1	1	1
TOTAL	13	19	23	19	15	12



It noted that the recommended solution is not presented as a decision but as a preliminary preference based on evaluation of information available through the background reports and studies.

6.4 PREFERRED SOLUTION

The recommended solution was presented to the public and stakeholders at a public information centre and subsequently presented to the City of Owen Sound Operations Committee (as discussed further in Section 7.4). Following consideration of the comments and input received, Alternative 2 was identified as the preferred solution.

6.5 **CONFIRMATION OF CLASS EA SCHEDULE**

In context of the preferred solution, the Schedule B Class EA framework is confirmed as appropriate. As noted previously, the Schedule B undertaking applies to the enlargement of a water distribution system and all works necessary to connect the system to an existing system or water source, where such facilities are not in either an existing road allowance or an existing utility corridor.



Stakeholder Engagement & Consultation

To satisfy the requirements of the Schedule B Class EA and to provide further opportunity for stakeholder engagement and consultation, several activities were completed which are detailed in the following sections.

7.1 NOTICE OF STUDY COMMENCEMENT

At the onset of the Class EA, the Notice of Study Commencement was posted on the project webpage on the City's website. The notice was issued on June 23, 2022 and is included in Appendix A for reference.

7.2 PROPERTY OWNER CONSULTATION

City of Owen Sound staff led efforts to consult with specific property owners in the study area. These included property owners where easements would be required to implement the watermain alignments being considered. Letters were sent by mail and email to 13 property owners which are included in Appendix G. The letters also included a copy of the Notice of Study Commencement.

7.3 **CITY OPERATIONS COMMITTEE PRESENTATION 1**

A project update was presented to the City of Owen Sound Operations Committee on April 20, 2023. While the presentation focused on the first phase of the project (i.e. the looping watermain from 6th Street East to 8th Street East), it also provided an update on the status of the Schedule B Class EA (at the time of the presentation, the Class EA was at the alternative solution identification stage). The presentation slides are provided in Appendix H for reference.

7.4 PUBLIC INFORMATION CENTRE & OPERATIONS COMMITTEE PRESENTATION 2

A Public Information Centre (PIC) was held on November 16, 2023 at Owen Sound City Hall. The purpose of the PIC was to provide information to the public and agencies and seek their input with respect to the following:

- identification of the problem/opportunity;
- development of alternative solutions to address the problem/opportunity;
- general inventory of the affected environments;
- potential impacts of the alternative solutions to the environments considered;



- evaluation of the alternative solutions and the identification of the recommended solution;
 and
- discussion of remaining tasks to be undertaken in completing the Class EA.

A Notice of PIC was sent to all stakeholders within the study area two weeks in advance. The notice was also posted on the project webpage on the City's website. A copy of the notice is included in Appendix A.

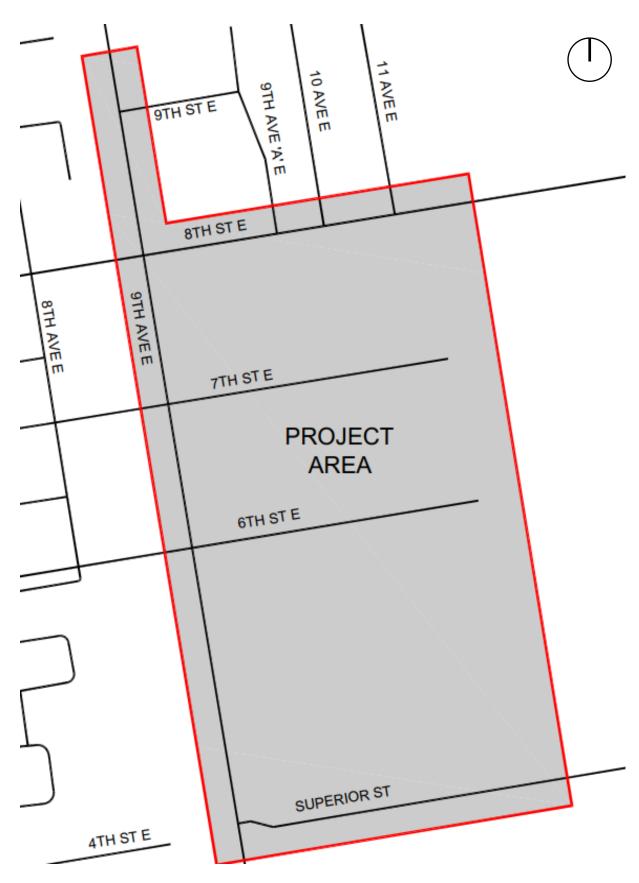
The PIC format was a one-hour open house with City and Tatham staff present. Comment sheets were available for feedback from stakeholders; however, no comments were received.

Following the open house, Tatham gave a further presentation to the City's Operations Committee to summarize the Class EA process and present the alternative solutions and the recommended alternative solution as presented at the PIC. The presentation slide deck is included in Appendix I.

7.5 NOTICE OF STUDY COMPLETION

A Notice of Study Completion will be issued in conjunction with the completion of this report, to be emailed to all stakeholders on the project contact list (including Indigenous Communities) and the MECP Southwest Region office. The notice will also be posted on the project webpage on the City's website. A copy of the notice is included in Appendix A.

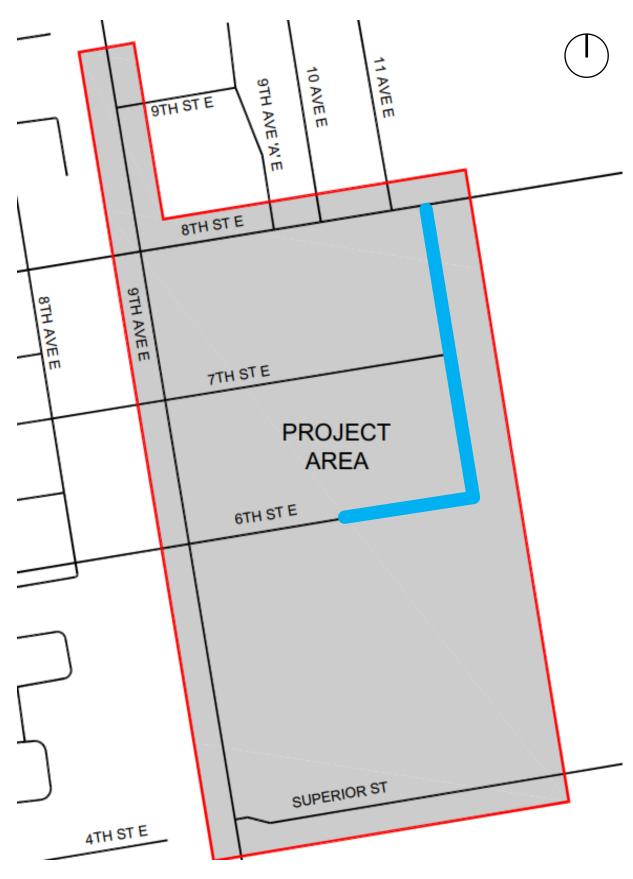




9th Avenue East Class Environmental Assessment







$9^{\,\mathrm{th}}$ avenue east class environmental assessment







9^{th} avenue east class environmental assessment





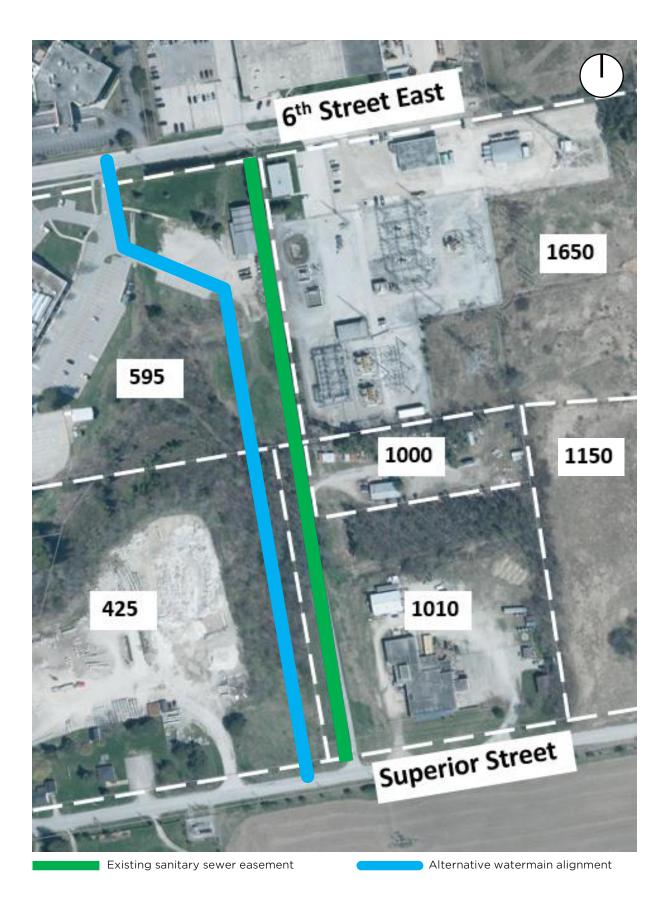


Figure 4: Looping Watermain from Superior Street to 6th Street East - Alternative 1





Figure 5: Looping Watermain from Superior Street to 6th Street East - Alternative 2



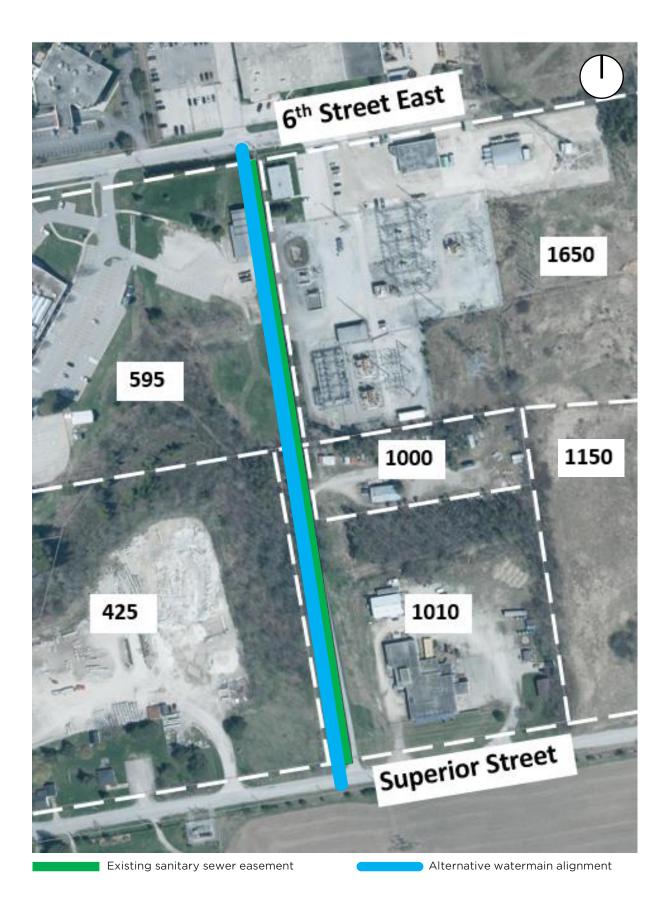


Figure 6: Looping Watermain from Superior Street to 6th Street East - Alternative 3





Figure 7: Looping Watermain from Superior Street to 6th Street East - Alternative 4





Figure 8: Looping Watermain from Superior Street to 6th Street East - Alternative 5



Appendix A: Study Notices

Engineering Services Division City of Owen Sound 808 2nd Avenue East Owen Sound ON N4K 2H4



Telephone: 519-376-1440 Facsimile: (519) 376-3579 Website: www.owensound.ca

9TH AVENUE EAST CLASS ENVIRONMENTAL ASSESSMENT

Notice of Study Commencement

The Study

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100m south of Superior Street to 100m north of 9th Street East;
- storm sewer system between Superior Street and 9th Street East;
- sanitary sewer system between 7th Street East and 8th Street East;
- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.

The Process

To appropriately consider any impacts associated with the proposed work, the City is undertaking a Schedule B Class EA which will address the following:

- the existing operations and conditions of the noted systems;
- alternative solutions to implementing the necessary repair, replacement and/or improvements;
- the location, extent and sensitivity of the existing environments within the area;
- the potential impacts of each alternative to the noted environments and possible mitigating measures;
- public and agency consultation and participation; and
- an assessment and evaluation of the alternative solutions culminating in a preferred solution.

Purpose of Notice

The purpose of this notice is to invite stakeholder input and comments early in the study such that they can be incorporated into the planning and overall study design. Comments should be directed to the City and/or Consultant as noted below. A further opportunity for stakeholder involvement will be provided at a Public Information Centre (PIC) to be held in the upcoming months, during which time additional details will be provided with respect to the system needs and deficiencies, the alternative solutions and assessment of such. Further details with respect to the PIC will be provided closer to the date.

Project Contacts

Owner

City of Owen Sound 808 2nd Avenue East Owen Sound, ON N4K 2H4 **Chris Webb, P.Eng.** Manager of Engineering Services cwebb@owensound.ca (519) 376-1440

This notice issued June 23, 2022

Consultant

Tatham Engineering Limited
115 Sandford Fleming Drive, Suite 200
Collingwood, ON L9Y 5A6
Allan Brownridge, P.Eng.
Project Manager
abrownridge@tathameng.com
(705) 444-2565 x2007

Engineering Services Division City of Owen Sound 808 2nd Avenue East Owen Sound ON N4K 2H4



Telephone: 519-376-1440 Facsimile: (519) 376-3579 Website: www.owensound.ca

9TH AVENUE EAST CLASS ENVIRONMENTAL ASSESSMENT

Problem / Opportunity Statement

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100 metres south of Superior Street to 100 metres north of 9th Street East;
- storm sewer system between Superior Street and 9th Street East;
- sanitary sewer system between 7th Street East and 8th Street East;
- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.

In consideration of the above and in context of the City's objective to provide safe and reliable infrastructure, road and sidewalk systems, the following Problem Statement has been defined to set the framework for the completion of the Class EA study.

That existing infrastructure, road and sidewalk needs and deficiencies within the subject length of 9th Avenue East (100 metres south of Superior Street to 100 metres north of 9th Street East) be addressed in an environmentally sound manner, in consideration of City standards and policies, infrastructure requirements and active transportation opportunities, with the objective of providing safe and reliable service to the people of Owen Sound.



Telephone: 519-376-1440 Facsimile: (519) 376-3579 Website: www.owensound.ca

9TH AVENUE EAST CLASS ENVIRONMENTAL ASSESSMENT – WATER DISTRIBUTION ALTERNATIVES FOR THE SUPERIOR STREET TO 6TH STREET EAST AREA

Notice of Public Information Centre

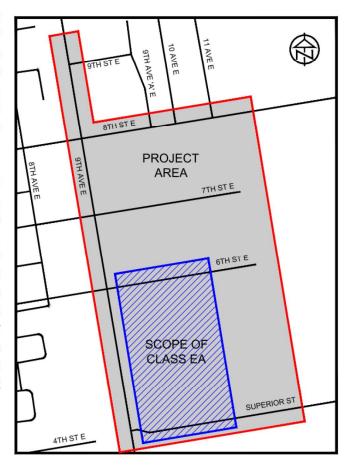
The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. Specifically, the City is considering options to improve the reliability of the water distribution system in this area where there are current water supply risks in the event of a watermain break.

Alternatives related to the existing watermain in 9th Avenue East from Superior Street to 6th Street East are being planned through the Schedule B process in the Municipal Class Environmental Assessment (2023). Consultation with the public, technical agencies and other stakeholders will inform the study recommendations.

A Public Information Centre (PIC) is being held to present alternative solutions being considered to improve the reliability of the water distribution system in the project area. The PIC will consist of an informal open house from 4:30 pm to 5:30 pm with materials pertaining to the study on display and members of the project team present to answer questions related to the project. A presentation will follow from the consultant at 5:30 pm at the City's Operations Committee meeting to provide an update on the status of the project and present the alternative solutions.

Date: November 16, 2023
Time: 4:30 pm – 6:30 pm
Location: Owen Sound City Hall,

Council Chambers (808 2nd Avenue East, Owen Sound, Ontario)



If you have any questions related to the PIC, please contact one of the following members of the Project Team. There will be an opportunity to provide comments at the PIC.

More information is also available on the City's project webpage: https://www.owensound.ca/en/city-hall/9th-avenue-east.aspx

Project Team

Owner

City of Owen Sound 808 2nd Avenue East Owen Sound, ON N4K 2H4 **Chris Webb, P.Eng.** Manager of Engineering Services cwebb@owensound.ca (519) 376-1440 x3300

Consultant

Tatham Engineering Limited
115 Sandford Fleming Drive, Suite 200
Collingwood, ON L9Y 5A6
Mark Figueroa, P.Eng.
Project Manager
mfigueroa@tathameng.com
(705) 444-2565 x2142

Engineering Services Division City of Owen Sound 808 2nd Avenue East Owen Sound ON N4K 2H4



Telephone: 519-376-1440 Facsimile: (519) 376-3579 Website: www.owensound.ca

9^{TH} AVENUE EAST CLASS ENVIRONMENTAL ASSESSMENT – WATER DISTRIBUTION ALTERNATIVES FOR THE SUPERIOR STREET TO 6^{TH} STREET EAST AREA

Notice of Study Completion

The City of Owen Sound has undertaken a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. Specifically, the City has considered options to improve the reliability of the water distribution system in this area where there are current water supply risks in the event of a watermain break. The recommended solution is to install a watermain from Superior Street to 6th Street East in easements on two private properties to complete a watermain loop parallel to 9th Avenue East from Superior Street to 8th Street East (watermain loop from 6th Street East to 8th Street East is already in place).

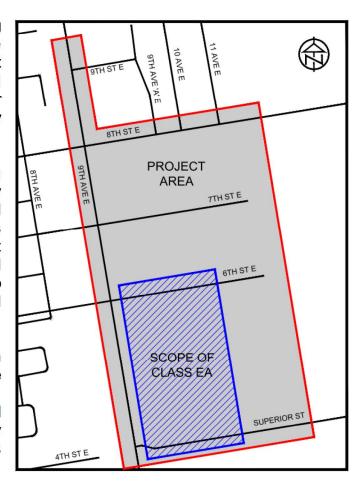
The watermain system improvements are being planned through the Schedule B process in the Municipal Class Environmental Assessment (2023). Consultation with the public, technical agencies, property owners and other stakeholders have informed the study recommendations.

A Project File Report documenting the planning process undertaken, details of the study recommendations and potential impacts and mitigation measures, has been completed and is being made available for public review. Subject to comments received following this Notice and the receipt of approvals, the City intends to proceed with construction of the recommended project, as outlined in the Project File Report.

The Project File Report is available for review on the City's website (https://www.owensound.ca/en/city-hall/9th-avenue-east.aspx) and at Owen Sound City Hall (808 2nd Avenue East). Further information may be obtained from one of the following members of the project team:

Owner

City of Owen Sound 808 2nd Avenue East Owen Sound, ON N4K 2H4 **Chris Webb, P.Eng.** Manager of Engineering Services cwebb@owensound.ca (519) 376-1440 x3300



Consultant

Tatham Engineering Limited
115 Sandford Fleming Drive, Suite 200
Collingwood, ON L9Y 5A6
Mark Figueroa, P.Eng.
Project Manager
mfigueroa@tathameng.com
(705) 444-2565 x2142

Interested persons may provide written comments to our project team by February 8, 2024. All comments and concerns should be sent directly to the City of Owen Sound by mail or email to the contact above.

Additionally, a request to the Minister of the Environment, Conservation and Parks for an order imposing additional conditions or requiring an individual environmental assessment may be made on the grounds that the requested order may prevent, mitigate or remedy adverse impacts on constitutionally protected Aboriginal and treaty rights. Requests should include your full name and contact information.

Requests should specify what kind of order is being requested (additional conditions or an individual environmental assessment), explain how an order may prevent, mitigate or remedy potential adverse impacts, and can include any supporting information.

The request should be sent to:

Minister of the Environment, Conservation and Parks Ministry of Environment, Conservation and Parks 777 Bay Street, 5th Floor Toronto, ON M7A 2J3 minister.mecp@ontario.ca

and

Director, Environmental Assessment Branch Ministry of Environment, Conservation and Parks 135 St. Clair Ave. W, 1st Floor Toronto, ON M4V 1P5 EABDirector@ontario.ca

Requests should also be sent to the City of Owen Sound by mail or email. Please visit the ministry's website for more information on requests for orders under Section 16 of the Environmental Assessment Act at: https://www.ontario.ca/page/classenvironmental-assessments-part-ii-order

All personal information included in your request such as name, address, telephone number and property location, is collected under the authority of Section 30 of the Environmental Assessment Act and is collected and maintained for the purpose of creating a record that is available to the general public. As this information is collected for the purpose of a public record, the protection of personal information provided in the Freedom of Information and Protection of Privacy Act (FIPPA) does not apply (s.37). Personal information you submit will become part of a public record that is available to the general public unless you request that your personal information remain confidential.

Personal information is collected under the authority of the Environmental Assessment Act, s.30. The information collected will be used to complete the environmental assessment process, and will form part of the public record. Questions about this collection should be addressed to Briana Bloomfield, City Clerk at bbloomfield@owensound.ca or 519-376-4440 ext. 1247.

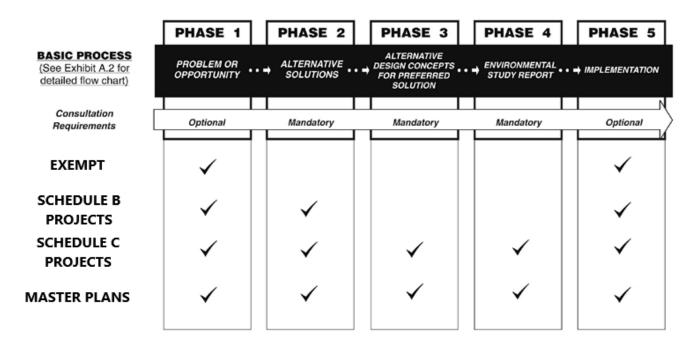
This notice issued January 9, 2024

Appendix B: Class EA Guidelines

MUNICIPAL CLASS ENVIRONMENTAL ASSESSMENT

Municipal Engineers Association

March 2023

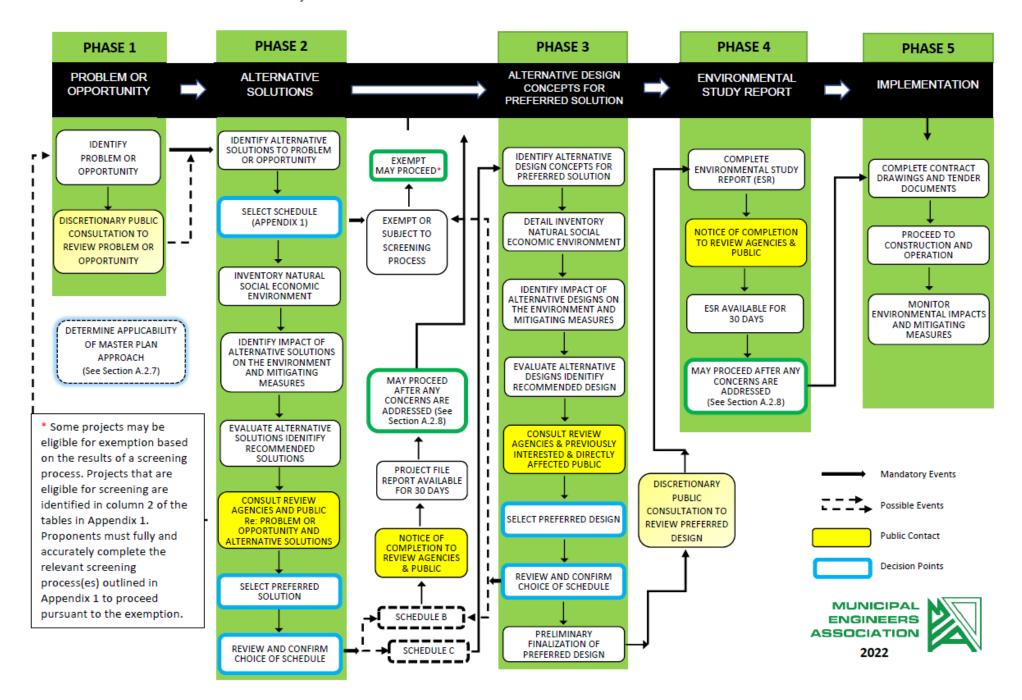


Notes:

 At a minimum, master plans the same steps of the first two phases of the MCEA process.

EXHIBIT A.2. MUNICIPAL CLASS EA PLANNING AND DESIGN PROCESS

NOTE: This flow chart is to be read in conjunction with Part A of the MCEA



Appendix C: Water Modelling Results Summary

tathameng.com



File 121387

Aug 26, 2022

Chris Webb City of Owen Sound 808 2nd Avenue East Owen Sound, Ontario N4K 2H4 cwebb@owensound.ca

Re: 9th Avenue East Watermain Replacement and Road Rehabilitation

Water Model Analysis

Dear Chris:

Tatham Engineering Limited (Tatham) has completed a hydraulic analysis using the City of Owen Sound's WaterCAD water distribution system model in support of the preliminary design for the 9th Avenue East watermain replacement and road rehabilitation project. The purpose of the analysis was to evaluate the hydraulic performance of the replacement watermain on 9th Avenue East and the 150 mm and 200 mm diameter pipe options for the new looping watermain from 8th Street East to Superior Street. The hydraulic analysis included consideration of future water demands for the proposed residential development at 1409 8th Street East.

DESIGN CRITERIA

The water distribution analysis was completed using the design criteria listed below, based on the Owen Sound Engineering Standards (City of Owen Sound, 2013) and the Design Guidelines for Drinking Water Systems (MECP, 2008).

Residential Population Density 2.3 persons per unit (ppu)

Average Day Demand - residential 400 L/person/day

Maximum Day Factor (MDF) 1.9

New or replacement PVC pipes created in the model were assigned a Hazen-Williams friction factor (C-factor) of 120.

WATER DEMANDS

Water demands were calculated for the proposed 721 residential units at the 1409 8th Street East future development site. The total Average Day Demand (ADD) and Maximum Day Demand (MDD) were calculated to be 7.68 L/s and 14.6 L/s, respectively.





The water demand calculations are appended in Attachment 1.

MODEL SETUP

The following changes were made to the City's WaterCAD water distribution model (last updated March 2022) to simulate the replacement of the 9th Avenue East watermain, the construction of the looping watermain, and the future development at 1409 8th Street East.

1409 8th Street East Future Development

New junction J-888 was created in the model on the 300 mm diameter PVC watermain on 8th Street East. The calculated ADD and MDD for the proposed residential development were assigned to junction J-888.

9th Avenue East Reconstruction

The existing 150 mm and 200 mm diameter cast iron watermain on 9th Avenue East from 8th Street to Superior Street was changed to 200 mm diameter PVC watermain.

The 150 mm diameter watermain connecting Superior Street to 9th Avenue East and located on private property, was deactivated in the model. A new 200 mm diameter watermain was added on 9th Avenue East to directly connect the watermain sections north and south of Superior Street.

Looping Watermain

New PVC watermain from 8th Street East to Superior Street was added based on Watermain Alignment Option #5 shown on Attachment 2.

The existing 150 mm diameter cast iron watermain on Superior Street from 9th Avenue East to the looping watermain connection was changed to a PVC pipe.

Physical scenarios were created in the model to simulate 150 mm and 200 mm diameter PVC pipe options for the looping watermain and the replacement of watermain on Superior Street. The lengths for the new PVC watermain were calculated using the scaled-length function in WaterCAD.

Connections from the looping watermain to the existing watermain on 6th Street East and 7th Street East were added to the model, eliminating the dead ends.

Initial Model Settings

The model results were simulated using the initial settings as found in the model. The initial model settings were the same for all demand scenarios and are summarized in Table 1. Pump 2 at the East Hill Booster Pump Station (BPS) was on, all pressure reducing valves (PRVs) across the boundary of the East Hill pressure zone were active, and the initial hydraulic grade line at the Norm Robertson Reservoir was 248.2 m.



Table 1: Initial Model Settings

ELEMENT	INITIAL STATUS	INITIAL WATER ELEVATION (m)	INITITAL PRESSURE SETTING (kPa)
East Hill BPS	Active. One pump ON (EH. P-2)	-	-
Norm Robertson Reservoir	Active	248.2	-
PRV-5 #108	Active	-	310.3
PRV-4 #112	Active	-	303.4
PRV-3 #111	Active	-	310.4
PRV-2 #110	Active	-	262

MODEL RESULTS

The model was used to analyze flows, pressures, and pipe velocities for the proposed new and replacement watermains under the following steady state scenarios: ADD, MDD, MDD + Fire Flow (FF), and simulated fire at 9th Avenue East and Superior Street (J-811).

Each scenario was analyzed for both 150 mm and 200 mm diameter PVC pipe options for the looping watermain and Superior Street.

A summary of the model set up and results for pipes and junctions located throughout the East Hill pressure zone (8th Street East, 9th Avenue East, Superior Street, and looping watermain), along with figures showing the model results for each scenario, are appended in Attachment 3.

Model Results for 200 mm Diameter PVC Watermain

Table 2 summarizes the range of pressures, flows, and pipe velocities under each scenario, for the 200 mm diameter watermain option.

The model results indicate the following:

- Pressure ranging between 336 kPa (49 psi), at node J-811 on 9th Avenue south of Superior Street, and 635 kPa (92 psi), at node J-22 on 9th Avenue at 6th Street East, under ADD and MDD scenarios. The pressures are within the City of Owen Sound's Engineering Standards allowable range for normal operating conditions of 275 kPa (40 psi) to 700 kPa (102 psi).
- Available fire flows ranging from 54 L/s, south of the intersection of 9th Avenue and Superior Street, to 233 L/s on 8th Street East with a minimum pressure of 20 psi.



A maximum pipe velocity of 1.63 m/s in pipe P-1393 on 9th Avenue south of Superior Street. This is below the maximum velocity of 3.0 m/s recommended by the Design Guidelines for Drinking Water Systems (MECP, 2008).

Table 2: 200 mm Diameter PVC Pipe Scenario

SCENARIO _	PRESSU	PRESSURE (kPa)		AFF (L/s)		PIPE VELOCITY (m/s)	
	MIN	MAX	MIN	MAX	MIN	MAX	
ADD	337	635	-	-	-	-	
MDD	336	634	-	-	-	-	
MDD + FF	138	405	54	233	-	-	
MDD + Fire at J-811	-	-	-	-	0.03	1.63	

Model Results for 150 mm Diameter PVC Watermain

Table 3 summarizes the range of pressures, flows, and pipe velocities under each scenario, for the 150 mm diameter watermain option.

Table 3: 150 mm Diameter PVC Pipe Scenario

SCENARIO —	PRESSU	IRE (kPa)	AFF	(L/s)	PIPE VELOCITY (m/s)	
3321711113	MIN	MAX	MIN	MAX	MIN	MAX
ADD	337	635	-	-	-	-
MDD	336	633	-	-	-	-
MDD + FF	138	424	43	244	-	-
MDD + Fire at J-811	-	-	-	-	0.03	1.63

The model results indicate the following:

• Pressure ranging between 336 kPa (49 psi) on 9th Avenue south of Superior Street, and 635 kPa (92 psi) at 9th Avenue and 6th Street under ADD and MDD scenarios, which are within the City of Owen Sound's Engineering Standards.



- Available fire flows ranging from 43 L/s, south of 9th Avenue and Superior Street, to 244 L/s on 8th Street East with a minimum pressure of 20 psi.
- A maximum pipe velocity of 1.63 m/s in pipe P-1393 on 9th Avenue south of Superior Street, which is below the maximum velocity of 3.0 m/s recommended by the MECP.

ANALYSIS

Analysis of the 150 mm and 200 mm diameter watermain options modelled is as follows:

- There is no significant difference in operating pressures between the two options.
- For the 200 mm option, available fire flow is improved by 11 L/s to 43 L/s along 9th Avenue, Superior Street, and the looping watermain.
- In the case of a fire in the vicinity of the intersection of 9th Avenue and Superior Street, the pipe velocities experienced in the 9th Avenue and looping watermains are slightly higher for the 150 mm option than for the 200 mm option. Pipe velocities are within MECP recommendations for both diameters.
- The 200 mm option provides full redundancy for the 9th Avenue watermain between 8th Street East and Superior Street.

RECOMMENDATIONS

The WaterCAD model results predict that either of the proposed watermain sizes will provide an adequate supply of water for domestic use and fire protection. However, the 200 mm option would provide a moderate improvement in fire flow and full redundancy for the 9th Avenue watermain. Therefore, construction of the 200 mm diameter watermain option is recommended.



We trust this report is sufficient to support the evaluation of watermain sizes with regard to hydraulic performance. Should you have any questions or require any further analysis, please do not hesitate to contact us.

Yours truly,
Tatham Engineering Limited

Emily Park, B. Eng. Engineering Intern

EP/JRC:pt

Encl. - WaterCAD Demand Calculations, Watermain Layout Figure, WaterCAD Results and Figures

Jason R. Covey, B.Sc.(Eng.), P.Eng.

Senior Engineer

copy: Spencer Hammill, EIT City of Owen Sound shammill@owensound.ca

l:\2021 Projects\121387 - 9th Avenue East Reconstruction, Owen Sound\Documents\Reports\Water Model Analysis\L - Webb - 9th Avenue Water Model Analysis.docx





PROJECT	9th Ave E Watermain Replacement and Road Rehabilitation	FILE DATE	1213 June	<i>-</i> ,	2022
SUBJECT			EP		
	Water Demand Calculation	PAGE	1	OF	1

Number of Units			
Residential			
Single Detached	117	units	
Townhouse	444	units	
Apartment	160	units	
Total	721	units	(Bousfields Inc., April 2021)
Population Density	2.3	persons/unit	(Owen Sound Engineering Standards, 2013)
Residential Population	1,659	persons	
Design Criteria			
Average Day Demand	400	L/person/day	(Owen Sound Engineering Standards, 2013)
Maximum Day Factor	1.9		(MECP Design Guidelines, for systems serving a population between 10,000 and 25,000 persons)
Design Flows			
Average Day Flow	7.68	L/s	
Maximum Day Flow	14.59	L/s	



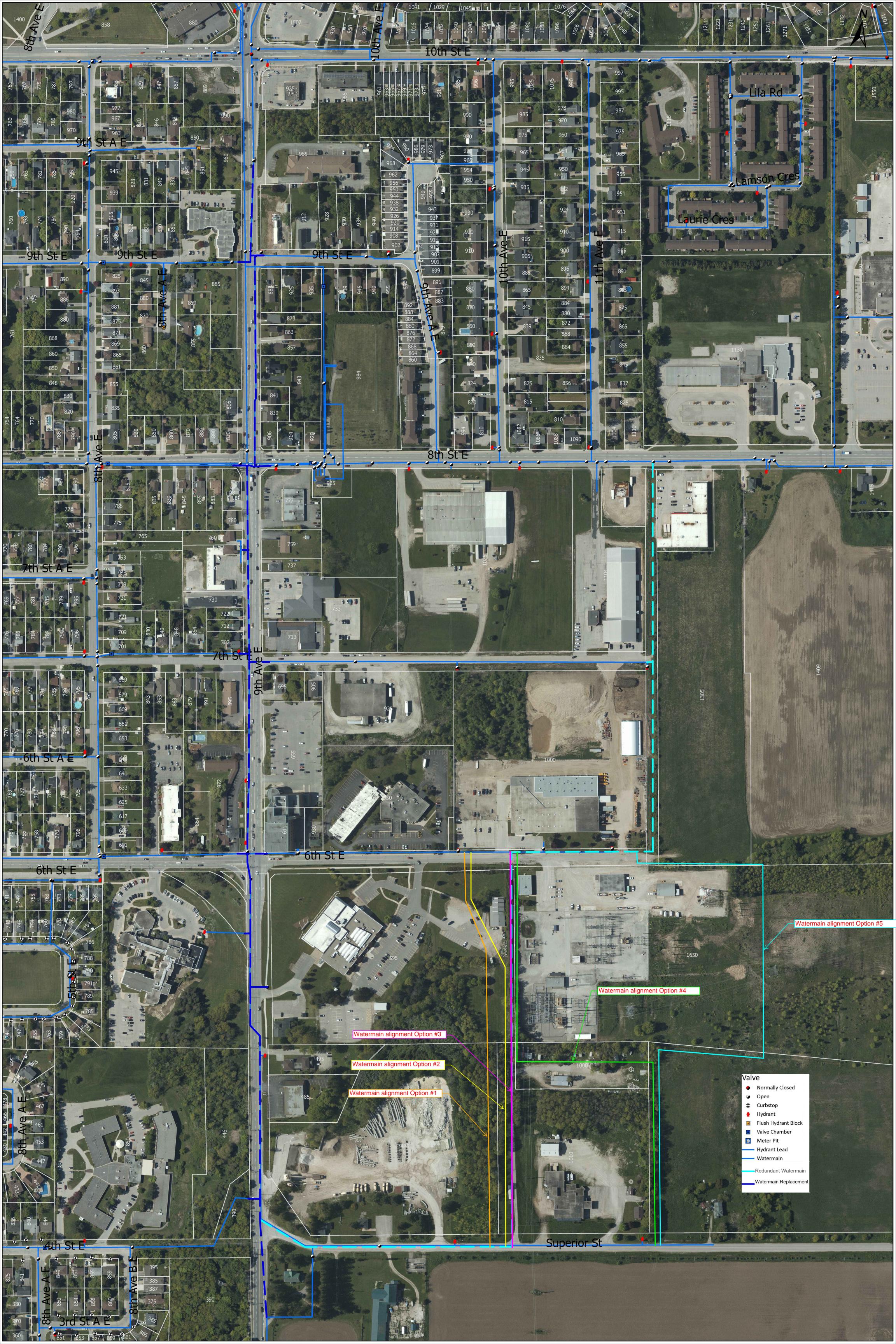
PROJECT	9th Ave E Watermain Replacement	FILE	1213	87	
	and Road Rehabilitation	DATE	June	29,	2022
SUBJECT	WaterCAD Demands	NAME	EP		
	WaterCAD Demands	PAGE	1	OF	1

Design Criteria

Average Day Demand 400 L/person/day (Owen Sound Engineering Standards, 2013)

Maximum Day Factor 1.9 (MECP Design Guidelines, for systems serving a population between 10,000 and 25,000 persons)

WaterCad Flows						Water D	emands		
Development	Description	Node ID	No. of Units	ppu	Pop.	ADD (L/s)	ADD (m³/day)	MDD (L/s)	MDD (m³/day)
1409 8th Street East	Residential	J-888	721	2.3	1658	7.68	663.32	14.59	1260.31





PROJECT	9th Ave E Watermain Replacement	FILE	1213	87	
and Road Rehabilitation		DATE	June	30,	2022
SUBJECT			EP		
	WaterCAD Results - Pressure	PAGE	1	OF	4

Watermain Diameter Scenarios

Scenario A: All watermains in reconstruction of 9th Ave E and looping watermain from 8th St to Superior St to be constructed of 200 mm diameter PVC pipes.

Scenario B: All watermains in reconstruction of 9th Ave E to be constructed of 200 mm diameter

PVC pipes and looping watermain from 8th St to Superior St to be constructed of 150

mm diameter PVC pipes.

Scenario A Average Day Demand

Node	Elev.	Demand	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	0.6	299.4	59	404
J-22	234.6	0.8	299.4	92	635
J-19	234.8	0.3	299.5	92	633
J-17	243	0.0	299.5	80	553
J-6	238.3	0.2	299.6	87	600
J-5	242.2	0.4	299.6	81	562
J-3	245.7	0.2	299.6	76	527
J-600	244.5	1.1	299.5	78	539
J-827	260.46	0.0	299.4	55	382
J-828	246	0.0	299.4	76	523
J-829	239.49	0.0	299.6	85	588
J-879	248.39	0.0	299.6	73	501
J-881	245.28	0.0	299.5	77	531
J-884	242	0.0	299.5	82	562
J-886	242	0.0	299.5	82	562
J-887	258.2	0.0	299.4	59	404
J-888	251.6	7.7	299.5	68	469
J-811	265	0.0	299.4	49	337
	Total	11.2			

Maximum Day Demand

Node	Elev.	Demand	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	0.6	299.4	58	403
J-22	234.6	0.9	299.4	92	634
J-19	234.8	0.3	299.5	92	633
J-17	243	0.0	299.4	80	552
J-6	238.3	0.2	299.6	87	600
J-5	242.2	0.4	299.6	81	561
J-3	245.7	0.2	299.5	76	527
J-600	244.5	1.1	299.4	78	538
J-827	260.46	0.0	299.4	55	381
J-828	246	0.0	299.4	76	522
J-829	239.49	0.0	299.5	85	587
J-879	248.39	0.0	299.5	73	500
J-881	245.28	0.0	299.4	77	530
J-884	242	0.0	299.4	81	562
J-886	242	0.0	299.4	81	562
J-887	258.2	0.0	299.4	58	403
J-888	251.6	14.6	299.4	68	468
J-811	265	0.0	299.4	49	336

Total 18.2



PROJECT	9th Ave E Watermain Replacement	FILE	1213	87	
	and Road Rehabilitation	DATE	June	30, 2	2022
SUBJECT	WaterCAD Results - Pressure	NAME	EP		
	WaterCAD Results - Pressure	PAGE	2	OF	4

Available Fire Flow

Node	Elev.	AFF	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	103	299.03	27	189
J-22	234.6	143	299.03	59	405
J-19	234.8	173	299.24	57	393
J-17	243	190	299.28	20	138
J-6	238.3	206	299.46	31	212
J-5	242.2	203	299.48	51	351
J-3	245.7	206	299.45	46	318
J-600	244.5	233	299.29	33	225
J-827	260.46	105	299.05	21	146
J-828	246	114	299.03	43	298
J-829	239.49	109	299.38	20	138
J-879	248.39	201	299.34	41	282
J-881	245.28	178	299.22	39	266
J-884	242	139	299.11	41	280
J-886	242	120	299.08	41	283
J-887	258.2	110	299.06	21	146
J-888	251.6	217	299.29	32	218
J-811	265	54	299.02	34	232



PROJECT	9th Ave E Watermain Replacement		1213	87	
	and Road Rehabilitation	DATE	June	30,	2022
SUBJECT		NAME	EP		
	WaterCAD Results - Pressure	PAGE	3	OF	4

Scenario B Average Day Demand

Node	Elev.	Demand	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	0.6	299.4	59	404
J-22	234.6	0.8	299.4	92	635
J-19	234.8	0.3	299.5	92	633
J-17	243	0.0	299.5	80	553
J-6	238.3	0.2	299.6	87	600
J-5	242.2	0.4	299.6	81	562
J-3	245.7	0.2	299.6	76	527
J-600	244.5	1.1	299.5	78	539
J-827	260.46	0.0	299.4	55	382
J-828	246	0.0	299.4	76	523
J-829	239.49	0.0	299.6	85	588
J-879	248.39	0.0	299.6	73	501
J-881	245.28	0.0	299.5	77	531
J-884	242	0.0	299.4	82	562
J-886	242	0.0	299.4	82	562
J-887	258.2	0.0	299.4	59	404
J-888	251.6	7.7	299.5	68	469
J-811	265	0.0	299.4	49	337
	Total	11.2			

Maximum Day Demand

Node	Elev.	Demand	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	0.6	299.3	58	402
J-22	234.6	0.9	299.3	92	633
J-19	234.8	0.3	299.4	92	633
J-17	243	0.0	299.5	80	553
J-6	238.3	0.2	299.6	87	600
J-5	242.2	0.4	299.6	81	561
J-3	245.7	0.2	299.6	76	527
J-600	244.5	1.1	299.5	78	538
J-827	260.46	0.0	299.3	55	380
J-828	246	0.0	299.3	76	522
J-829	239.49	0.0	299.5	85	587
J-879	248.39	0.0	299.5	73	500
J-881	245.28	0.0	299.4	77	530
J-884	242	0.0	299.3	81	561
J-886	242	0.0	299.3	81	561
J-887	258.2	0.0	299.3	58	402
J-888	251.6	14.6	299.5	68	468
J-811	265	0.0	299.3	49	336
	Total	18 2			



PROJECT	9th Ave E Watermain Replacement and Road Rehabilitation		1213	87	
			June	30, 2	2022
SUBJECT			EP		
	WaterCAD Results - Pressure	PAGE	4	OF	4

Available Fire Flow

Node	Elev.	AFF	HGL	Pres	sure
ID	(m)	(L/s)	(m)	psi	kPa
J-25	258.2	79	298.82	28	190
J-22	234.6	109	298.84	61	424
J-19	234.8	151	299.13	61	420
J-17	243	190	299.31	20	138
J-6	238.3	205	299.46	31	217
J-5	242.2	201	299.47	51	355
J-3	245.7	206	299.45	46	316
J-600	244.5	244	299.31	30	209
J-827	260.46	67	298.83	20	138
J-828	246	87	298.82	45	309
J-829	239.49	109	299.4	20	138
J-879	248.39	203	299.37	39	270
J-881	245.28	150	299.1	22	152
J-884	242	99	298.89	25	174
J-886	242	77	298.86	33	226
J-887	258.2	67	298.85	20	138
J-888	251.6	230	299.32	30	206
J-811	265	43	298.81	34	232



PROJECT	9th Ave E Watermain Replacement		121387			
	and Road Rehabilitation	DATE	July	4, 20	22	
SUBJECT	WaterCAD Results - Pipe	NAME	EP			
	Velocitiy	PAGE	1	OF	2	

Watermain Diameter Scenarios

Scenario A: All watermains in reconstruction of 9th Ave E and looping watermain from 8th St to Superior St to be constructed of 200 mm diameter PVC pipes.

Scenario B: All watermains in reconstruction of 9th Ave E to be constructed of 200 mm diameter PVC pipes and looping watermain from 8th St to Superior St to be constructed of 150

mm diameter PVC pipes.

Scenario A

MDD + Fire at J-811 (50 L/s)

Pipe	Diameter (mm)	Length (m)	Roughness	Velocity (m/s)	Friction Loss (m/m)			
Red	udant Wate	rmain +	Superior Stree	t (200 mm dia	1.)			
P-1385(1)	200	198	120	0.93	0.006			
P-1385(2)	200	214	120	0.87	0.005			
P-1390	200	188	120	0.64	0.003			
P-1391	200	118	120	0.64	0.003			
P-1392	200	234	120	0.64	0.003			
P-1305	200	170	120	0.64	0.003			
	9th A	venue E	ast Reconstru	ction				
P-25	200	198	120	1.06	0.007			
P-28	200	212	120	1.07	0.007			
P-1306	200	247	120	1.03	0.007			
P-1393	200	155	120	1.63	0.016			
		7th	Street E					
P-1209	150	281	72	0.08	0			
	-	6th	Street E					
P-30	200	380	60	0.2	0.001			
8th Street E								
P-3	300	101	140	0.65	0.001			
P-820(2)(1)(1)	300	160	140	0.23	0			
P-822	300	233	140	0.03	0			



PROJECT	9th Ave E Watermain Replacement	FILE	1213	387	
	and Road Rehabilitation	DATE	July	4, 20	22
SUBJECT	WaterCAD Results - Pipe	NAME	EP		
	Velocitiy	PAGE	2	OF	2

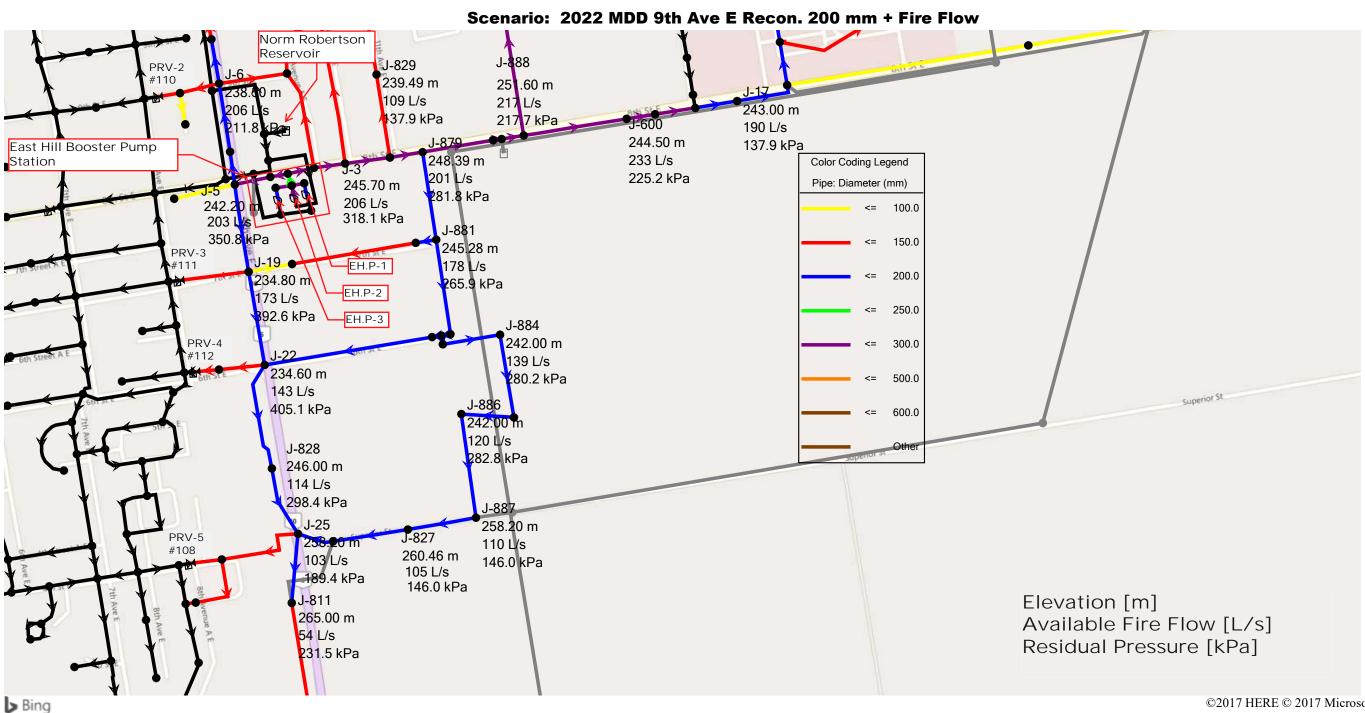
Scenario B

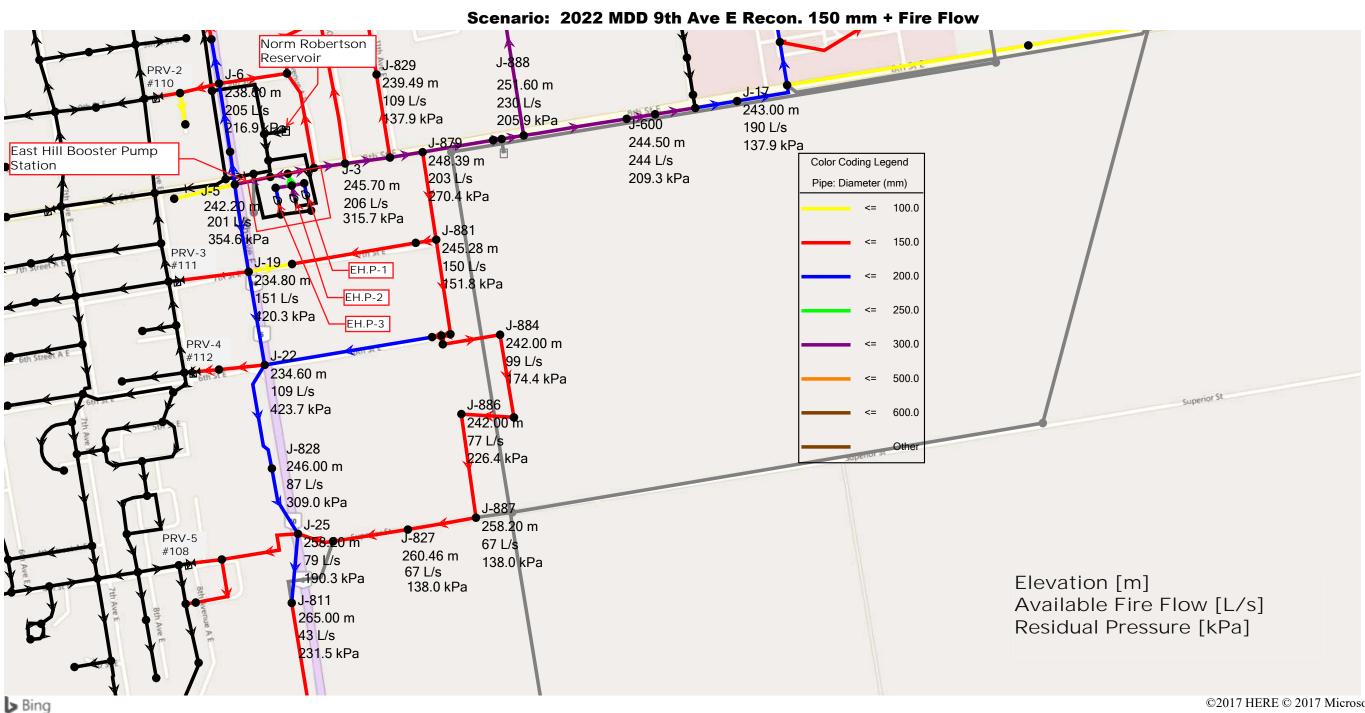
MDD + Fire at J-811 (50 L/s)

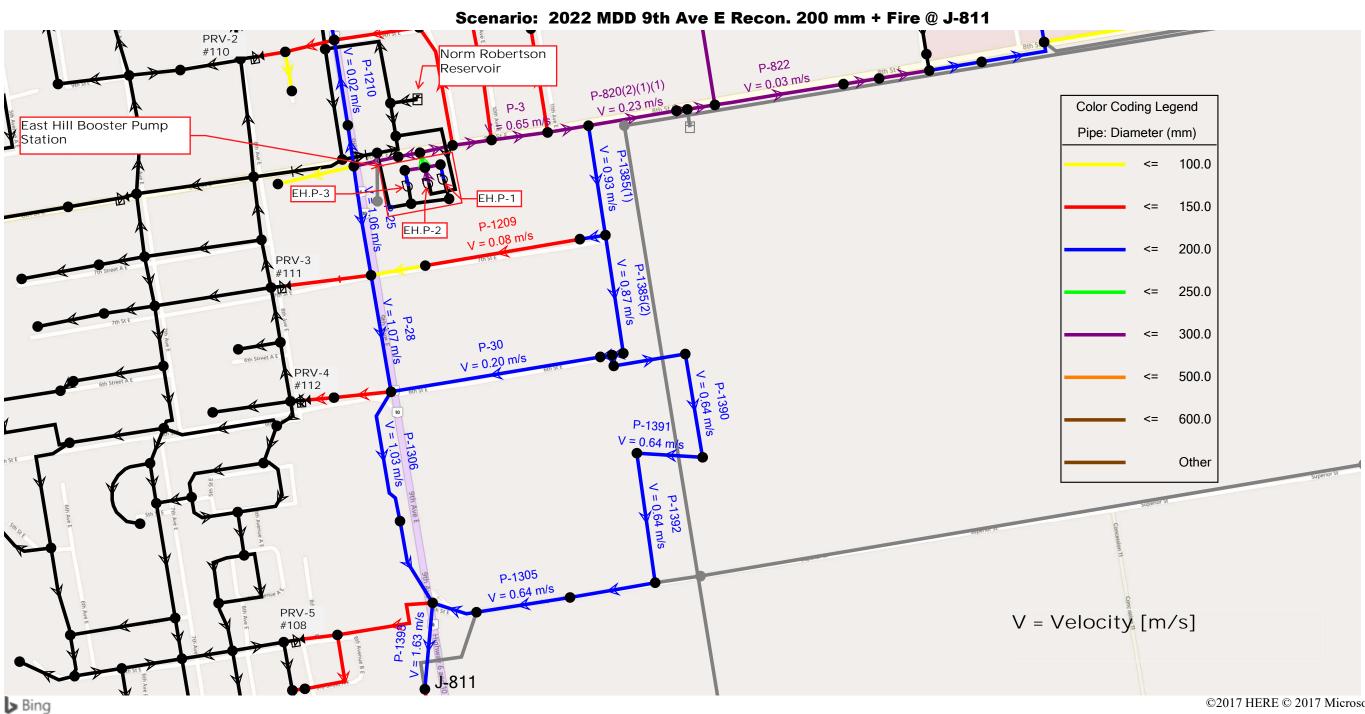
Pipe	Diameter (mm)	Length (m)	Roughness	Velocity (m/s)	Friction Loss (m/m)		
Redi	udant Wate	rmain +	Superior Stree	t (150 mm dia	a.)		
P-1385(1)	150	198	120	1.12	0.011		
P-1385(2)	150	214	120	1.01	0.009		
P-1390	150	188	120	0.65	0.004		
P-1391	150	118	120	0.65	0.004		
P-1392	150	234	120	0.65	0.004		
P-1305	150	170	120	0.65	0.004		
9th Avenue East Reconstruction							
P-25	200	198	120	1.36	0.011		
P-28	200	212	120	1.38	0.011		
P-1306	200	247	120	1.3	0.01		
P-1393	200	155	120	1.63	0.016		
		7th	Street E				
P-1209	150	281	72	0.08	0		
		6th	Street E				
P-30	200	380	60	0.17	0.001		
8th Street E							
P-3	300	101	140	0.54	0.001		
P-820(2)(1)(1)	300	160	140	0.25	0		
P-822	300	233	140	0.03	0		

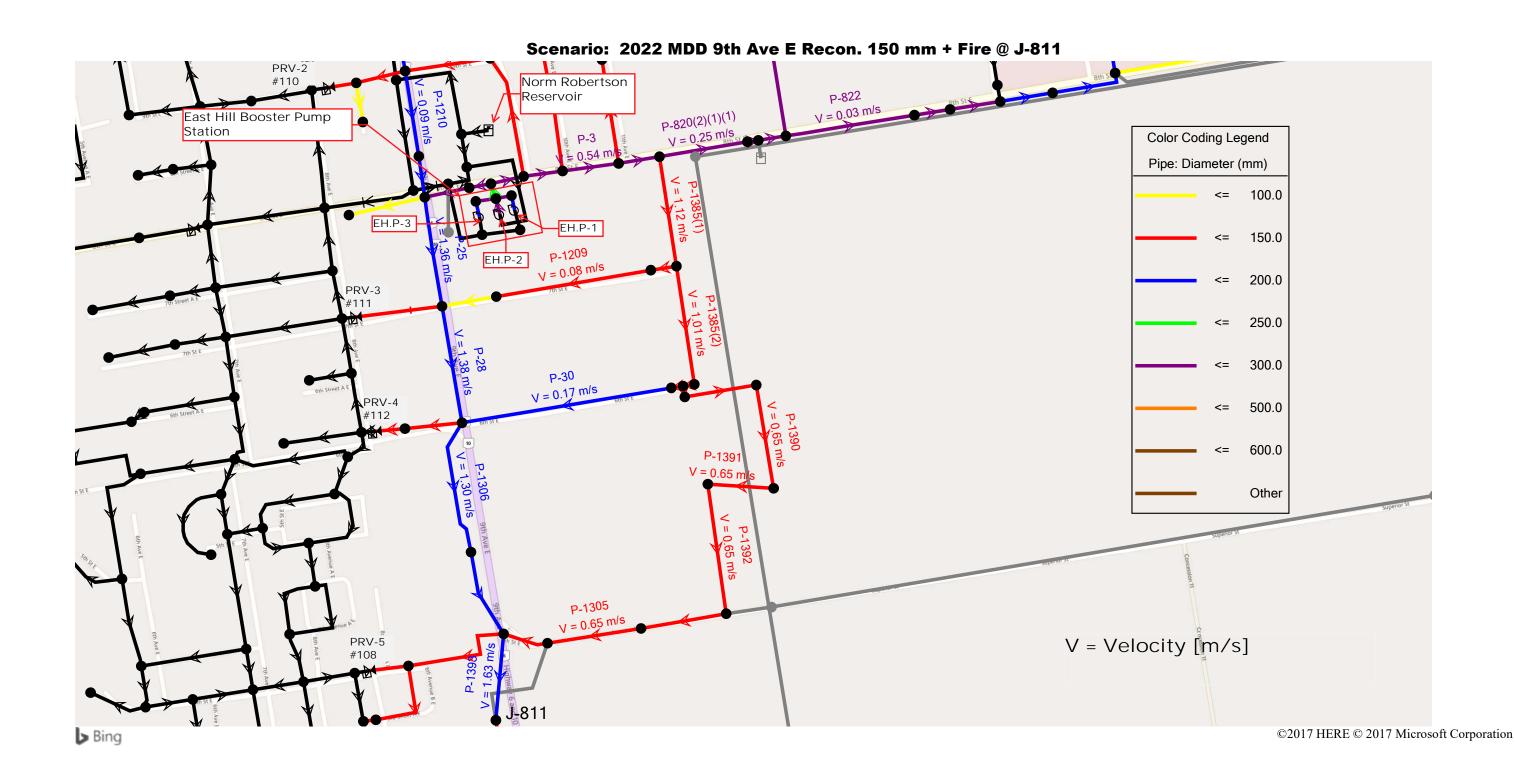
Scenario: 2022 MDD 9th Ave E Recon. 200 mm Norm Robertson Reservoir J-829 587.3 kPa J-88 468.2 kPa 239.49 m J-600 552.4 kPa 251.60 m 537.7 kPa 243.00 m Color Coding Legend 244.50 m Pipe: Diameter (mm) East Hill Booster Pump 500.0 kPa Station <= 100.0 248.39 m 526.9 kPa 245.70 m <= 150.0 EH.P-1 242.20 m 200.0 530.0 kPa PRV-3 245.28 m 632.9 kPa 250.0 EH.P-3 234.80 m <= 300.0 J-884 561.8 kPa 500.0 242.00 m 634.0 kPa 600.0 234.60 m Other 561.7 kPa 242.00 m J-828 522.4 kPa 246.00 m 403.1 kPa J-25 258.20 m #108 380.9 kPa 258.20 m 260.46 m J-811 Pressure [kPa] 336.4 kPa Elevation [m] 265.00 m **Bing**

Scenario: 2022 MDD 9th Ave E Recon. 150 mm Norm Robertson Reservoir J-829 587.4 kPa J-88 468.8 kPa 239.49 m J-600 552.5 kPa 251.60 m 537.8 kPa 243.00 m Color Coding Legend 244.50 m East Hill Booster Pump Pipe: Diameter (mm) 500.1 kPa Station <= 100.0 248.39 m 527.0 kPa 245.70 m <= 150.0 242.20 m 200.0 529.7 kPa J-19 🕶 EH.P-1 245.28 m 632.5 kPa 250.0 EH.P-2 234.80 m <= 300.0 EH.P-3 J-884 561.1 kPa 500.0 242.00 m 633.4 kPa 600.0 234.60 m Other 561.0 kPa 242.00 m J-828 521.7 kPa 246.00 m J-887 J-25 402.4 kPa J-827 PRV-5 402.9 kPa 258.20 m #108 380.2 kPa 258.20 m 260.46 m J-811 Pressure [kPa] 335.7 kPa Elevation [m] 265.00 m **Bing**









Appendix D: Environmental Impact Study



Scoped Environmental Impact Study Owen Sound Watermain Improvements – Early Design Stage City of Owen Sound

Prepared for: Tatham Engineering Ltd.

Prepared by: Azimuth Environmental Consulting, Inc.

February 2023

AEC 21-453



Environmental Assessments & Approvals

February 3, 2023 AEC 21-453

Tatham Engineering Ltd.
Mark Figueroa
115 Sandford Fleming Drive, Suite #200
Collingwood, Ontario L9Y 5A6

Re: Scoped Environmental Impact Study – 9th Avenue East to 10th Street East, City of Owen Sound

Dear Mr. Figueroa:

Azimuth Environmental Consulting, Inc. was retained to provide a Scoped Environmental Impact Study in support of a Municipal Class Environmental Assessment pertaining to municipal watermain improvements between 9th Avenue and 10th Avenue in the City of Owen Sound. The purpose of this report is to provide the City with an understanding of natural environmental conditions and potential impacts related to the proposed design alternatives on natural heritage features and functions in the study area, including Species at Risk and their habitat.

The assessment concludes that the recommended Preferred Option #3 can be achieved with the least impact to natural heritage features and functions, including Species at Risk, relative to the other design alternatives. Confirmatory planning consultation may be advised regarding the Niagara Escarpment Plan.

Should you have any questions please do not hesitate to contact the undersigned.

Yours truly,

AZIMUTH ENVIRONMENTAL CONSULTING, INC.

Dr. Scott Tarof, Ph.D. (Biology)

Terrestrial Ecologist



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1.0 INTRODUCTION

Azimuth Environmental Consulting, Inc. (Azimuth) was retained by Tatham Engineering Ltd. (Tatham) to prepare a Scoped Environmental Impact Study (EIS) supporting a Municipal Class Environmental Assessment (Class EA) involving watermain improvements in the City of Owen Sound (City), Grey County (County) (Figure 1). The project is in the early design stages. It is our understanding that a Scoped EIS has been requested in support of the Class EA. The study area is in the jurisdiction of the Grey Sauble Conservation Authority (GSCA), but is not within the GSCA Regulation Limit, therefore it is expected a permit under Ontario Regulation (O. Reg.) 151/06 will not be required.

The purpose of this Scoped EIS is to identify candidate Natural Heritage Features and Functions (NHFFs) in the study area associated with five watermain alignment alternative solutions (Alternative Options #1-5) and evaluate potential impacts of the proposed alternatives on those NHFFs to recommend a preferred solution from a natural heritage perspective. The Scoped EIS satisfies the natural heritage obligations of the Class EA and will assist the project team in identification of a preferred alignment solution. A review of background information, combined with field surveys, was undertaken in spring/summer 2022 to identify existing NHFFs in the study area. The report also examines potential for Species at Risk (SAR) and SAR habitat protected under Ontario's *Endangered Species Act*, 2007 (ESA). The potential for negative impacts to identified NHFFs is considered and recommendations for avoidance and mitigation are provided.

For the purposes of this Scoped EIS, the study area comprises lands containing the watermain alignment alternatives, as shown on Figures 1-3, plus adjacent lands within approximately 120 metres (m) of the alignment alternatives. Natural heritage features and functions in the overall planning area beyond study area limits are discussed where applicable throughout the report.

2.0 PLANNING CONTEXT

2.1 Provincial Planning Policy (2020)

The Provincial Policy Statement (PPS) (MMAH, 2020) outlines policies related to natural heritage features (Section 2.1) and water resources (Section 2.2). Ontario's *Planning Act*, (1990) requires that planning decisions shall be consistent with the PPS. The study area for this assessment is located entirely in Ecoregion 6E. According to the PPS, development and site alteration shall not be permitted in:



- Significant wetlands in Ecoregions 5E, 6E and 7E; and,
- Significant coastal wetlands.

Similarly, Section 2.1.5 of the PPS states that, unless it has been demonstrated that there will be no negative impacts on the natural features or their ecological functions, development and site alteration shall not be permitted within:

- a) significant wetlands in the Canadian Shield north of Ecoregions 5E, 6E; and 7E;
- b) significant woodlands in Ecoregions 6E; and 7E;
- c) significant valleylands in Ecoregions 6E; and 7E;
- d) significant wildlife habitat;
- e) significant areas of natural and scientific interest; and,
- f) coastal wetlands in Ecoregions 5E, 6E; and 7E that are not subject to policy 2.1.4(b)

It is ultimately the responsibility of the Province and/or the Municipality to designate areas identified within Section 2.1.4 and 2.1.5 of the PPS as "significant".

Section 2.1.6 of the PPS states that development and site alteration is not permitted in fish habitat except in accordance with federal and provincial requirements.

Section 2.1.7 of the PPS states that development and site alteration shall not be permitted in habitat of Threatened and Endangered species, except in accordance with provincial and federal requirements.

Furthermore, under Section 2.1.8 of the PPS, no development and site alteration will be permitted on lands adjacent to natural heritage features and areas identified in policies 2.1.4, 2.1.5 and 2.1.6 unless the ecological function of the adjacent lands has been evaluated and it has been demonstrated there will be no negative impacts on the natural features and ecological functions.

2.2 Endangered Species Act (2007)

Ontario's ESA provides regulatory protection to Endangered and Threatened species prohibiting harassment, harm and/or killing of individuals and destruction of their habitats. Habitat is broadly characterized within the ESA as the area prescribed by a regulation as the habitat of the species or an area on which the species depends, directly or indirectly, to carry on its life processes including reproduction, rearing of young, hibernation, migration or feeding.



The various schedules of the ESA included under O. Reg. 230/08 identify SAR in Ontario. These include species listed as Extirpated, Endangered, Threatened and Special Concern. As noted above, only species listed as Endangered and Threatened receive protection from harm and destruction to habitat on which they depend.

2.3 County of Grey

According to Schedule A - Map 1 of the County Official Plan (OP; 2019), the study area is designated as within a Primary Settlement Area (Appendix A).

The study area does not occur in mapped Provincially Significant Wetlands (PSWs), Significant Coastal Lands or Hazard Lands (Schedule A - Map 1; Appendix A), nor is it in a mapped Core Area or Linkage Area (Schedule C; Appendix A). Grey County mapping (2022) shows no woodlands, County Forests, unevaluated wetlands or watercourses associated with the study area (County Map #1; Appendix A).

The southern portion of the study area is mapped as part of the Niagara Escarpment Plan Area [Urban Area and Escarpment Protection Area (County Map #2), see also OP Schedule A - Map 1; Appendix A)] (see Section 2.5 below).

2.4 City of Owen Sound

The study area is designated in the City OP (2022) as Employment, Arterial Commercial, Institutional and Niagara Escarpment Plan Area (Schedule A; Appendix A).

Section 6.1.4.3 states that municipal public works projects are exempt from development constraints associated with Significant Woodlands.

2.5 Niagara Escarpment Plan (2017)

As per the Niagara Escarpment Plan (NEP; NEC, 2017), part of the study area is in the Niagara Escarpment Plan Area - Urban Area and Escarpment Protection Area (Map #7 and County Map 2; Appendix A). Section 1.3.3 of the Niagara Escarpment Plan (2017) lists "Infrastructure" as a permitted land use in the Niagara Escarpment Plan Area. Although a development permit through the Niagara Escarpment Commission (NEC) would not be anticipated, the client may wish to confirm with the Niagara Escarpment Commission.

2.6 Grey Sauble Conservation Authority

The study area is outside the GSCA Regulation Limit (Schedule A - Map 1, GSCA Regulation Limit Map; Appendix A). Consequently, it is anticipated a GSCA permit under O. Reg. 151/06 would not be required.



3.0 STUDY APPROACH

A combination of background information and field data were used to fulfill the objectives of this Scoped EIS. Unless indicated otherwise, the scope of the field program focused on the defined study area. Azimuth undertook the following activities for this study:

- Searched the County, GSCA, Ministry of Natural Resources and Forestry
 (MNRF) and Ministry of the Environment, Conservation and Parks (MECP)
 records to obtain available background information, including current information
 related to natural heritage conditions including SAR;
- Conducted the following field surveys:
 - Defined and mapped vegetation community types in the area of watermain alignment alternatives based on Ecological Land Classification (ELC) methods;
 - o Completed two (2) vascular plant inventories (spring and summer, 2022);
 - Completed two (2) dawn breeding bird surveys with emphasis on determining if habitat for Bobolink and/or Eastern Meadowlark were present (SAR birds);
 - Characterized the vegetated area designated as "woodland" to determine potential habitat for SAR bats;
- Completed a SAR habitat assessment based on background information and fieldwork to identify SAR/SAR habitat that could be present in the study area;
- Recorded wildlife observations and assessed potential for Significant Wildlife Habitat (SWH) function according to provincial criteria;
- Assisted the client with evaluation of alignment alternatives for proposed watermain improvements with regard for NHFFs identified; and,
- Assessed the potential direct and indirect impacts of the project on NHFFs in the study area.

The early design stage of the project involves an evaluation of alternative solutions to help identify a preferred solution for future detailed design, and the study area is not regulated by the GSCA. Consequently, confirmation of a Terms of Reference with the GSCA for the field program and impact assessment was not part of the scope.

3.1 Background Data

A review of background documents provided information on property characteristics, habitat, wildlife, rare species and communities, and general cultural/historic aspects of the study area. Background documentation included a review of the following:



- Natural Heritage Information Center (NHIC) data from the Ministry of Natural Resources and Forestry (MNRF, 2022);
 - o Make-A-Map: Natural Heritage Areas application
- Ontario Ministry of Natural Resources (OMNR) Natural Heritage Reference Manual (NHRM; OMNR, 2010);
- Atlas of the Breeding Birds of Ontario (OBBA; Cadman *et al.*, 2007);
- Ontario Reptile and Amphibian Atlas (2020);
- iNaturalist (2022);
- MECP SAR Ontario list (2022);
- Bat Survey Standards Note (MECP, 2021);
- Government of Canada's Species at Risk Public Registry (2022);
- Aerial photographs available for the study area (Google Earth Pro, VuMap);
- Atlas of the Mammals of Ontario (Dobbyn, 1994);
- County interactive mapping (2022);
- County OP (2019); and,
- City OP (2022).

3.2 Vegetation Community Mapping and Surveys

Prior to undertaking detailed field studies, an initial classification of habitats was undertaken using recent air photo imagery for an area encompassing the study area. Vegetation community types and boundaries in association with the study area were confirmed and characterized in the field using ELC methods (Lee 2008, Lee *et al.* 1998) based on field surveys undertaken on June 10 (temperature: 19°C, cloud cover: 0%, Beaufort wind: B2, precipitation: none) and August 12, 2022 (temperature: 22°C, cloud cover: 5%, Beaufort wind: B1-2, precipitation: none) during spring and summer growing seasons, respectively (Figure 2).

To describe vascular plant species composition, a two-season plant inventory was conducted to compile a list of species by ELC vegetation community. Property visits were undertaken by a qualified ecologist with existing knowledge related to rare, Threatened and Endangered vascular plant species with potential to occur in the area. The assessment was focused during ELC work to ensure that appropriate effort was made to detect any federally or provincially designated plant species, notably SAR as identified by the provincial ESA or provincially rare plants. The inventories included consideration for SAR plants, such as Butternut (*Juglans cinerea*) (Endangered) and Black Ash (*Fraxinus nigra*) (Endangered) which are protected under the ESA.

To estimate the amount of woodland cover (ha) in the study area and on adjacent lands (*i.e.* landscape scale), the polygon tracing tool was used in Google Earth Pro. Woodland cover east of the terminus of 6th Street East and west of 9th Avenue East was excluded



because gaps between woodland edges were approximately 70-165m wide, exceeding the maximum 20m gap that constitutes a single woodland feature, as defined in the NHRM (OMNR, 2010).

3.3 Wildlife Surveys

Wildlife species utilizing the study area were identified from direct observation, auditory signs and through interpretation of other signs (tracks, scats, vocalizations, *etc.*) as a matter of course while conducting field surveys.

3.3.1 Species at Risk

The SAR screening undertaken for this assignment included an assessment of SAR with potential to occur at the County scale. The County list was modified based on habitat features in the area and species' ranges. Where potentially suitable habitat was present, the assessment included SAR occurrence records from the NHIC database (Appendix B). Habitat requirements and appropriate designations (Endangered, Threatened or Special Concern) are outlined in Table 1. The SAR assessment followed the MECP Guidance Document - Client's Guide to Preliminary Screening for SAR (MECP, 2019).

3.3.2 Breeding Birds

Two dawn breeding bird surveys were conducted at six point count stations on June 2 and June 15, 2022 (Figure 2), guided by point count methodology in the OBBA Guide for Participants (OBBA, 2001). Surveys were conducted no earlier than one half hour before sunrise and were completed prior to 10:00am. Surveys were completed under suitable weather conditions [*i.e.* light winds (Beaufort wind scale ≤3)]. Point counts were five minutes (min) in duration and otherwise followed the protocol of the Ontario Breeding Bird Atlas Guide for Participants (OBBA, 2001). Survey station locations were distributed throughout the study area to confer reasonable coverage of vegetation communities relative to the alternative solutions. Breeding evidence was assessed using OBBA (2001) criteria. All birds seen or heard were identified to species and counted.

3.3.3 Bats and Bat Habitat

Several bat species including (but not limited to) SAR Little Brown Myotis, Northern Myotis and Tri-colored Bat may utilize trees in early stages of decay ("snag" trees) for the purposes of maternity colony roosting and/or day roosting during the late spring and summer seasons. Larger trees [e.g. at least 25 centimetres (cm) diameter at breast height (DBH)] are often preferred by bats as roost trees; however, trees of any size have the potential to be used (MECP, 2021; MNRF, 2015a). Trees described as "snag" trees are those having cracks, splits, holes, etc. that could feasibly provide access for roosting bats.



Given the woodland cover in portions of the study area, on June 14, 2022 Azimuth conducted a *high level* screening for SAR bat habitat in the study area. The objective of the screening was to evaluate whether or not there was potential for SAR bat habitat to be present in the vicinity of any of the proposed watermain alignment alternatives. Since the objective was not to generate a detailed map of each candidate bat snag tree, the screening was completed during leaf-out. The survey involved a roving search of woodland areas; the presence of leaves on the trees did not limit survey effectiveness. Given the characteristics of the woodland areas screened (*e.g.* relatively narrow treed areas, access throughout), results of the bat habitat screening would not be expected to be different had the survey been completed during leaf-off conditions. The general areas in the study area where potential SAR bat habitat was observed were mapped in relation to the ELC vegetation communities (Figure 2).

4.0 EXISTING CONDITIONS

4.1 Land Use

The estimated 15.8 hectare (ha) defined study area is located on the southeastern perimeter of Owen Sound, and is bound by 9th Avenue East to the west, 8th Street East to the north and Superior Street to the south. The eastern-most extent of the study area is approximately 730m east of 9th Avenue East. The study area consists of a combination of industrial (*e.g.* Hydro One, Miller aggregate site) and residential land uses interspersed with woodland and open field habitat areas (Figure 2). A hydroelectric corridor passes through the central region of the study area in a generally north-south direction.

Adjacent land use includes rural residential lots along Superior Street separated by open fields, hedgerows and agricultural lands.

4.2 Terrestrial Resources

4.2.1 Vegetation

Limits of the 11 unique ELC communities identified in the study area are illustrated on Figure 2. Some of the communities occur multiple times in the study area, but they differ in species composition. The patch of White-Ash Deciduous Woodland Thicket (WODM4-2) is adjacent to Maintained Lawn that extends south to the Dry-Fresh White Ash-Hardwood Deciduous Forest (FODM4-2) (Figure 2). A complete list of vascular plant species identified is presented in Tables 2a and 2b, and summary descriptions of ELC vegetation communities are provided in Table 3. Appendix C provides a photographic record of the study area associated with the alternative options.



A total of 151 vascular plant species were identified in the study area, 83 (55%) of which are considered native to Ontario (Tables 2a and 2b). No SAR plant species were observed, including no Butternut or Black Ash. None of the vegetation communities or plant species documented are of federal or provincial conservation concern, and no plant species are considered rare provincially (*i.e.* S1-S3) (NHIC, 2022).

4.2.2 Wildlife

4.2.2.1 Mammals and Other Incidental Wildlife Observations

Evidence of three mammalian species [Eastern Chipmunk (*Tamias striatus*). Gray Squirrel (*Sciurus carolinensis*), White-tailed Deer (*Odocoileus virginianus*)] were observed in the study area. Given study area proximity to large natural wooded and field areas at the landscape scale, it is expected that the following mammals could also conceivably be encountered in the study area: small mammal species (various mice, voles and shrews); Red Squirrel (*Tamiasciurus hudsonicus*); Eastern Cottontail (*Sylvilagus floridanus*); Ermine (*Mustela erminea*); Long-tailed Weasel (*Neogale frenata*); Least Weasel (*Mustela nivalis*); Groundhog (*Marmota monax*); Striped Skunk (*Mephitis mephitis*); Porcupine (*Erethizon dorsatum*); Eastern Coyote (*Canis latrans*); Red Fox (*Vulpes vulpes*); and Raccoon (*Procyon lotor*).

No salamanders, newts or reptiles were observed over the course of the field program.

4.2.2.2 Breeding Birds

A total of 35 bird species were detected in the study area during the dawn breeding bird surveys (Table 4). Eastern Meadowlark (Threatened), including at least one female, was confirmed in the study area in association with the Dry-Fresh Mixed Meadow (MEMM3) ELC polygon proximal to Point Count Stations #2-3 (Figure 2). The species was also detected on adjacent lands approximately 150-200m east of 1150 Superior Street on the north side of the road (Figure 2). Eastern Meadowlark were detected during both dawn breeding bird surveys, and evidence of breeding was treated as evident based on observations of at least one female.

Eastern Wood-pewee (Special Concern) was heard singing near Point Count Station #6 and on adjacent lands on the south side of Superior Street (Figure 2).

4.2.3 Bats and Bat Habitat

Woodland screening for presence of potential candidate bat snags in the study area identified a small number of trees that may potentially be used by roosting bats. Approximately two hedgerow trees immediately west of 1025 6th Street East were observed in the hedgerow/fencerow (TAGM5) ELC community to have low quality bat snag features (Figure 2); however, in Azimuth's experience, hedgerow habitat is not



typically considered to be habitat for SAR bats. Immediately south of this hedgerow, in the FODM4-2 corridor west of 1000 Superior Street, an estimated 20 trees were observed to have bat snag features (cavities, hollows, peeling bark, dead limbs) that could be used by SAR bats (if present) (Figure 2). Approximately 50% of the candidate bat snag trees observed in this FODM4-2 corridor would likely be considered "high quality" bat snag trees because of the combination of snag features present, feature height (3-10m, >10m up the trunk of the trees) and tree location (on edge of corridor – bats often travel along woodland edges when searching for insects). No other trees were observed in the study area that had candidate bat snag features.

4.3 Species at Risk

The SAR assessment (Table 1) considers SAR and SAR habitat with potential to occur in the study area in accordance with field data, known SAR for Grey County (Endangered, Threatened or Special Concern) and NHIC records (see Appendix B), scoped to consider potential habitat opportunities in the study area limits. Based on this assessment, in combination with vegetation communities and other environmental features observed during the investigation, the following species are considered below in this report:

• Threatened or Endangered;

- Eastern Meadowlark;
- o Little Brown Myotis (Potential);
- o Northern Myotis (Potential);
- o Tri-colored Bat (Potential);

• Special Concern;

- o Eastern Wood-pewee; and,
- Monarch (Potential).

Only species designated as Threatened or Endangered receive individual and habitat protection under Section 9 and Section 10 of the ESA. Special Concern species are discussed in the context of Significant Wildlife Habitat (SWH) (Special Concern and Rare Wildlife Species).

4.4 Wetlands

Background NHIC and VuMap mapping indicate no wetlands in the study area or on adjacent lands, including no PSWs on municipal or provincial resources for the area (Appendix B). Three small marsh communities (MAMM1-2, MAMM1-16 and MAMM3) were observed in the field (Figure 2). For the purposes of this assessment, these features are considered as "Other Wetlands".



4.5 Significant Woodlands

Woodlands in the study area and on adjacent lands were estimated to be 4.1ha in size. The City OP defines woodlands as Significant Woodlands if the feature is 4ha or greater in size. Consequently, woodlands in the study area are considered Candidate Significant Woodlands for the purposes of this assessment.

4.6 Significant Valleylands

No portion of the study area is identified as Significant Valleyland nor assigned a similar designation on City, County (Appendix A) or provincial mapping resources (NHIC, 2022; Appendix B). There are no valleyland features in the study area according to standards presented in the NHRM, principally due to the lack of permanent or intermittent watercourses that constitute a defining component of a valleyland feature. Furthermore, no portion of the study area fulfills the well-defined valley morphology and landform prominence required to be considered Candidate Significant Valleyland.

4.7 Significant Wildlife Habitat

An assessment of the potential for SWH in the study area was conducted using criteria outlined in MNRF's Significant Wildlife Habitat Technical Guide (2000) and the accompanying the Ecoregion 6E Criteria Schedules (MNRF, 2015). The following SWH types were considered to be present, or have potential to occur, based on results of the field program, organized by habitat type below:

- Bat Maternity Colonies (Potential);
- Special Concern and Rare Wildlife Species;
 - o Eastern Wood-pewee; and,
 - o Monarch Butterfly (Potential).

These candidate SWH types are discussed below (Impact Assessment) in the context of SWH function.

4.8 Areas of Natural and Scientific Interest

No portion of the study area is identified as ANSI on City, County (Appendix A) or provincial mapping resources (NHIC, 2022; Appendix B).

4.9 Fish and Fish Habitat

No mapped watercourses are indicated in the study area, as per City, County or regional mapping resources (Appendix A), nor were watercourses observed in the field in the study area. No features with potential to provide fish habitat were documented in study area limits.



5.0 NATURAL HERITAGE FEATURES AND FUNCTIONS

The results of Azimuth's field studies combined with review of background information indicate the potential for the following candidate NHFFs in the study area:

- Habitat for Threatened or Endangered Species;
 - o Eastern Meadowlark:
 - o Little Brown Myotis (Potential);
 - o Northern Myotis (Potential);
 - o Tri-colored Bat (Potential);
- Other Wetlands:
- Candidate Significant Woodlands;
- Candidate Significant Wildlife Habitat;
 - o Bat Maternity Colonies (Potential);
 - Special Concern and Rare Wildlife Species;
 - Eastern Wood-pewee; and,
 - Monarch Butterfly (Potential).

6.0 PRELIMINARY PROPOSED ALTERNATIVE SOLUTIONS

The project is in the early design stage. The proposed development is a municipal works project involving five watermain alignment alternatives (Figure 3). The looping watermain will be constructed east of 9th Avenue East and extend between 8th Street East and Superior Street. The two main portions of the watermain will be between 8th Street East to 6th Street East, and then continue south from 6th Street East to Superior Street. The 8th Street East to 6th Street East section will consist of a single line approximately 430m in length, installed in a City-owned block currently lined with hydro poles.

The City is considering five alignment alternatives between 6th Street East and Superior Street. The preferred solution will be installed with open-cut construction methods and a minimum cover of 1.8m. Below we summarize the watermain alignment alternatives under consideration between 6th Street East and Superior Street. Detailed design drawings will be part of a future design stage once the preferred solution has been identified. As such, specific details regarding the work limits associated with each watermain alignment alternative are not currently known.

6.1 Alternative Option #1

Alternative Option #1 would involve installing the watermain from the City-owned block in the 6^{th} Street East road allowance to the 6^{th} Street East frontage at the 595 9^{th} Avenue East property. The watermain would continue south underneath the existing parking lot within easements on the 595 9^{th} Avenue East and the 425 9^{th} Avenue East properties.



The existing watermain on Superior Street would be replaced to connect to the 9th Avenue East watermain. Alternative Option #1 involves the watermain running south at the left-most position in that portion of the study area in easements on the 595 9th Avenue East and the 425 9th Avenue East (Figure 3).

6.2 Alternative Option #2

In Alternative Option #2, watermain construction would entail installing the watermain from the City-owned block in the 6th Street East road allowance to the 6th Street East frontage at the 595 9th Avenue East property. The watermain would continue south in easements on the 595 9th Avenue East property in front of the building at the northeast corner of the property and the property at 1010 Superior Street. The existing watermain on Superior Street would be replaced to connect to the 9th Avenue East watermain. Alternative Option #2 involves the watermain running south in a central alignment within easements on the 595 9th Avenue East and the 425 9th Avenue East (Figure 3).

6.3 Alternative Option #3

In Alternative Option #3, watermain construction would entail installing the watermain from the City-owned block in the 6th Street East road allowance to the 6th Street East frontage at the 595 9th Avenue East property. The watermain would continue south in easements on the 595 9th Avenue East property behind the building at the northeast corner of the property and the 1010 Superior Street property. The existing watermain on Superior Street would be replaced to connect to the 9th Avenue East watermain. Between 6th Street East and Superior Street, Alternative Option #3 involves the watermain running south along the eastern edge of the easements on the 595 9th Avenue East and the 425 9th Avenue East (Figure 3).

6.4 Alternative Option #4

Alternative Option #4 would involve installing the watermain from the City-owned block in the 6th Street East road allowance to the 6th Street East frontage at the 595 9th Avenue East property. The watermain would continue south in easements on the 595 9th Avenue East property behind the building at the northeast corner of the property, turn east through the 1000 Superior Street property and then turn south along the west side of 1150 Superior Street. The existing watermain on Superior Street would be replaced to connect to the 9th Avenue East watermain (Figure 3).

6.5 Alternative Option #5

Alternative Option #5 would originate southward from 8th Street East in the City-owned block (the same as Alternative Options #1-4) to 6th Street East, then turn east and then south in easements along the central portions of 1650 Superior Street. The watermain



would then continue west toward 1000 Superior Street and south in easements on the 1150 Superior Street property (Figure 3). The existing watermain on Superior Street would be replaced to connect to the 9th Avenue East watermain.

7.0 PRELIMINARY IMPACT ASSESSMENT OF ALTERNATIVE SOLUTIONS

This impact assessment is prepared with regard for the proposed watermain alignment alternatives. Background information and results of the field program were used to evaluate possible preliminary impacts to NHFFs pertaining to the alternative solutions. The assessment summarizes potential constraints that may be associated with each solution. The primary intent is to identify possible environmental sensitivities for client consideration as the project progresses to detailed design. A more detailed impact assessment may be needed during detailed design once more information is available for the preferred solution. Constraints deemed worthy of further consideration are discussed below in relation to each alternative solution, followed by a summary.

7.1 Habitat for Threatened or Endangered Species

Impacts with regards to the ESA and Habitat of Threatened or Endangered species are covered under Section 9 and 10 of the ESA. Section 9 deals directly with killing, harming or harassing living members of a species. Section 10 covers destruction or damage to habitat of Threatened or Endangered species. According to the PPS, development and site alteration shall not be permitted in habitat of Threatened or Endangered species, except in accordance with provincial and federal requirements. The following Threatened or Endangered species have the potential to occur in or adjacent to the study area:

- Eastern Meadowlark;
- Little Brown Myotis (Potential);
- Northern Myotis (Potential); and,
- Tri-colored Bat (Potential).

7.1.1 Eastern Meadowlark

Eastern Meadowlark were detected calling in one portion of the study area, specifically in association with Alternative Option #5 and on adjacent lands approximately 150m east of 1150 Superior Street (Figure 2). Nest locations were not identified. Under Section 10 of the ESA in regards to habitat protection, damage or destruction of habitat is considered a contravention. Habitat for Eastern Meadowlark in MEMM3 would be impacted by encroachment if Alternative Option #5 were to be selected. Under this scenario, consultation with MECP would be required to outline a mitigation approach to help minimize impacting the species. Due to the nature of the proposed watermain



improvements (*i.e.* a temporary open-cut trench), mitigation might take the form of habitat restoration (*e.g.* site preparation and reseeding post-construction); however, MECP consultation would be recommended. The MECP might also require an Information Gathering Form for Eastern Meadowlark with Alternative Option #5.

The anticipated work limits associated with Alternative Options #1 to #4 would not encroach into habitat for Eastern Meadowlark. Consequently, proposed infrastructure works in these other four regions of the study area would not pose an impact to Eastern Meadowlark. The study area is proximal to a highly urbanized landscape to the north, south and west, with Eastern Meadowlark present to the east. The species will most likely continue to be present post-construction. Providing the mitigation measures recommended in Section 8.0 below are followed, the potential for indirect impacts to SAR grassland bird habitat would be considered mitigable.

7.1.2 Little Brown Myotis, Northern Myotis and Tri-colored Bat

The screening for potential bat snag trees found approximately 20 candidate bat snag trees in the FODM4-2 woodland corridor between 405 9th Avenue East and 1010 Superior Street (Figure 2). Work limits associated with Alternative Options #1, #2 or #3 would be considered an encroachment into potential SAR bat habitat in this region of the study area. Consequently, the proposed infrastructure works in Alternative Options #1, #2 or #3 would represent removal of a small number of candidate snag trees with potential to provide habitat for SAR bats (if present). The anticipated work limits associated with Alternative Options #4 or #5 would not encroach into suitable habitat for SAR bats.

In regards to treed habitat for maternity or day roosting by SAR bats, the Bat Survey Standards Note (MECP, 2021) states "If a proposed activity will avoid impairing or eliminating the function of habitat for supporting bat life processes (*e.g.* remove, stub, *etc.* a small number of potential maternity or day roost trees in treed habitats) but the timing of tree removal will avoid the bat active season (April 1-September 30 in Southern Ontario), then there is no need to conduct species at risk bat surveys of treed habitats." Based on this direction from the MECP, and given only a small number of potential bat habitat snags would be removed, the potential for impact to SAR bat habitat would be considered acceptable and would not trigger the need for additional bat surveys or MECP consultation. This assessment is based on tree removals occurring outside the active bat season (*i.e.* removals between October 1 and March 31 of a given year).

Providing the mitigation measures recommended in Section 8.0 below are followed, the potential for indirect impacts to SAR bat habitat in relation to Alternative Options #1 to #5 would be considered mitigable.



7.2 Other Wetlands

Three small isolated MAMM (Mineral Meadow Marsh) wetlands were identified in the field east of 1025 6th Street East (Figure 2). Alternative Option #5 would encroach into Other Wetlands in the form of an open-cut trench. Consequently, Alternative Option #5 would pose a direct impact to Other Wetlands. The anticipated open-cut trench work limit for Alternative Option #4 would be adjacent (within approximately 5m) to Other Wetlands. Alternative Options #1 to #3 would not encroach into wetland, and therefore, would not represent a direct impact to wetlands. In some development situations, encroachment into wetlands may be approved (*e.g.* for infrastructure); however, GSCA consultation, mitigation and possible restoration of indirect wetland impact would likely be required for works in or immediately adjacent to wetlands.

Another consideration pertaining to Alternative Options #4 or #5 is the possibility of alteration of wetland hydrology. Soils in the vicinity of the wetlands were observed to be moist in the field. Engineering input regarding the potential need for dewatering of the open-cut trench during construction would be advised in relation to Alternative Options #4 or #5. Dewatering, if required, may affect wetland hydroperiod. In addition, pipe bedding might function as a wetland "drain", slowly removing water from the wetlands post-construction.

Provided the mitigation measures recommended below in Section 8.0 are followed, the potential for indirect impact to Other Wetlands in relation to Alternative Options #1 to #5 are considered mitigable.

7.3 Candidate Significant Woodlands

According to the PPS, development and site alteration are not permitted in Significant Woodlands in Ecoregion 6E, unless it can be demonstrated there will be no negative impacts to the feature and its ecological function. One (1) Candidate Significant Woodland feature was identified in the study area in association with the FODM4-2 ELC vegetation community west and south of 1000 6th Street East (Figure 2, see also Appendix B). Since the project will require tree removals to accommodate Alternative Options #1 to #4, watermain alignment work in this part of the study area would result in tree removals within Candidate Significant Woodlands. The anticipated work limits associated with Alternative Option #5 would not encroach into Candidate Significant Woodlands. Consequently, this alignment alternative would not result in tree removals in Candidate Significant Woodlands.



Section 6.1.4.3 in the City OP indicates that municipal public works projects are permitted in Significant Woodlands. Consequently, impacts to Candidate Significant Woodlands associated with Alternatives Options #1 to #4 would likely be deemed acceptable to the City, as per municipal policies. Regardless, it is Azimuth's opinion that Alternative Options #3 or #4, in particular, would not compromise the overall form or ecological function of the feature since construction would be along the eastern-most edge of the Candidate Significant Woodland as opposed to approximately 10-20m west of the feature edge (*i.e.* within the Candidate Significant Woodland - as the case would be for Alternative Options #1 or #2). Alternative Options #1 or #2 would fragment part of the Candidate Significant Woodland and possibly increase forest "edge effects" (*e.g.* increased risk of predation on bird nests and exposure to nest parasitism). Despite the urban setting, these impacts could affect breeding success of local birds. Providing mitigation recommendations in Section 8.0 below are implemented, the potential for indirect impacts to Candidate Significant Woodlands would, for the most part, be treated as mitigable.

7.4 Candidate Significant Wildlife Habitat

According to the PPS, development and site alteration are not permitted in SWH in Ecoregion 6E, unless it can be demonstrated there will be no negative impacts upon the feature and its ecological function.

7.4.1 Bat Maternity Colonies

Potential bat maternity roosting habitat was identified in the study area within the FODM4-2 ELC vegetation community (Figure 2). Although limited tree removals to accommodate Alternative Options #1 to #4 would be anticipated, the scale of tree removals will likely be relatively small (especially with Alternative Options #3 or #4) and the likelihood of loss of SWH form or function would be considered minimal and mitigable (especially with Alternative Options #3 or #4). Overall, the feature will remain post-development, and, at the landscape scale, potential habitat for roosting bats will not be impacted.

7.4.2 Special Concern and Rare Wildlife Species

Eastern Wood-pewee (Special Concern) was detected on adjacent lands only - approximately 60m east of the study area near Point Count Station #6 during the first dawn breeding bird survey but not during the second survey. A breeding evidence status of "Possible" would apply to the species. Since the species was not detected in the study area during the field program, neither the species nor its habitat will be impacted by the



proposed watermain improvements. As such, SWH feature and function for Eastern Wood-pewee will not be impacted.

Potential habitat for Monarch Butterfly [i.e. Common Milkweed plants (Asclepias syriaca)] was observed in THDM3, MEMM3 and WODM4-2 ELC vegetation communities in the study area (Figure 2), indicating the potential for Monarch Butterfly to be present. Individual Monarch were not observed. Habitat quality for Monarch Butterflies in these ELC polygons was low. Trees and thickets limited milkweed to a very sparse distribution. Areas in the surrounding landscape to the northeast and east would be considered to represent higher quality habitat more suitable for the species. Consequently, the likelihood for impact to Monarch habitat would be negligible.

Provided that the mitigation measures recommended in Section 8.0 are followed, the potential for indirect impacts to SWH function is considered mitigable.

7.5 Preliminary Impact Assessment Summary

The identification of a Preferred Option from a natural heritage perspective has been based on the relative degree to which each Alternative Option would encroach into NHFFs, or have the potential for direct or indirect impacts on NHFFs. Encroachment into a feature was considered a larger impact compared with no encroachment or works adjacent to a feature.

Based on the assessment, the Preferred Option recommended by Azimuth from a natural heritage perspective would be a watermain alignment footprint that extends south from 8th Street East to 6th Street East, west along 6th Street East to west of 1025 6th Street East, and then continues as Preferred Option #3 west of 1025 6th Street East and 1000/1010 Superior Street to the existing watermain along Superior Street. Preferred Option #3 would avoid impacts to Eastern Meadowlark habitat, wetlands (within or adjacent) and maintain the majority of SWH form and function for potential roosting bats. As per MECP (2021), Preferred Option #3 would not be considered a significant impact to habitat of SAR bats in the region. Preferred Option #3 would minimize impacts to the Candidate Significant Woodland. In addition, this option would avoid fragmentation of the FODM4-2 vegetation community (part of the Candidate Significant Woodland) and increasing possible edge effects for birds and local wildlife (Figure 3).

While Alternative Options #1 or #2 would be similarly mitigable as Preferred Option #3 in regards to possible impacts to SAR bats, these two options would most likely create some fragmentation effects of the Candidate Significant Woodland. In the case of Alternative Option #4, while the potential for impacts to the Candidate Significant Woodland, SAR bat habitat and SWH habitat for non-SAR bats would be



minimal/avoidable/mitigable, this option would involve construction immediately adjacent to wetlands (Figure 3). Construction immediately adjacent to wetlands may increase the possibility of chemicals entering into the wetlands in the event of a spill or leak. Alternative Option #5 would be mitigable (*e.g.* timing windows) in terms of species impacts to Eastern Meadowlark; however, it would be associated with impacts to habitat for Eastern Meadowlark (Figure 3). It follows that Alternative Option #5 would require consultation with the MECP and possible habitat restoration/compensation. Other Wetlands would also be impacted under Alternative Option #5, likely triggering GSCA consultation and possible wetland restoration/compensation post-construction. Consequently, overall, Preferred Option #3 would be considered the solution that minimizes natural heritage impacts to the extent possible.

8.0 RECOMMENDATIONS

8.1 Species at Risk

It should be noted that absence of a protected species in the study area does not indicate that they will never occur in the area. Given the dynamic character of the natural environment, there is a constant variation in habitat use. Care should be taken in the interpretation of presence of species of concern, including those listed under the ESA. Changes to policy or the natural environment could result in shifts, removal or addition of new areas to the list of areas currently considered candidate NHFFs. This report is intended as a point in time assessment of the potential to impact SAR; not to provide long term "clearance" for SAR. While there is no expectation that the assessment should change significantly, it is the responsibility of the proponent to ensure that they are not in contravention of the ESA at the time property works are undertaken.

8.2 Migratory Breeding Birds and Bat Habitat

Activities involving removal of vegetation/trees should be restricted from occurring during the migratory bird breeding season. Migratory birds, nests and eggs are protected by the *Migratory Birds Convention Act*, 1994 (MBCA) and the *Fish and Wildlife Conservation Act*, 1997 (FWCA). Environment Canada outlines dates when activities in any region have potential to impact nests at the Environment Canada Website (https://www.canada.ca/en/environment-climate-change/services/avoiding-harm-migratory-birds/general-nesting-periods.html). In Zones C1 and C2, vegetation/tree clearing should be avoided between **April 1 and August 31** of a given year to avoid impacts to migratory birds.

According to MECP guidelines, the window during which tree removals should not occur to avoid potential impacts to SAR bats and/or SAR bat habitat protected under the ESA is April 1 to September 30. To ensure protection measures for *both* birds and bats,



vegetation/tree removals should be avoided between **April 1 and September 30** of a given year.

8.3 Sediment and Erosion Controls

Diligent application of sediment and erosion controls based on Best Management Practices (BMPs) is recommended for future construction activities to minimize accidental or unavoidable impacts to adjacent vegetation communities (including Candidate Significant Woodlands, wetlands), bird, bat and wildlife habitat. Prior to commencement of site works, silt fencing should be applied along the length of the proposed work limits that are directly adjacent to natural or naturalized features. Routine inspection/maintenance of silt fencing is recommended (*e.g.* weekly or monthly) throughout future construction to help avoid the potential for impact to NHFFs. Soil stockpiles should be suitably isolated using sediment controls.

8.4 Operations

All maintenance activities required during future construction should be at least 30m away from woodlands, wetlands, habitat of SAR and SWH habitat, and follow BMPs at the time to prevent accidental spillage of deleterious substances that may harm natural environments. Snow fencing or equivalent should be installed around the perimeter of future work limits to prevent accidental intrusion of machinery operations into adjacent undisturbed natural areas.

9.0 CONCLUSIONS

Based on our analysis of NHFFs, it is concluded that Preferred Option #3 represents the least potential impact to environmental conditions in the study area through incorporation of the environmental protection measures described in Section 8.0. Given the NHFFs described resulting from the field program, Preferred Option #3 is Azimuth's recommendation as the most appropriate alignment for the City's watermain improvements in terms of minimizing impacts to NHFFs to the extent possible. While Alternative Options #1, #2 and #4 would be similar to the preferred option in some respects, they would have somewhat elevated natural heritage constraints related to either the Candidate Significant Woodland or wetlands. Due to Eastern Meadowlark habitat and wetlands, Alternative Option #5 would be associated with more substantial constraints relative to the other four options.

At this time, our findings are summarized as follows in regards to Preferred Option #3:

 Preferred Option #3 is consistent with policies/legislation of the ESA. Our impact assessment has given full consideration to habitat requirements of all SAR assumed and documented to occur in the area, and results indicate the Preferred



Option #3 will not result in unacceptable impacts to habitat of SAR, as identified in this study, providing conformance is demonstrated to mitigation measures described in Section 8.0;

- Preferred Option #3 is not expected to impact negatively the form or ecological function of Candidate Significant Woodland or Candidate SWH outlined in Section 5.0 if the appropriate mitigation measures outlined in Section 8.0 are followed; and,
- Proposed earth works or construction to implement watermain improvements at a
 future design stage may require additional assessment to confirm the potential for
 impacts to NHFFs.

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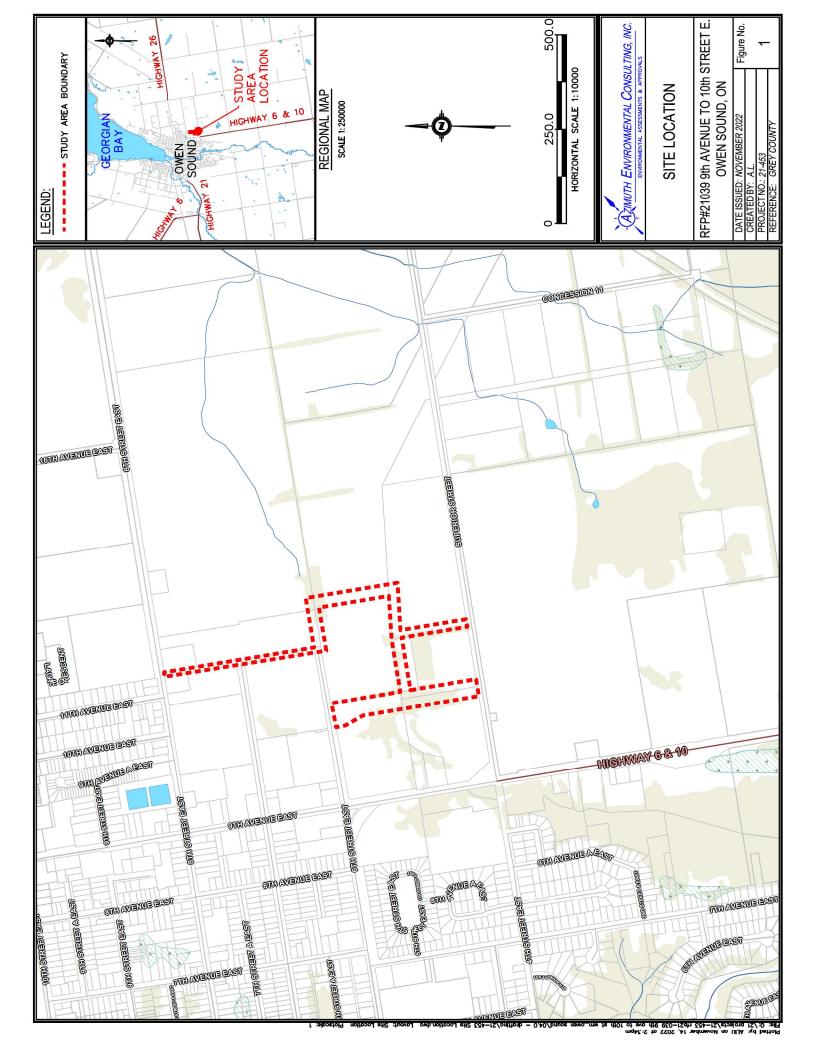
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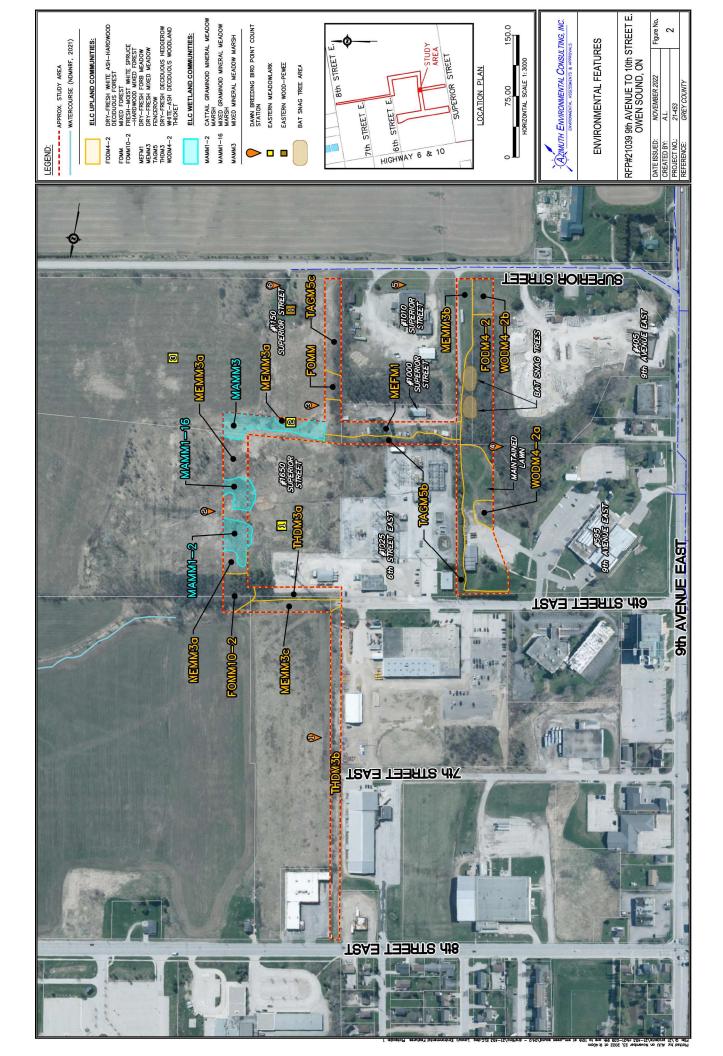
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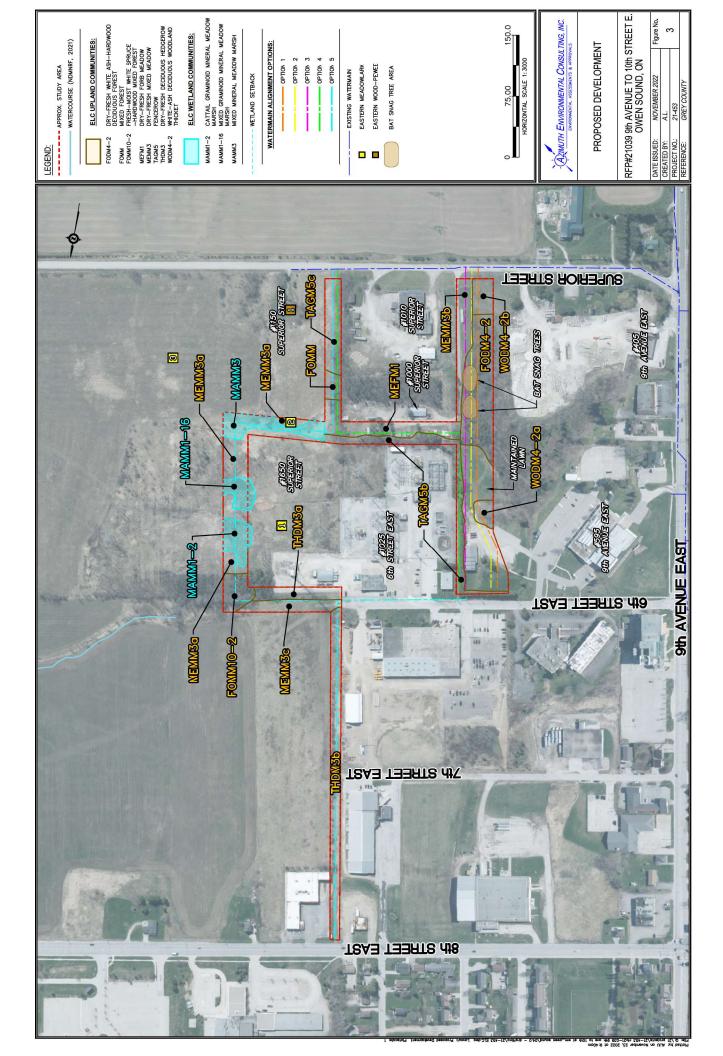


Table 1: Species at Risk Habitat Summary

Table 1. Species at Misk Manual Sum	isk manuat Summ	lat y			
Common Name	Species Name	ESA	SARA	Key Habitats Used By Species	Initial Assessment
Bald Eagle	Haliaeetus leucocephalus	SC	No status	Nests are typically found near the shoreline of lakes or large rivers, often on forested islands (Cadman et al., 2007). ESA Protection: N/A	Study area not near shorelines of lakes or large rivers, or forested islands. Species not observed during surveys.
Barn Swallow	Hirundo rustica	THR	THR	Ledges and walls of man-made structures such as buildings, barns, boathouses, garages, culverts and bridges. Also nest in caves, holes, crevices and cliff ledges (COSEWIC, 2011a). ESA Protection: Species and general habitat protection	No suitable o'd buildings, barns, box culverts, bridges erc. in the study area or on adjacent lands. Species not observed.
Black Ash	Fraxinus nigra	END	No status	Facultative wetland tree species frequently found in floodplain forests, swamps, seepage areas, shoreline margins and fens. Occupied sites are generally seasonally-flooded (COSEWIC, 2018). ESA Protection: Species and general habitat protection (ESA protections take effect January 27, 2024)	Key habitat requirements not found in the study area. Species not observed.
Віаск Тет	Chlidonias niger	SC	No status	Colonial nesters typically found within marshes. Its preferred nesting habitat is a hemi-marsh (i.e. a wetland with 50:50 open water and emergent vegetation). Nests are usually built on an upturned cattail root, floating vegetation mat or patch of mud (Cadman et al., 2007). ESA Protection: N/A	Small isolated patches of marsh habitat present in MAMM3 ELC ploygon, but not considered suitable for species (e.g. not hemi-marsh habitat). Species not found during surveys.
Bobolink	Dolichonyx oryzivorus	THR	THR	Nests primarity in forage crops (e.g. hayfields and pastures) dominated by a variety of species such as clover. Timothy, Kentucky Bluegrass, tall grass, and broadleaved plants. Also occurs in wet prairie, graminoid peatlands, and abandoned fields dominated by tall grasses. Does not generally occupy fields of row crops (e.g. corn, soybeans, wheat) or short-grass prairie. Sensitive to habitat size and has lower reproductive success in small habitat fragments (COSEWIC, 2010a). ESA Protection: Species and general habitat protection	NHIC records exist in 1km grid squares 17NK0634 and 17NK0635 (Appendix B). Potentially Ssuitable habitat for species present in study area in MEMM3 ELC polygon, but species was not observed in study area or on adjacent lands. Not considered further in our assessment.
Butternut	Juglans cinerea	END	END	Commonly found in riparian habitats, but is also found in rich, moist, well-drained loams, and well-drained gravels. Butternut is intolerant of shade (COSEWIC, 2003a). ESA Protection: Species and general habitat protection	Species not observed.
Chimney Swift	Chaetura pelagica	THR	THR	Nests primarily in chimneys though some populations (i.e. in rural northern areas) may nest in cavity trees (COSEWIC, 2007a). Recent changes in chimney design may be a significant factor in recent declines in numbers (Cadman et al., 2007). ESA Protection: Species and general habitat protection	NHIC records exist in 1km grid squares 17NK0535 (Appendix B) but species was not observed in study area or on adjacent lands during field program. Not considered further in our assessment.

Table 1 (AEC21-453)

Table 1: Species at Risk Habitat Summary

Common Name	Species Name	ESA	SARA	Key Habitats Used By Species'	Initial Assessment
Eastern Meadowlark Sturnella magna	Surnella magna	THR	THR	Most common in grassland, pastures, savannahs, as well as anthropogenic grassland habitats, including hayfields, weedy meadows, young orchards, golf courses, restored surface mines, etc. Occasionally nest in row crop fields such as corn and sobban, but there are considered low-quality habitat. Large tracs of grassland are preferred over smaller fragments and the minimum area required is estimated at 5ha (COSEWIC, 2011b). ESA Protection: Species and general habitat protection	NHIC records exist in 1km grid squares 17NK0533, 17NK0534, 17NK0635 17NK0635 and 17NK0635 (Appendix B). Suitable habitat present in study area and species was observed. Considered further in main text.
Eastern Prairie Fringed-orchid	Platanthera leucophaea	END	END	It is a species primarily of mesic prairies, fens and old fields (COSEWIC, 2003b). ESA Protection: Species and regulated habitat protection	Species not observed.
Eastern Small-footed Myotis	Myotis leibii	END	END	Generally occurs in mountainous or rocky regions as well as in buildings, on the face of rock bluffs and beneath slabs of rock and stones. Hibemation is typically confined to caves and old mines (Best and Jennings, 1997). ESA Protection: Species and general habitat protection	Key roosting habitat requirements not found. Hibernation habitat not present.
Eastern Ribbonsnake	Thannophis saurius	SC	SC	Found in wetland habitats with both flowing and standing water such as marshes, bogs, fens, ponds, lake shorelines and wet meadows. Most sightings occur near the water's edge (COSEWIC, 2012a). ESA Protection: N/A	Habitat requirements not met in study area. Wetland areas present are small and do not have flowing and standing water.
Eastern Wood-pewee Contopus virens	Contopus virens	SC	SC	Mostly in mature and intermediate-age deciduous and mixed forests having an open understory. It is often associated with forests dominated by Sugar Maple and oak. Usually associated with forest clearings and edges within the vicinity of its nest (COSEWIC, 2012d). ESA Protection: N/A	Habitat generally not present in study area, but species detected at one location adjacent. Considered further in main text.
Hart's-tongue Fern	Asplenium scolopendrium vat. americanum	SC	SC	Grows on calcareous rocks in deep shade on slopes in deciduous forest. Most occurrences are in maple-beech forest (MECP, 2022). ESA Protection: N/A	Suitable habitat for species not present and species not observed.
Henslow's Sparrow	Anmodramus henslowii	END	END	Requires grassland habitat and occurs more frequently and at higher densities in large patches of suitable habitat. Nests in tallgrass prairie, wet meadow, and marsh habitats as well as agricultural grasslands, lightly grazed pasture and grasslands on reclaimed surface mines (COSEWIC, 2011c). ESA Protection: Species and general habitat protection	Grassland habitat of suitable size for species not present in study area. Species not observed.
King Rail	Rallus elegans	END	END	Wide variety of freshwater marsh habitat types with cattails. Large marshes, especially those that contain a range of water level conditions and a mosaic of habitats, are preferred (COSEWIC, 2011d). ESA Protection: Species and general habitat protection	Suitable habitat for species not present and species not observed.

Table 1 (AEC21-453)

Table 1: Species at Risk Habitat Summary

hyotis lucifigus END END Lanius lucifigus END END Lanius END END Lanius END END Sistrarus THR SC motacilla THR SC plexippus SC Sc flotthyomyzon SC SC flotthyomyzon SC	Common Name Spec	Species Name	ESA	SARA	Key Habitats Used By Species'	Initial Assessment
Myotis lucifugus END END Lanius ludovicianus END (mirgrans subspecies) Parkesia THR SC Sistrurus THR THR Danaus SC Plekthyomyzon SC SC Schiptus SC SC Schiptus SC SC Sc Sc Sc Sc Sc Sc Sc Sc		ychus exilis	THR	THR	Breed strictly in marshes of emergents (usually cattails) that have relatively stable water levels and interspersed areas of open water (COSEWIC, 2009a). ESA Protection: Species and general habitat protection	Suitable habitat for species not present and species not observed.
Lanius END (mirgrans subspecies) Parkesia THR SC Sistrurus THR THR Saturus Sec Sc plexippus SC SC formation SC SC formation SC SC	wn Myotis Myoti	is lucifugus	END	END	Forests and regularly aging human structures as maternity roost sites. Regularly associated with attics of older buildings and barns for summer maternity roost colonies. Overwintering sites are characteristically mines or caves (MNRF, 2014) (COSEWIC, 2013a). ESA Protection: Species and general habitat protection	Key habitat requirements for the species, including potential candidate trees with suitable bat snag features, occur in FODM4-2 ELC polygon in the study area. Species has potential to occur. Considered further in main text.
Parkesia THR SC motacilla Sistrurus catenatus Danaus Pexippus SC SC Ichthyomyzon SC		anius ovicianus	END	END (mirgrans subspecies)	Breeding habitat characterized by open areas dominated by grasses and/or forbs, interspersed with scattered shrubs or small trees and bare ground. Suitable habitat includes pasture, old fields, prairie, savannah, pinyon-juniper woodland, shrub-steppe and alvar (COSEWIC, 2014). ESA Protection: Species and general habitat protection	Some open habitat present in study area and on adjacent lands, but scattered shrubs/small trees generally absent. Species not observed.
Sistrarus THR THR Catenatus Danaus plexippus Ichthyomyzon SC		arkesia otacilla	THR	SC	Occupies specialized habitat, showing a strong preferences for nesting and wintering along relatively pristine headwater streams and wetlands situated in large tracts of mature forest. Prefers running water, but also inhabits heavily wooded swamps and vernal or senti-permanent pools (COSEWIC, 2015).	Suitable habitat for species not present and species not observed.
Danaus SC SC Plexippus Ichthyomyzon SC		istrurus itenatus	THR	THR	In Georgian Bay, Massasaugas use bedrock barrens, conifer swamps, beaver meadows, fens, bogs, and shoreline habitats. On the upper Bruce Peninsula, forested habitats are used during hibernation and open, wetland, and edge habitat with canopy closure <50% in mid-late summer (COSEWIC, 2012b). ESA Protection: Species and general habitat protection	Study area over 2km from Georgian Bay. Suitable habitat not present in study area.
Ichthyomyzon SC SC		Sanaus exippus	SC	SC SC	Breeding habitat is confined to sites where milkweeds, the sole food of caterpillars, grow. Milkweeds grow in a variety of environments, including meedows in farmlands, along roadsides and in ditches, open wetlands, dry sandy areas, short and tall grass prairie, river banks, irrigation ditches, arid valleys, and south-facing hills (COSEWIC, 2010b). ESA Protection: N/A	Common Milkweed present in the study area but species not observed. Considered further in main text.
		hyomyzon bossor	SC	SC	Inhabits clear, coolwater streams. Adults are found in fast flowing riffles comprised of rock or gravel (MECP, 2022). ESA Protection: N/A	NHIC records exist in 1km grid squares 17NK0533, 17NK0534, 17NK0535, 17NK0635 and 17NK0635 (Appendix B). Watercourses not present in study area. Not considered further in our assessment.
Northern Myotis Northern Myotis Monthern Myotis END END END END END END END EN	and the second	Myotis mtrionalis	END	END	Maternity roost sites are generally located within deciduous and mixed forests and focused in snags including loose bark and cavities of trees. Overwintering sites are characteristically mines or caves (COSEWIC, 2013a). ESA Protection: Species and general habitat protection	Key habitat requirements for the species, including potential candidate trees with suitable bat snag features, occur in FODM4-2 ELC polygon in the study area. Species has potential to occur. Considered further in main text.

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Table 1: Species at Risk Habitat Summary

Species not observed.	(COSEWIC, 2002a). ESA Protection: N/A	sc		SC
Key habitat requirements for the species, including potential candidate trees with suitable bat snag features, occur in FODM4.2 ELC polygon in the study area. Species has potential to occur. Considered further in main text.	Maternity roost sites include forests and modified landscapes (barns or human-made structures). Overwintering sites include mines and caves (COSEWIC, 2013a). ESA Protection: Species and general habitat protection	Mate huma (COS	Mater huma (COS END ESA	
NHIC records exist in 1km grid squares 17NK0533 and 17NK0633 (Appendix B), but habitat not present in study area. MAMM wetlands unsuitable due to lack of standing water, basking/foraging function. Not considered further in our assessment.	Habitat is characterized by slow-moving water with a soft mud bottom and dense aquatic vegetation. Often located in ponds, sloughs, shallow bays or river edges and slow streams, or areas combining several of these wetland habitats (COSEWIC, 2008a). ESA Protection: N/A	Habitat is and dens bays or ri these wet ESA Pro	Habitat is and dens bays or in SC these wet ESA Pro	
No watercourses in study area.	Found in pools and slow-flowing sections of relatively smail, clear headwater streams with both pool and riffle habitats and an moderate to high gradient. These streams typically flow through meadows, pasture (COSEWIC, 2007c). ESA Protection: Species and regulated habitat protection.	Found in headwate high grac or shrub (COSEW	Found in headwatt headwatt headwatt high grad high grad or shrub (COSEW (COSEW ESA Pro	
No suitable habitat present in study area or on adjacent lands. Species not observed.	Most nest on cliff ledges or crevices, but some will use tall buildings or bridges near good foraging areas. Nests are typically close to bodies of water (COSEWIC, 2007b). ESA Protection: N/A	120	Most nest SC or bridges of water ((anatum/tund rius) ESA Prote	120
Initial Assessment	Key Habitats Used By Species		SARA	ESA SARA

Habitat as outlined within the MNRF's Species at Risk in Ontario website files (https://www.ontario.ca/environment-and-energy/species-risk-ontario-list), or Species Specific COSEWIC Reports referenced in this document. Species at Risk in Ontario List (June 13, 2017)

Best, T., and J. Jennings. 1997. Mammalian Species, Myotis leibii. The American Society of Mammalogists. No. 547, pp. 1-6, 5 figs. Cadman, M., D. Sutherland, G. Beck, D. Lepage and A. Couturier. 2007. Atlas of the Breeding Birds of Ontario 2001-2005. Bird Studies

COSEWIC, 2002a. COSEWIC assessment and update status report on the Tuberous Indian-plantain Annoglossum plantagineum in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vi + 11 pp. COSEWIC 2003a. COSEWIC assessment and status report on the Butternut Juglans cinerea in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii + 32 pp.

COSEWIC, 2003b. COSEWIC assessment and update status report on the Eastern Prairie Fringed-orchid Platanthera leucophaea in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vi + 27 pp. COSEWIC, 2007a. COSEWIC assessment and update status report on the Chimney Swift Chaetura pelagic a in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii + 49 pp.

COSEWIC. 2007b. COSEWIC assessment and status report on the Peregrine Falcon Falco peregrinus (pealei subspecies - Falco peregrinus and pealei anatum/sundrius - Falco peregrinus

COSEWIC, 2007c. COSEWIC assessment and update status report on the Redside Dace Clinostomus elongates in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii + 59 pp. anatum/tundrius) in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii +45 pp.

COSEWIC, 2010a. COSEWIC assessment and update status report on the Bobolink Dolichonyx oryzivorus in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa vi + 42 pp. COSEWIC. 2008a. COSEWIC assessment and status report on the Snapping Turtle Chelydra serpentina in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii + 47 pp. COSEWIC, 2009a. COSEWIC assessment and update status report on the Least Bittern Ixobrychus exilis in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vi + 36 pp.

COSEWIC, 2011a. COSEWIC assessment and update status report on the Barn Swallow Hirundo rustica in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. ix +37 pp. COSEWIC, 2010b. COSEWIC assessment and status report on the Monarch Danaus plexippus in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. vii + 43 pp.

COSEWIC. 2011c. COSEWIC assessment and update status report on the Henslow's Sparrow Ammodramus henslowii in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. x + 37 pp. COSEWIC, 2011b. COSEWIC assessment and update status report on the Eastern Meadowlark Starmella magna in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. x + 40 pp.

COSEWIC, 2011d. COSEWIC assessment and update status report on the King Rail Relius elegan s in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. x + 32 pp. COSEWIC, 2012a COSEWIC assessment and status report on the Eastern Ribbonsnake Thamnophis sauritus in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. xii + 39 pp. COSEWIC, 2012b. COSEWIC assessment and update status report on the Massasauga Sistrurus catenatus in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. xiii + 84 pp. COSEWIC. 2013a. COSEWIC assessment and update status report on the Little Brown Myotis Myotis Incifigus, Northern Myotis Myotis Agrits septentrionalis and Tri-colored Bat Perinyotis subfathws in COSEWIC, 2014. COSEWIC assessment and update status report on the Loggerhead Shrike Lanius Iudovicianus ssp. and the Prairie subspecies Lanius Iudovicianus excubitorides in Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. xiii + 51 pp.

Canada. Committee on the Status of Endangered Wildlife in Canada. Ottawa. xxiv + 93 pp.

Table 1 (AEC21-453) Page 4 of 5

Table 1: Species at Risk Habitat Summary

Table 1: Species at Ki	ISK Habitat Summ	lary			
Common Name	Species Name	ESA	SARA	Key Habitats Used By Species¹	Initial Assessment
COSEWIC, 2015, COS	SEWIC assessment	t and status repor	t on the Louisia	na Waterthrush Parkesia motacilla in Canada. Committee on the Status	of Endangered Wildlife in Canada. Ottawa. xi + 58 pp.

COSEWIC. 2018. COSEWIC assessment and status report on the Black Ash *Praxinus rigra* in Canada. Committee on the Satus of Endangered Wildlife in Canada. Ottawa. xii + 95 pp. Ministry of the Environment, Conservation and Parks (MECP). 2022. Species at Risk in Ontario (https://www.ontario.ca/page/species-risk-ontario)
Ministry of Natural Resources and Forestry (MNRF). 2014. Eastern Small-footed Bat. Queen's Printer for Ontario. https://www.ontario.ca/environment-and-energy/eastern-small-footed-bat

Table 1 (AEC21-453)

Sound Class EA Table 2a: Vascular Plant Species List. Ower

	rank as randam rank proces and offer young class and	Surveyor: Adam McCleffand	ŀ			1	١			l	l	l	l	l	l	l	ŀ			l
	3						Ve	Vegetation Communities ²	ioi	Com		ities ²						Con	Conservation Rankings ³	=
${ m FAMILY}^1$	SCIENTIFIC NAME ¹	COMMON NAME ¹	MEMM38	2-IMMAM	EMMAM	TAGMSa	FOMM10-2	ТНРМЗА ТНРМЗЬ	THINKS	FODM4-2	MODM4-2a	WODM4-2b		MEKMI MEMM3P		FOMM	TAGMSe	СВУИК	SBVNK	TRACK
Aceraceae	Acer negundo	Manitoba Maple	×			×		X	ļ	×		 ×			×	X		5	S5	Z
Aceraceae	Acer platanoides	Norway Maple				×	-			×			····		×		G	GNR	SE5	Z
Aceraceae	Acer saccharum	Sugar Maple				×					×			×			X G5	2	\$5	Z
Anacardiaceae	Rhus typhina	Staghorn Sumac	X			 	-	ļ		×		ļ		×		····	G5	5	\$5	Z
Anacardiaceae	Toxicodendron radicans var. radicans	Eastern Poison Ivy	×			×											Ö	G5T5	S5	Z
Apiaceae	Anthriscus sylvestris	Wild Chervil	×			••••				×				×	×		5	GNR	SE4?	Z
Apiaceae	Daucus carota	Wild Carrot	×				×	X	×	×	×	X	×	×	×	X	X	GNR	SE5	Z
Apocynaceae	Asclepias syriaca	Common Milkweed	X					X			×		ļ	ļ			G5	5	S5	Z
Apocynaceae	Vinca minor	Lesser Periwinkle					×	×	}	×							X	GNR	SE5	Z
Asteraceae	Achillea millefolium	Common Yarrow	×							×								2	SE5?	z
Asteraceae	Ambrosia ariemisiyona	Common Burdook]	Þ	>					<		`	<		G Z	CN C	CEC	2 2
Asteraceae	Contained incea	Proun Knapused	>	×		< ≻	۲.	·}	 >	>	 >	` `	< >				_	GNP	SES	2
Asteraceae	Cichorium intybus	Wild Chicory	1			; ×	+	: ×		····					: ×	+	_	GNR	SES	Z
Asteraceae	Cirsium arvense	Canada Thistle				:	†	·.	1	ļ	-		×			†		5	SE5	Z
Asteraceae	Cirsium vulgare	Bull Thistle				·····	×	ļ	ļ			×				×		GNR	SE5	Z
Asteraceae	Erigeron annuus	Annual Fleabane								X	×			X	×		X G5	5	S5	Z
Asteraceae	Erigeron canadensis	Canada Horseweed	X						×						×		X G5	5	S5	Z
Asteraceae	Erigeron philadelphicus	Philadelphia Fleabare	×														G5	5	S5	Ы
Asteraceae	Euthamia graminifolia	Grass-leaved Goldenrod			×												G5	5	S5	Z
Asteraceae	Eutrochium maculatum var. maculatum	Spotted Joe Pye Weed		×									∤				Ö	GSTS	S5	z
Asteraceae	Lapsana communis	Common Nipplewort				×	×			×							5	GNR	SE5	z
Asteraceae	Leucanthemum vulgare	Oxeye Daisy	×									••••			×			GNR	SE5	Z
Asteraceae	Solidago canadensis var. canadensis	Canada Goldenrod	X		×	×						•••••			×		X	GSTS	S5	Z
Asteraceae	Solidago gigantea var. gigantea	Giant Goldenrod	×				-	×		×			×	×		-	3 0	GST5	SS	z
Asteraceae	Sonchus arvensis ssp. arvensis	Glandular Sow-thistle	×						×	∤-	×	×	∤-		×	>		GNRTNRSES	SES	Z
Asteraceae	Symphyoti tenum tenengotum sen Jenese	Healt-leaved Aster	>		>	>	>		>	< >			>			< >	CO V	CSTS	25	2 0
Asteraceae	Symphysia triam tancestaiam 55p. tancesta Eastell Falleted Aster	Calico Acter	<	1	<		۱ ×	1	∤	١			;-	+	+	۲		21.5	25	
Asteraceae	Symphyotrichum novae-angliae	New England Aster			×	×	:	X	×			×	×				GS	2	S5	Z
Asteraceae	Symphyotrichum sp.	an Aster					 					·	•••••	×		 	Ż	(A	N/A	N/A
Asteraceae	Tanacetum vulgare	Common Tansy		ļ		····		ļ	}	ļ	ļ	ļ		×	ļ		G	GNR	SE5	Z
Asteraceae	Tragopogon pratensis	Meadow Goatsbeard	X										X	X			G	GNR	SE5	Z.
Asteraceae	Tussilago farfara	Coltsfoot		X	X	Х				X	X	X		X	X	X	G	GNR	SE5	Z
Brassicaceae	Alliaria petiolata	Garlic Mustard				×									X		X	GNR	SE5	Z
Brassicaceae	Erysimum cheiranthoides	Wormseed Wallflower										X	••••				G5	2	S5?	Z
Brassicaceae	Hesperis matronalis	Dame's Rocket							X			X		X	X		Ğ	G4G5	SE5	Z
Brassicaceae	Lepidium campestre	Field Peppergrass				····	٠								×		G	GNR	SE5	Z.
Brassicaceae	Thlaspi arvense	Field Pennycress										X					G	GNR	SE5	Z
Caprifoliaceae	Lonicera sp.	a Honeysuckle				·····	·		{					{		X	Ż	N/A	N/A	N/A
Caprifoliaceae	Lonicera tatarica	Tatarian Honeysuckle					×			×	×	×	×			×	X	GNR	SE5	Z
Caprifoliaceae	Viburnum lentago	Nannyberry	×														Ö	2	S5	Z
Caprifoliaceae	Viburnum opulus	Cranberry Viburnum	×			····}·	×		×	×				×		×	GS	2	SS	z
Caprifoliaceae	Viburnum rafinesqueanum	Downy Arrowwood				×											Ü	GS	SS	Z.
Caryophyllaceae	Saponaria officinalis	Bouncing-bet	-									••••		×			5	NK	SES	Z

Page 1 of 4 Table 2a (21-453)

							Vege	tation	Vegetation Communities ²	nmu	ities ²						Conservation Rankings ³	ES3
FAMILY ¹	SCIENTIFIC NAME ¹	COMMON NAME ¹	MEMM38	2-IMMAM	MAMM3	FOMM10-2	тнрмза	ТНРМЗР	FODM4-2	WODM4-2a	MODW4-7P LVCW2P	MEMM3P	MEEMI	FOMM	TAGMSc	CBVNK	211110	SBANK
Caryophyllaceae	Silene vulgaris	Bladder Campion		ļ	ļ	ļ				ļ	^	ζ	X		ļ	GNR	SE5	Z
Chenopodiaceae	Chenopodium album	Common Lamb's-quarters			ļ						X					GS	SES	
Convolvulaceae	Convolvulus arvensis	Field Bindweed				ļ						×		ļ		GNR	SE5	Z
Cornaceae	Comus alternifolia	Alternate-leaved Dogwood			ļ				×		×			×		G5	SS	Z
Cornaceae	Comus racemosa	Grey Dogwood	×		ļ										ļ	GS	SS	
Cornaceae	Comus sericea	Red-osier Dogwood	×	×	×	X	×	×		×	×		×	×		G5	SS	
Cupressaceae	Thuja occidentalis	Eastern White Cedar	×			×		ļ	×		×		ļ	ļ	ļ	G5	S5	Z.
Cyperaceae	Carex lasiocarpa	Woolly-fruit Sedge			ļ	ļ	ļ	ļ	····	×		ļ	ļ	ļ	ļ	G5	S5	Z
Cyperaceae	Carex retrorsa	Retrorse Sedge		×		ļ								ļ		G5	SS	
Cyperaceae	Carex stipata	Awl-fruited Sedge		×	ļ	ļ	ļ	ļ			ļ	ļ	ļ	ļ	ļ	G5	SS	Z
Cyperaceae	Carex viridula	Greenish Sedge		X												G5	SS	
Cyperaceae	Carex vulpinoidea	Fox Sedge	×	×				×								G5	SS	Z.
Cyperaceae	Scirpus atrovirens	Dark-green Bulrush	×	×	ļ	ļ				×				ļ		G5	SS	Z
Cyperaceae	Scirpus microcarpus	Red-tinged Bulrush		×												G5	SS	Z.
Equisetaceae	Equisetum arvense	Field Horsetail	×	×	X	X			×	×	×		×	×		G5	SS	
Euphorbiaceae	Euphorbia esula	Leafy Spurge									×					GNRT	GNRTNR SE	
Fabaceae	Lathyrus latifolius	Everlasting Pea	×				×									GNR	SE4	
Fabaceae	Lotus corniculatus	Garden Bird's-foot Trefoil	×				×	×		×	×	×			×	GNR	SE5	
Fabaceae	Medicago lupulina	Black Medick	×		-	}					 ×					GNR	SE5	
Fabaceae	Melilotus albus	White Sweet-clover	×				×	×				×	×		×	GS	SES	
Fabaceae	Robinia pseudoacacia	Black Locust											∤-		×	GS	SES	
Fabaceae	Trifolium pratense	Red Clover	×									×	×			GNR	SES	
rabaceae	Trifolium repens	white Clover			+							∤-	∤-			GNK	SES	
Fabaceae	Vicia cracca	Tufted Vetch	×	×			×	×	×			×				GNR	SES	
Fagaceae	Quercus rubra	Northern Red Oak														3 3	S	
Geraniaceae	Geranum robertianum	Herb-Kobert				ļ	ļ		× >			}		< >	×	3	25	Z . Z
Giossulaitaceae	Nibes cynospan	ri di Filoniy Goosebelly	>		- -				۲					۲.		6	00	7 7
Indaceae	Tris versicolor	Harleduin Blue Flag	< >	+	- -			Ţ.	>							3 5	52	7 7
Jugiandaceae	Jugians nigra	Black wainut	<		۷ ۵				<			<			ļ	3	34.	Z 2
Juncaceae	Juncus brevicaudatus	Short-tailed Kush		× ;	× .	-										3	S	Z Z
Juncaceae	Juncus canadensis	Canada Kush		< :												3 3	S	
Juncaceae	Juncus effusus	Soft Kush	;	< ;												3	20	Ζ,
Juncaceae	Juncus tenuts	Path Kush	×	×	+				;							GNK	S	Z
Lamiaceae	Clmopodum vulgare ssp. vulgare	Wild Basil		;	-	×		;	×	;	<u> </u>	× .				CICS	S	
Lamiaceae	Prunella vulgaris ssp. vulgaris	Common Self-heal		×				×	×	×				×		GSTU	SE3	
Liliaceae	Asparagus officinalis	Garden Asparagus	×													G5?	SES	
Liliaceae	Convallaria majalis	European Lily-of-the-valley				×			×			×				G5	SE5	Z
Liliaceae	Hemerocallis fulva	Orange Daylily													×	GNA	SE5	
Liliaceae	Maianthemum stellatum	Star-flowered False Solomon's Seal													×	G5	SS	
Lythraceae	Lythrum salicaria	Purple Loosestrife	×	×												G5	SE5	
Malvaceae	Malva moschata	Musk Mallow				×										GNR	SE5	
Oleaceae	Fraxinus americana	White Ash	×		×	X	×	×	×	×	×	X	×	×	×	G4	S ₄	
Oleaceae	Fraxinus pennsylvanica	Red Ash	×		×											G4	S	
Oleaceae	Syringa vulgaris	Common Lilac							×	••••	X					GNR	SE	Z
			•	ĺ	Ì	l							I	I	ļ			

Page 2 of 4 Table 2a (21-453)

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			ŀ			V	refati			Vegetation Communities ²	2'S					Conse	Conservation Rankings ³	_
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	_			ŀ		۲.		٥ ا	 	ĺ		ŀ	ŀ	ŀ	+			l.
FAMILY ¹	SCIENTIFIC NAME ¹	COMMON NAME ¹	MEMM38	EMMAM	TAGMSa	FOMM10-2	вемант тнрмзь	FODM4-2	MODW4-2a	TAGMSb	MODW4-3P	WEMM3P	EOMM MEEMI	TAGMSe		СВУИК	SKANK	TRACK
Onagraceae	Epilobium parviflorum	Small-flowered Hairy Willowherb		X		ļ		ļ			ļ	ļ		ļ	II .		SE4	Z
Onagraceae	Oenothera biennis	Common Evening-printrose		 .			X		X	X			X	^			35	Z
Pinaceae	Abies balsamea	Balsam Fir		ļ		×	×	ļ					ļ	^	X G5		S5	Z
Pinaceae	Picea glauca	White Spruce		ļ	×		×	ļ		×				ļ	GS		SS	Z
Pinaceae	Pinus resinosa	Red Pine		ļ		ļ	×	ļ			ļ	ļ	ļ	ļ	GS		S5	z
Pinaceae	Pinus sylvestris var. sylvestris	Scots Pine	×	×	×	ļ	ļ	×		×			×	×	S	GNRTNR SE5	E5	Z
Plantaginaceae	Plantago lanceolata	English Plantain		ļ		<u> </u>	ļ	ļ	×	×		×		<u> </u>	G5		SE5	z
Plantaginaceae	Plantago major	Common Plantain		ļ				ļ	×	×		X	×	ļ	G5		SE5	Z
Poaceae	Agrostis stolonifera	Creeping Bentgrass									••••	×			GS		SE5	Z
Poaceae	Andropogon gerardi	Big Bluestem		X											GS		S4	Z
Poaceae	Bromus inermis	Smooth Brome	X		Χ		XX	7	X	X	X	X		X	G5T5		SE5	Z
Poaceae	Dactylis glomerata	Orchard Grass	×			×			×	×	•••••		×		X GNR		E5	Z
Poaceae	Elymus repens	Quackgrass	X							×					GNR		SE5	Z
Poaceae	Leersia oryzoides	Rice Cutgrass										•••••		X	GS	2,000,000	S5	Z
Poaceae	Lolium arundinaceum	Tall Ryegrass	×				XX					×	×	^	X GNR		SE5	Z
Poaceae	Panicum capillare	Common Panicgrass											X		G5		S5	Z
Poaceae	Phalaris arundinacea	Reed Canarygrass		X	×		X	<u> </u>		X	••••	×		X	GS		S5	Z
Poaceae	Phleum pratense	Common Timothy	×	×			×				×	×			GNR		SE5	Z
Poaceae	Phragmites australis ssp. australis	European Reed	X	X											G5T5	2022.0340	SE5	Z
Poaceae	Setaria pumila	Yellow Foxtail								X					GNR	0.03000	SE5	Z
Polygonaceae	Reynoutria japonica	Japanese Knotweed			×									^	X GNR		SE5	Z.
Polygonaceae	Rumex crispus	Curled Dock	×				×			×		×	×	^		0022558	SE5	z
Polygonaceae	Rumex obtusifolius	Bitter Dock												×	GNR	~	SE5	Z
Ranunculaceae	Anemonastrum canadense	Canada Anemone							••••		••••				X G5		S5	Z
Ranunculaceae	Ranunculus acris	Common Buttercup	×	X	×	×		×	×	×		×	×	×	S	0000	SE5	z
Rhamnaceae	Frangula alnus	Glossy Buckthorn				}	}	∤	∤					∤			SE5	z
Rhamnaceae	Rhamnus cathartica	European Buckthorn	×		×	×		X	×		×				X GNR		SE5	Z
Rosaceae	Crataegus coccinea var. coccinea	Scarlet Hawthorn		_	1		X	∤	∤					×	G5		S4	z
Rosaceae	Fragaria virginiana	Wild Strawberry	×		×			×	×	×	×		-	×	GS		55	Z
Rosaceae	Geum aleppicum	Yellow Avens			×			×						×	GS		SS	z
Rosaceae	Malus pumila	Common Apple					×								S		SE4	Z.
Rosaceae	Potentilla anserina ssp. anserina	Common Silverweed							[×		×			GSTS		SS	Z.
Rosaceae	Potentilla norvegica	Rough Cinquefoil		_				_					×	-			S5	z
Rosaceae	Potentilla recta	Sulphur Cinquefoil	×								••••	•••		^	X		SE5	z
Rosaceae	Prunus avium	Sweet Cherry										×			GN		SE4	Z
Rosaceae	Prunus pensylvanica	Pin Cherry			×		×	×					×		G5		S5	Z
Rosaceae	Prunus serotina	Black Cherry						×							GS		35	Z
Rosaceae	Prunus virginiana	Chokecherry			X	X		X		X				X	GS	0.000000	35	Z
Rosaceae	Rosa acicularis	Prickly Rose		ļ				ļ		X					GS		S5	Z
Rosaceae	Rosa multiflora	Multiflora Rose		ļ			×	ļ		×					GNR		SE5	z
Rosaceae	Rubus idaeus ssp. idaeus	European Red Raspberry	X		X			X				X			GSTS		SE1	Z
Rosaceae	Rubus occidentalis	Black Raspberry						×				×			X G5		SS	Z
Rosaceae	Sorbus aucuparia	European Mountain-ash			×										GS		SE4	z
Rubiaceae	Galium mollugo	Smooth Bedstraw					×		[GNR		SE5	Z.
Rubiaceae	Galium palustre	Common Marsh Bedstraw	×	×			×]						S		55	Z.

Page 3 of 4 Table 2a (21-453)

Table 2a: Vascular Plant Species List, Owen Sound Class EA

Surveyor: Adam McClelland

					Vege	Vegetation Communities	Comm	unities					Conservation Rankings ³	ion s ³
FAMILY ¹	SCIENTIFIC NAME ¹	COMMON NAME ¹	MEMM38	MAMM3 TAGM58	FOMM10-2 THDM3a	ТНРМЗЬ	MODW4-2a FODW4-2	MODW4-3P LYCM2P	МЕМИЗР МОБИН-70	MEEMI	EOMM	TAGMSe	SBVAK	TRACK
Salicaceae	Populus balsamifera	Balsam Poplar		X		X						GS	S2	Z
Salicaceae	Populus tremuloides	Trembling Aspen	×					X		×		GS	SS	Z.
Salicaceae	Salix bebbiana	Bebb's Willow					X					G5	S5	Z
Salicaceae	Salix discolor	Pussy Willow	X	X								G5	S5	Z
Salicaceae	Salix interior	Sandbar Willow						X				G5	S2	N
Scrophulariaceae	Verbascum thapsus	Common Mullein			ļ					×		GNR		Z
Solanaceae	Solanum dulcamara	Bittersweet Nightshade		X							×	GNR		Z
Tiliaceae	Tilia americana	Basswood		X				X		X	X	G5	S5	N
Typhaceae	Typha angustifolia	Narrow-leaved Cattail	X	XX		×						G5	SE5	Z
Typhaceae	Typha latifolia	Broad-leaved Cattail		X								G5	S5	Z
Ulmaceae	Ulmus americana	White Elm	X	XX	X	X	XX		X	X	X	X G4	S2	N
Vitaceae	Parthenocissus quinquefolia	Virginia Creeper					×	×			×	X G5	S4?	Z.
Vitaceae	Parthenocissus vitacea	Thicket Creeper				×	×					G5	S5	Z
Vitaceae	Vitis riparia	Riverbank Grape	XX		XX	XXXX	X	X	$X \mid X$	XXX		X G5	SS	Z
						ĺ				Ì				

¹ Nomenclature based on Ministry of Natural Resources and Forestry (MNRF) Natural Heritage Information Centre (NHIC, 2022)
² ELC Codes based on Ecological Land Classification for Southern Ontario manual (Lee et al., 1998, 2008)
³ Conservation Rankings: From Ontario Ministry of Natural Resources and Forestry, Natural Heritage Information Centre (https://www.ontario.ca/page/natural-heritage-information-centre)

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Surveyor: Adam McClelland

Conservation Rankings³

Vegetation Communities²

¹ Nomenclature based on Ministry of Natural Resources and Forestry (MNRF) Natural Heritage Information Centre (NHIC, 2022)

$\mathbf{FAMIL}\mathbf{Y}^1$	SCIENTIFIC NAME ¹	${ m COMMON~NAME}^1$	91-1MMAM	МЕММЗС	CBYNK	SKVNK	TRACK
Apiaceae	Daucus carota	Wild Carrot		X	GNR	SE5	Z
Asteraceae	Ambrosia artemisiifolia	Common Ragweed		×	G5	S5	Z
Asteraceae	Centaurea jacea	Brown Knapweed		X	GNR	SE5	Z
Asteraceae	Euthamia graminifolia	Grass-leaved Goldenrod	X		G5	S5	Z
Asteraceae	Solidago canadensis var. canadensis	Canada Goldenrod		X	G5T5	S5	Z
Cornaceae	Cornus sericea	Red-osier Dogwood	X		G5	S5	Z
Cyperaceae	Carex vulpinoidea	Fox Sedge	X		G5	S5	Z
Cyperaceae	Scirpus atrovirens	Dark-green Bulrush	X		G5	S5	Z
Fabaceae	Vicia cracca	Tufted Vetch	X		GNR	SE5	Z
Juncaceae	Juncus canadensis	Canada Rush	X		G5	S5	Z
Juncaceae	Juncus tenuis	Path Rush	X		GNR	S5	Z
Lamiaceae	Mentha canadensis	Canada Mint	X		G5	S5	Z
Lamiaceae	Prunella vulgaris ssp. vulgaris	Common Self-heal	X		G5TU	SE3	Z
Oleaceae	Fraxinus pennsylvanica	Red Ash	X		G4	S4	Z
Onagraceae	Epilobium parviflorum	Small-flowered Hairy Willowherb	X		GNR	SE4	Z
Plantaginaceae	Plantago major	Common Plantain		X	G5	SE5	Z
Poaceae	Glyceria striata var. striata	Fowl Mannagrass	X		G5T5	S5	Z
Poaceae	Lolium arundinaceum	Tall Ryegrass	X		GNR	SE5	Z
Poaceae	Phalaris arundinacea	Reed Canarygrass	X	X	G5	S5	Z
Poaceae	Phleum pratense	Common Timothy	X	X	GNR	SE5	Z
Polygonaceae	Rumex crispus	Curled Dock	X		GNR	SE5	Z
Typhaceae	Typha angustifolia	Narrow-leaved Cattail	×		G5	SE5	Z

 $^{^2}$ ELC Codes based on Ecological Land Classification for Southern Ontario manual (Lee et al., 1998, 2008)

³ Conservation Rankings: From Ministry of Natural Resources and Forestry, Natural Heritage Information Centre (https://www.ontario.ca/page/natural-heritage-information-centre)

Table 3: Ecological Land Classification, Owen Sound Class EA, 2022

	Ecolog	Ecological Land Classification	ation		
System	Community Class	Community Series	Ecosite/Vegetation Type	Canopy/Shrub Layer	Ground Cover
Terrestrial	Meadow	MEM, Mixed Meadow	MEMM3a, Dry-Fresh Mixed Meadow	Tree cover was sparse, and included White Elm, Green Ash, and Scots Pine. Scattered shrub cover included Dogwood species and Common Buckthom.	Vegetation was deminated by grass and forb species, including Reed Canary Grass, Brown Knapweed and Wild Carrot.
Wetland	Marsh	MAM, Meadow Marsh	MAMM1-2, Cattail Graminoid Mineral Meadow Marsh	Shrub cover was sparse, and consisted of Red Osier Degwood and Pussy Willow.	The community was dominated by cattails. Graminoid and forb species observed included sedges, rushes, Dark Green Bultush, and Purple Loosestrife.
Wetland	Marsh	MAM, Meadow Marsh	MAMM3, Mixed Meadow Marsh	Shrub cover consisted of Red Osier Dogwood. Sparse tree cover included Green Ash and Scots Pine.	Abundant graminoid and forb cover included Reed Canary Grass, Asters, Grass-leaved Goldenrod, Narrow-leaved Cattail and Common Reed.
Terrestrial	Cultural	TAG, Treed Agriculture	TAGM5a, Fencerow	Tres species observed included White Ash, Green Ash, Pin Cherry and Scots Pine. Shrub cover included Common Buckthorn, Red Osier Dogwood and Pussy Willow.	The ground cover consisted of grass and forb species, including Reed Canary Grass, Yellow Avens, Asters, Canada Goldenrod and Colsfoot.
Terrestrial	Forest	FOM, Mixed Forest	FOMM10-2, Fresh- Moist White Spruce- Hardwood Mixed Forest	Tres species observed included White Ash, White Elm, White Cedar, and White Sprace. Shrub species observed included Red Osier Dogwood, Cranberry Viburnum and Common Buckthorn.	The ground cover was dominated by forb species, including Eastern Panicled Aster, Calico Aster and Wild Basil. A large patch of Lesser Periwinkle and European Lily-of-the-valley was observed.
Terrestrial	Cultural	THD, Deciduous Thicket	THDM3a, Dry-Fresh Deciduous Hedgerow Thicket	Tree and shrub cover was dominated by Commno Buckthorn, Hawthorn, Red Osier Dogwood and White Ash.	The ground cover consisted of grass and forb species. Common species observed included Brown Knapweed, Timothy, Orchard Grass, Goldenrod, and Wild Madder.
Terrestrial	Cultural	THD, Deciduous Thicket	THDM3b, Dry-Fresh Deciduous Hedgerow Thicket	Shrub cover was dominated by Common Buckthorn: Hawthorn and Red Osier Dogwood were also present. Scattered White Ash and White Elm were observed.	The ground cover consisted of grass and forh species Common species observed included Brown Knapweed, Reed Canary Grass, Orchard Grass, Goldenrod, and New England Aster.
Terrestrial	Forest	FOD, DeciduousForest	FODM4-2, Dry-Fresh White Ash-Hardwood Deciduous Forest	The canopy was dominated by White Ash; Sugar Maple, Scots Pine, White Elm, Norway Maple and Black Cherry were also observed. Shurb cover was sparse in some areas and consisted of Lilac, Alternate-leaved Dogwood, Thicket Creeper Riverbank Grape and Common Buckthom.	The ground cover consisted primarily of forb species, including Goldemods, Asters, Periwinkle, Herb-robert and Coltsfoot.
Terrestrial	Woodland	WOD, Deciduous Woodland	WODM4-2a, White Ash Deciduous Woodland	The canopy was open and consisted of White Ash. Shub species observed included Red Osier Dogwood, Riverbank Grape, Thicket Creeper, Common Buckthorn and Bebb's Willow.	The ground cover consisted of graminoid and forb species, including Goldemod, Brown Knapweed, Smooth Brome, Dark-green Bulrush and Wild Carrot.
Terrestrial	Cultural	TAG, Treed Agriculture	TAGM5b, Fencerow	The fencerow was dominated by White Cedar; other specie present included Trembling Aspen, Red Oak. White Spruce and White Ash. Shrub cover was sparse in some areas and included Red Osier Dogwood, Thicket Creeper and Rose species.	The ground cover consisted of forb and grass species, including Goldemods, Asters, Bird's-foot Trefoil, Brown Knapweed, Quackgrass, Reed Canary Grass and Smoth Brome.
Terrestrial	Woodland		WODM4-2b, White Ash Deciduous Woodland	WOD, Deciduous WODM4-2b, White Ash White Bim was also observed. Shrub cover was sparse Woodland in some areas and included Common Buckthorn, Tatarian Honeysuckle and Riverbank Grape	The ground cover consisted of grass and forb species. Common species observed included Reed Canary Grass, Smooth Brome, Timothy, Tufted Vetch, Goldenrods, Asters, and Wild Carrot.

Table 3 (AEC21-453) Page 1 of 3

Table 3: Ecological Land Classification, Owen Sound Class EA, 2022

The community was dominated by a variety of grass and forb species, including Smooth Brome, Tall Ryegrass, Timothy, Reed Canary Grass, Brown Knapweed, Goldenrod, and Bird's-foot Trefoil.	The community was dominated by a variety of forb species, including Brown Knapweed, Wild Carrot, Annual Fleabane, Bird's-foot Trefoil, Chicory and White Sweet-clover	The ground cover consisted of a variety of grass and forb species, including Orchard Grass, Smooth Brome, Field Horsetail, Asters, Yellow Avens, Buttercup, Reed Canary Grass and Colisfoot.	The ground cover consisted of a variety of grass and forb species, including Orchard Grass, Tall Ryegrass, Goldenrod, Asters, Chicory, Wild Carrot, White Sweet-clover and Periwinkle.	The community was dominated by graminoid species, including Dark-green Bultrush, Narrow-leaved Cattail, sedges, rushes, and Tall Ryegrass. Forb species observed included Grass-leaved Goldenrod, Canada Mint and Willowherb.	The ground cover was dense and dominated by forb and grass species, including Brown Knapweed, Reed Canary Grass, Canada Go'demod and Wild Carrot.
Tree cover consisted of a treerow along the laneway; White Ash, Scots Pine, Sweet Cherry and Black Walnut were observed. Shrub cover consisted of several patches of Raspberry and Riverbank Grape.	Tree species observed included White Ash, Scots Pine, Norway Maple, White Elin and American Basswood. Sparse shrub cover included Riverbank Grape and Red Osier Dogwood	The canopy was dominated by Scots Pine and White Ash. Shrub cover consisted of Common Buckthom, Red Osier Dogwood, Tatarian Honeysuckle and Glossy Buckthorn.	Tree species observed included Sugar Maple, White Ash, White Elm, and Black Locust. Shrub cover consisted of Riverbank Grape, Thicket Creeper, Common Buckthorn, Tatarian Honeysuckle and a patch of Japanese Knotweed.	Tree and shrub cover was very sparse and included Red Osier Dogwood and young Green Ash.	No trees or shrubs were observed.
MEMM3b, Dry-Fresh Mixed Meadow	MEFMI, Dry-Fresh Forb Meadow	FOMM, Mixed Forest	TAGM5c, Fencerow	MAMM1-16, Mixed Graminoid Mineral Meadow Marsh	MEMM3c, Dry-Fresh Mixed Meadow
MEM, Mixed Meadow	MEF, Forb Meadow	FOM, Mixed Forest	TAG, Treed Agriculture	MAM, Meadow Marsh	MEM, Mixed Meadow
Meadow	Meadow	Forest	Cultural	Marsh	Meadow
Terrestrial	Terrestrial	Terrestrial	Terrestrial	Wetland	Terrestrial

Table 3 (AEC21-453) Page 2 of 3

Table 4: Dawn Breeding Birds Survey, Owen Sound Class EA, 2022

AEC21-453

							T	Location 1,2	2)	onservatio	Conservation Rankings ³	gs3		
														nt						
FAMILY	SCIENTIFIC NAME	COMMON NAME	\downarrow			П	۳,	\neg	4		5		T	Lands Inci	Incidental G	GRANK S	SRANK	ESA	SARA	TRACK
			Visit 1	Visit 2	Visit 1	Visit 2	Visit 1 Visit 2	t 2 Visit	1 Visit 2	Visit 1	Visit 2	Visit 1	Visit 2							
Accipitridae	Buteo jamaicensis	Red-tailed Hawk			C											GS	S5			Z
Bombycillidae	Bombycilla cedrorum	Cedar Waxwing		S		S		S	S			à	S			G5	S5			Z
Cardinalidae	Cardinalis cardinalis	Northern Cardinal		S			S	S		S						G5	S5			Z
Cardinalidae	Passerina cyanea	Indigo Bunting					S									G5	S5B			Z
Cathartidae	Cathartes aura	Turkey Vulture	F/O											VIS			S5B,S3N			Z
Charadriidae	Charadrius vociferus	Killdeer		S		S	S							S		GS	S4B			Z
Columbidae	Zenaida macroura	Mourning Dove							S	VIS	VIS					GS	S5			Z
Corvidae	Corvus brachyrhynchos	American Crow	C					C	C, VIS	S	C		C			G5	S5			Z
Corvidae	Cyanocitta cristata	Blue Jay								C			C			GS	S5			Z
Fringillidae	Spinus tristis	American Goldfinch	S	C, S	S,C	S	S	ပ	S	S, C		C				G5	S5			Z
Icteridae	Agelaius phoeniceus	Red-winged Blackbird	Ü	S, C	Ü	C, S	C, S C	ပ		C, VIS	Ü	C	C			GS	S5			Z
Icteridae	Molothrus ater	Brown-headed Cowbird						S	S		S					GS	S5			Z
Icteridae	Quiscalus quiscula	Common Grackle										Ü				GS	S5			Z
Icteridae	Sturnella magna	Eastern Meadowlark			S	S, C	S S									GS	S4B,S3N	THR	THR	Y
Laridae	Larus argentatus	Gull sp.				C								C		GS	S4B,S5N			Z
Mimidae	Dumetella carolinensis	Gray Cathird					S								>		S5B,S3N			Z
Parulidae	Geothlypis trichas	Common Yellowthroat	S			S	S S					C	S, C			GS	S5B,S3N			Z
Parulidae	Seiurus aurocapilla	Ovenbird												S		G5	S5B			Z
Parulidae	Setophaga petechia	Yellow Warbler			S		S										S5B			Z
Parulidae	Setophaga pinus	Pine Warbler						S	S								S5B,S3N			Z
Parulidae	Setophaga raticilla	American Redstart			S		S		S							G5	S5B			Z
Passerellidae	Melospiza melodia	Song Sparrow	S	S	S	S (C S, C	S	S	S	S		S, C			G5	S5			Z
Passerellidae	Spizella passerina	Chipping Sparrow		S		S										2000	S5B,S3N			Z
Passerellidae	Spizella pusilla	Field Sparrow			S												S4B,S3N			Z
Phasianidae	Meleagris gallopavo	Wild Turkey	VIS								C					G5	S5			Z
Picidae	Dryocopus pileatus	Pileated Woodpecker					C									G5	S5			Z
Sturnidae	Sturnus vulgaris	European Starling	S	S	S	S	S	S		S						GS	SNA			Z
Troglodytidae	Troglodytes aedon	House Wren									S					G5	S5B			Z
Turdidae	Turdus migratorius	American Robin	S	C	S	S, C	S, C S	S	S	S	S		C, S	S		G5	S5			Z
Tyrannidae	Contopus virens	Eastern Wood-pewee										S		S		GS	S4B	SC	SC	Y
Tyrannidae	Empidonax traillii	Willow Flycatcher				S										G5	S4B			Z
Tyrannidae	Sayornis phoebe	Eastern Phoebe	S					_								GS	S5B			Z
Tyrannidae	Tyrannus tyrannus	Eastern Kingbird			S		S									GS	S4B			Z
Vireonidae	Vireo gilvus	Warbling Vireo			S	S	S					S				G5	S5B			Z
Vireonidae	Vireo olivaceus	Red-eyed Vireo				S			S		S					G5	S5B			Z
Visit 1. Inne 2	2022 Observer S Tarof Ten	Vicit 1. line 2 2022 Observer S Tarof Tempurature 13% Cloud Cover 10% Wind: R3	00% Wi	-	orinitation	" No rain	Precipitation: No rain Survey Time 08:44 to 08:49: Visit 2: Inne 15 2022	P 08.44 to	. 08.49. Vi	sit ?. Inn	COC 519	Observer		S Tarof Tempurature 16°C	2091 0					

Visit I. June 2, 2022, Observer: S. Tarof, Tempurature 13°C, Cloud Cover 10%, Wind: B3, Precipitation: No rain, Survey Time 08:44 to 08:49; Visit 2: June 15, 2022, Observer: S. Tarof, Tempurature 16°C,

Cloud Cover 5%, Wind: B2, Precipitation: No rain, Survey Time 08:49 to 08:54

Table 4 (AEC21-453)

Page 1 of 1

² Breeding Bird Evidence Codes: XN · Species observed or heard, C · Call heard, FO · Flyover (Species presence); H · Species observed in its breeding season in suitable nesting habitat, S · Singing male (Possible Breeding); P · Pair cbserved, T · Territorial behaviour, A · Agitated behaviour or anxiety calls of adult, V · Visiting a probably nest site, N · Nest building or excavation of nest hole (Probable Breeding); DD · Distraction display or injury feigning, NU · Used Nest or egg shells, FY · Recently fledged young, AE · Adult leaving or entering nest sites, FS · Adult carrying fecal sac, CF · Adult carrying food for young, NE · Nest containing eggs, NY · Nest with young seen or heard (Confirmed Breeding).

S-Rank = Sub-national/provincial scale (from 1-5), S1 - Extremely Rare, S2 - Very Rare, S3 - Rare to Uncommon, S4 - Common, S5 - Very Common, E - Exotic G-Rank = Global scale (from 1 - "Critically Imperiled" to 5 - "Secure" or common), G1 - Critically Imperiled, G2 - Imperiled, G3 - Vulnerable, G4 - Apparently Secure, G5 - Secure. B = Breeding Populations, N = Non-breeding Populations; M = Migratory Populations; SARO: EXT - Extirpated, END - Endangered, THR - Threatened, SC - Special Concern. Track (Is the species tracked provincially?) = Y - Yes, N = No, P = Partial NA - Not Applicable (i.e. not native to Ontario), Blank - Not at Risk in Ontario. ³ Conservation Rankings: From Ontario Ministry of Natural Resources, Natural Heritage Information Centre (http://nhic.mnr.gov.on.ca/nhic_.cfm)



APPENDICES

Appendix A: Municipal and Regional Background Information and

Correspondence

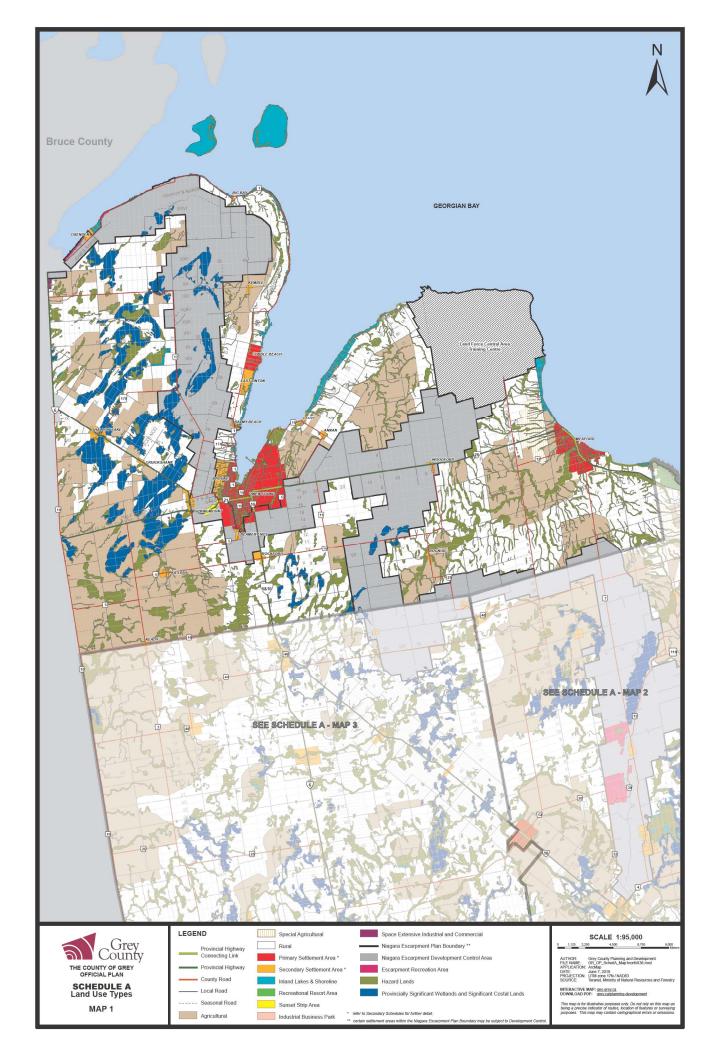
Appendix B: Provincial Background Mapping

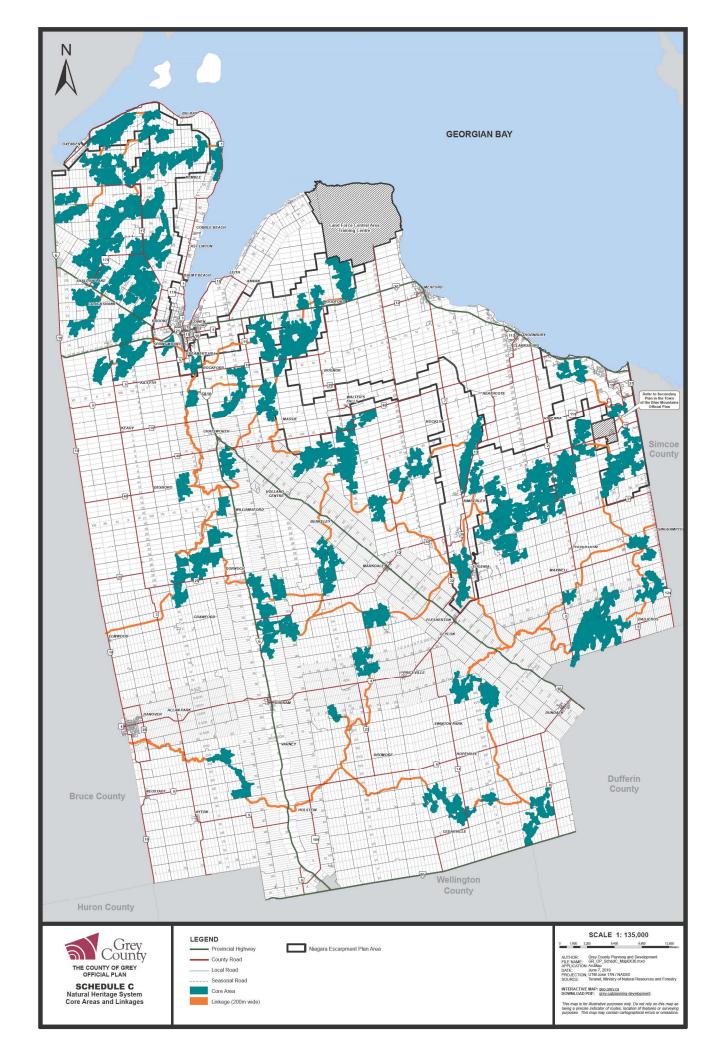
Appendix C: Photographic Record

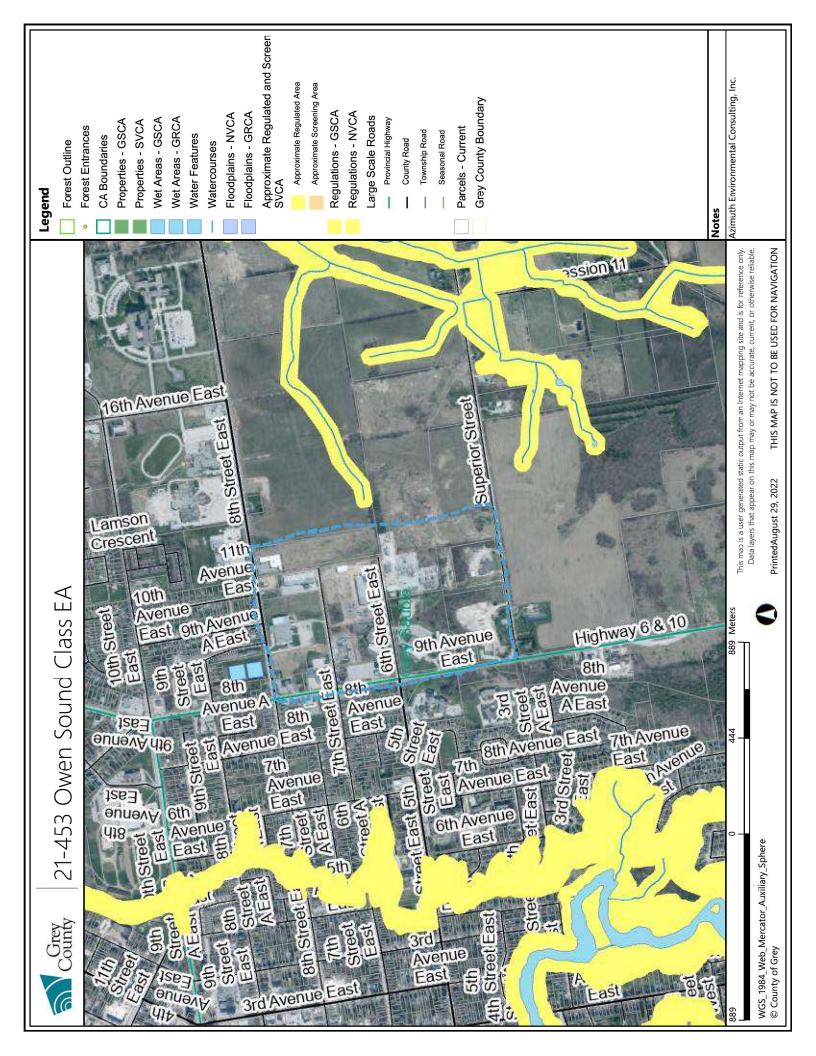


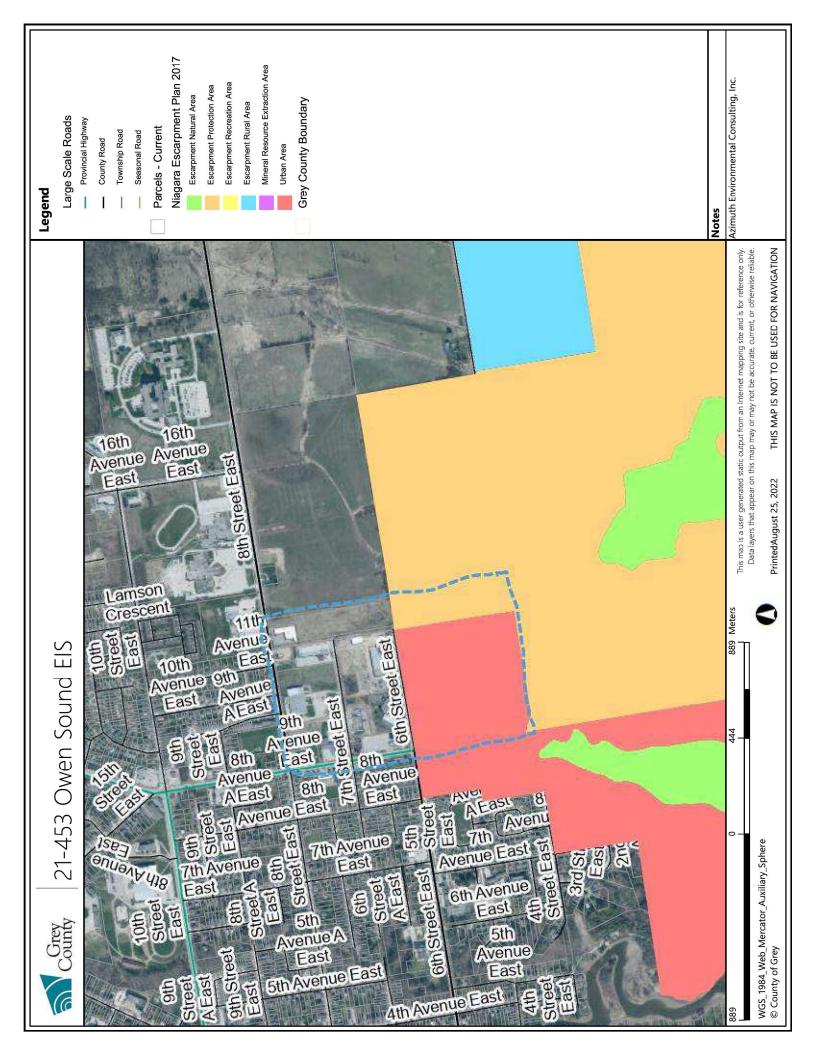
APPENDIX A

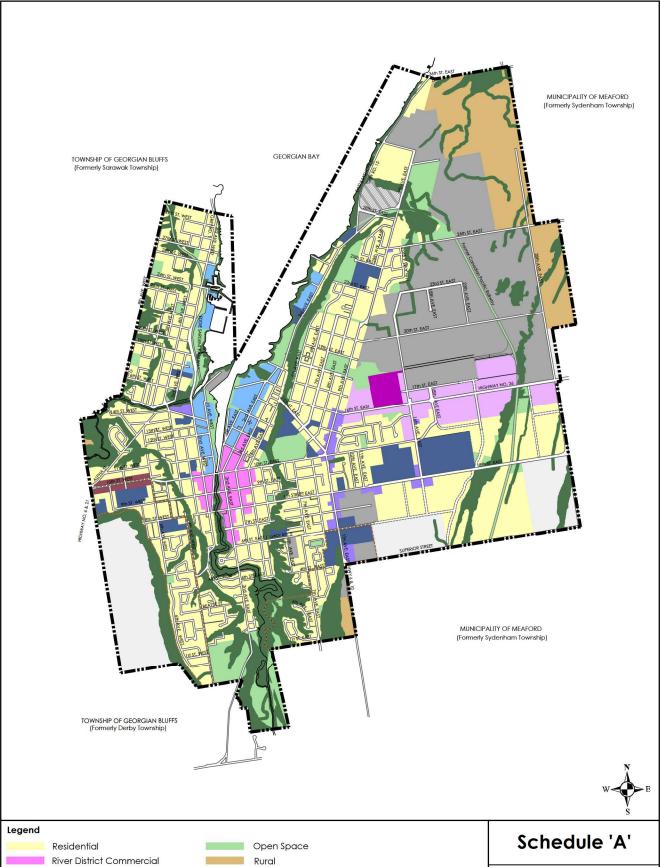
Municipal and Regional Background Information and Correspondence











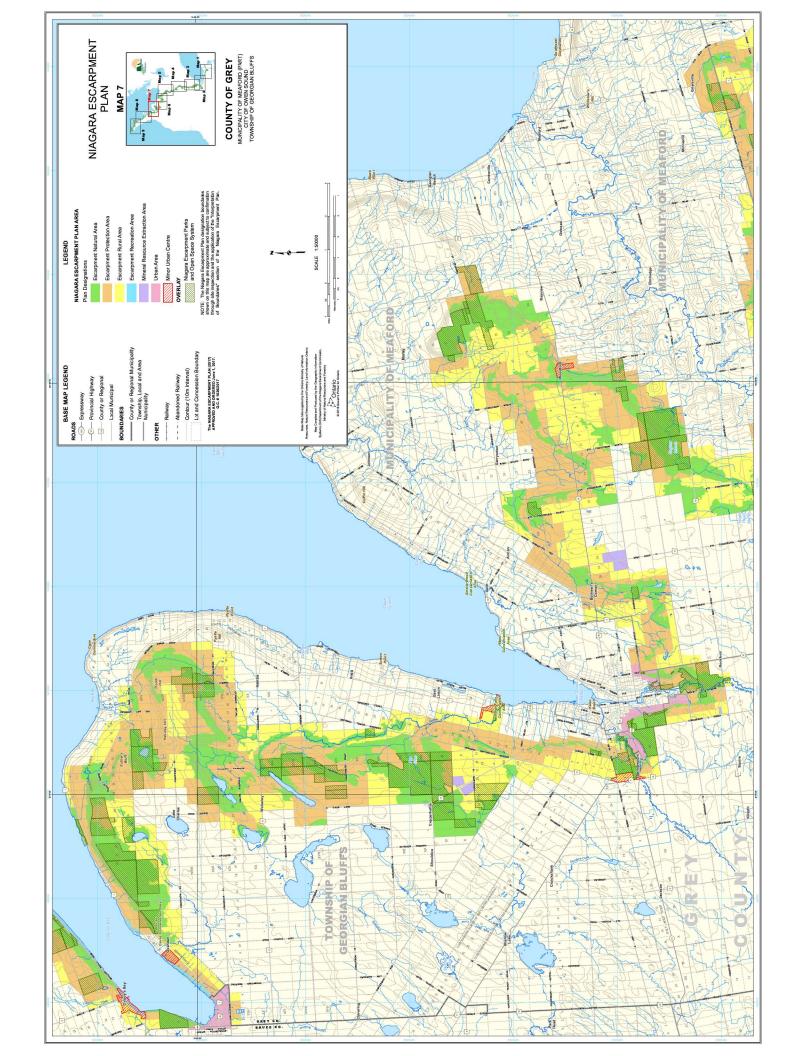


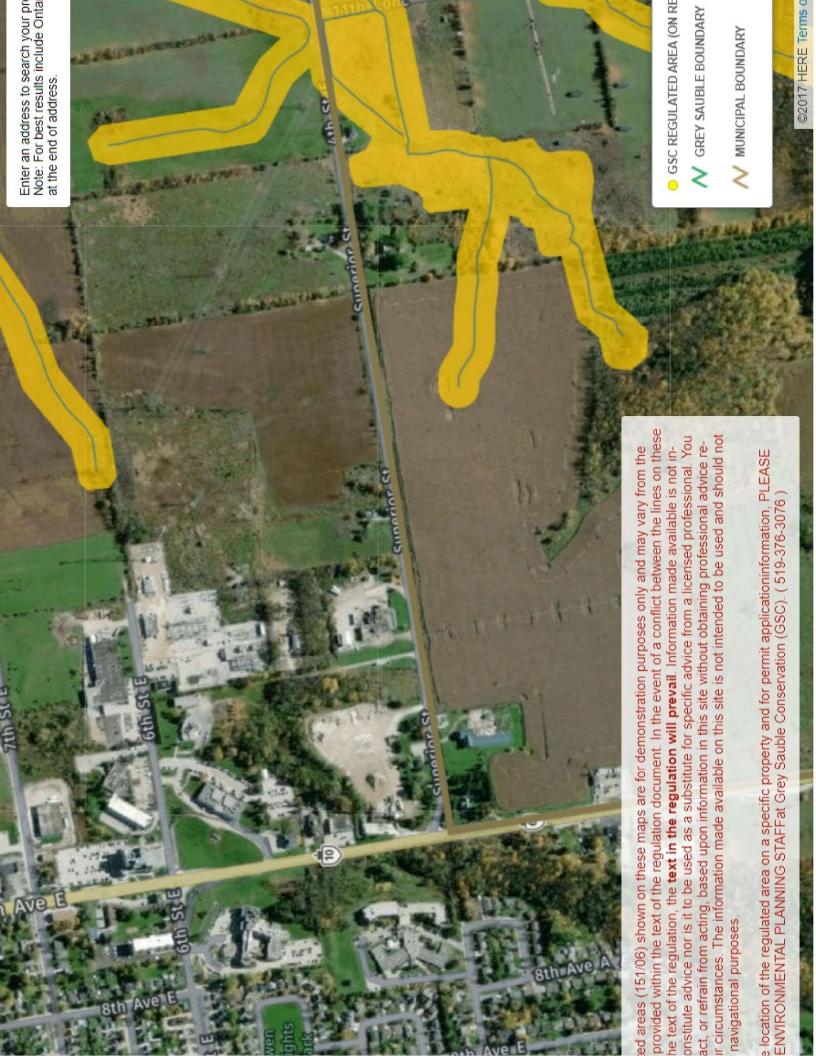


Official Plan
City of Owen Sound
Land Use Plan



May 2021 1:28,000

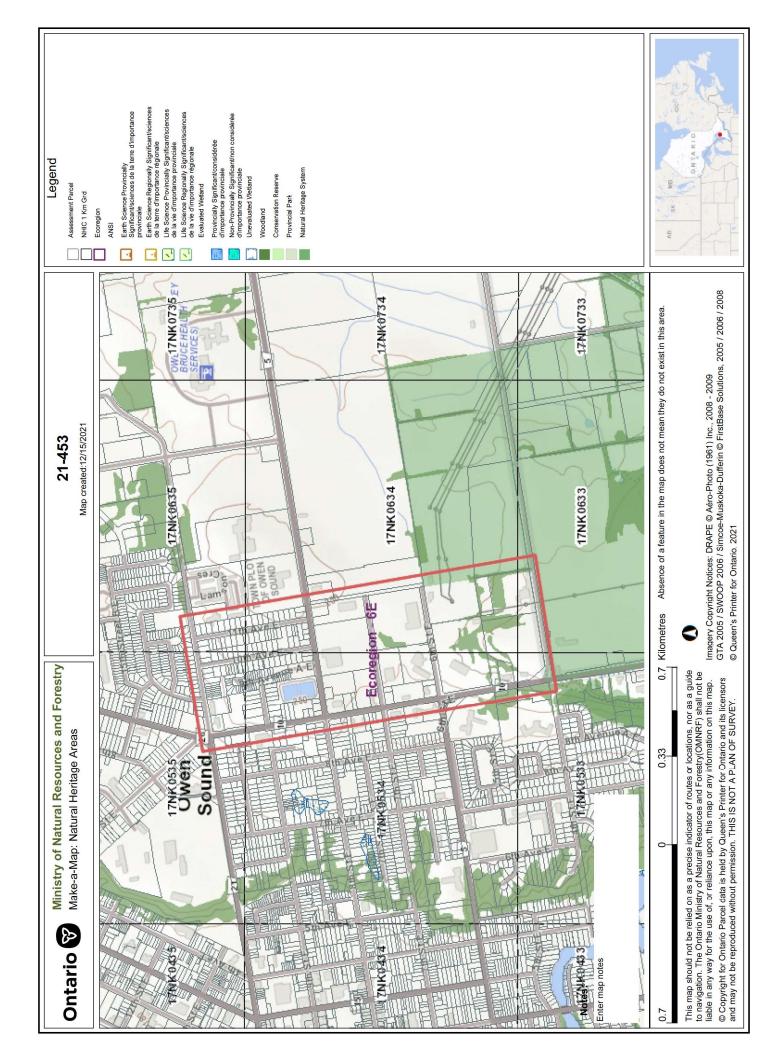






APPENDIX B

Provincial Background Mapping



NHIC Data

To work further with this data select the content and copy it into your own word or excel documents.

OGF ID	Element Type	Common Name	Scientific Name	SRank	SARO Status	COSEWIC Status	ATLAS NAD83 IDENT	COMMENTS
905289	SPECIES	Northern Brook Lamprey	Ichthyomyzon fossor		SC	SC	17NK0535	
905289	SPECIES	Chimney Swift	Chaetura pelagica		THR	THR	17NK0535	
905289	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0535	
905299	SPECIES	Northern Brook Lamprey	Ichthyomyzon fossor		SC	SC	17NK0635	
905299	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0635	
905299	SPECIES	Bobolink	Dolichonyx oryzivorus		THR	THR	17NK0635	
905288	NATURAL AREA	Niagara Escarpment Biosphere Reserve					17NK0534	
905288	SPECIES	Rusty-patched Bumble Bee	Bombus affinis		END	END	17NK0534	
905288	SPECIES	Hart's-tongue Fern	Asplenium scolopendrium				17NK0534	
905288	SPECIES	Midland Painted Turtle	Chrysemys picta marginata			SC	17NK0534	
905288	SPECIES	Northern Brook Lamprey	Ichthyomyzon fossor		SC	SC	17NK0534	
905288	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0534	
905287	NATURAL AREA	Niagara Escarpment Biosphere Reserve					17NK0533	
905287	SPECIES	Hart's-tongue Fern	Asplenium scolopendrium				17NK0533	
905287	SPECIES	Midland Painted Turtle	Chrysemys picta marginata			SC	17NK0533	
905287	SPECIES	Northern Brook Lamprey	Ichthyomyzon fossor		SC	SC	17NK0533	
905287	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0533	
905287	SPECIES	Butternut	Juglans cinerea		END	END	17NK0533	
905287	SPECIES	Snapping Turtle	Chelydra serpentina		SC	SC	17NK0533	

OGF ID	Element Type	Common Name	Scientific Name	SRank	SARO Status	COSEWIC Status	ATLAS NAD83 IDENT	COMMENTS
905298	NATURAL AREA	Niagara Escarpment Biosphere Reserve					17NK0634	
905298	SPECIES	Northern Brook Lamprey	Ichthyomyzon fossor		SC	SC	17NK0634	
905298	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0634	
905298	SPECIES	Bobolink	Dolichonyx oryzivorus		THR	THR	17NK0634	
905297		Niagara Escarpment Biosphere Reserve					17NK0633	
905297	SPECIES	Hart's-tongue Fern	Asplenium scolopendrium				17NK0633	
905297	SPECIES	Eastern Meadowlark	Sturnella magna		THR	THR	17NK0633	
905297	SPECIES	Snapping Turtle	Chelydra serpentina		SC	SC	17NK0633	







APPENDIX C

Photographic Record



Photograph 1. THDM3 ELC community in hydro corridor north of 1025 6th Street East (in detection area of Dawn Breeding Bird Point Count Station #1), facing west (June 10, 2022).



Photograph 2. TAGM5 ELC community/hedgerow between 1025 6th Street East and 595 9th Avenue East, facing east (June 10, 2022).



Photograph 3. FODM4-2 ELC community immediately west of 1000 Superior Street near Dawn Breeding Bird Point Count Station #4, facing south (June 10, 2022).



Photograph 4. MEMM3 ELC community along driveway immediately west of 1010 Superior Street (in detection area of Dawn Breeding Bird Point Count Station #5), facing north/northwest) (June 10, 2022).



Photograph 5. MEFM1 ELC community at 1000 Superior Street (in detection area of Dawn Breeding Bird Point Count Station #3), facing east (June 10, 2022).



Photograph 6. MEMM3 ELC community immediately east of 1025 6th Street East, (in detection area of Dawn Breeding Bird Point Count Station #2) facing east (June 10, 2022).



Photograph 7. MAMM1-2 ELC community east of 1025 6th Street East (in detection area of Dawn Breeding Bird Survey Point Count Station #2), with MEMM3 in background, facing east (June 10, 2022).



Photograph 8. FOMM ELC community immediately northeast of 1010 Superior Street (in detection area of Dawn Breeding Bird Point Count Station #3), facing west (June 10, 2022).

Appendix E: Geotechnical Investigation Report



Geotechnical Investigation

Proposed Watermain Replacement and Road Reconstruction

9th Avenue East, Owen Sound, Ontario

Submitted to:

Tatham Engineering Limited 115 Sanford Fleming Drive, Suite 200 Collingwood, Ontario, L9Y 5A6

Submitted by:

GEI Consultants Ltd. 647 Welham Road, Unit 14 Barrie, Ontario, L4N 0B7 www.canada.geiconsultants.com

March 24, 2023 Project No. 2201530

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1. Introduction

GEI Consultants (GEI) was retained by Tatham Engineering Limited, on behalf of the City of Owen Sound, to complete a subsurface investigation and provide a geotechnical report in support of the proposed watermain replacement and road reconstruction on 9th Avenue East, Owen Sound, Ontario. A site location plan is shown in Figure 1.

The City of Owen sound is proposing to replace the watermain water services on a section of 9th Avenue East in Owen Sound, Ontario from Superior Street to just north of 9th Street East approximately 1000 m in length. Some sections of sanitary and storm sewer may also be replaced along with all sanitary laterals. The current section of road is a four-lane road with curb and gutter and sidewalks. The road cross section will not change and the service trenches will be repaired after service installation (full road reconstruction is not required). It is understood that the inverts for the watermain would be about 2.0 m and inverts for the storm and sanitary sewer would be as deep as 3.5 m below the road grade.

Also, a looping watermain is part of the project. The alignment is about 1,350 m in length and extends from 8th Street East southerly to 6th Street East (through a Hydro One corridor), then west along 6th Street East for about 150 m, then south along private lands to Superior Street, then west along Superior Street to 9th Avenue East. then east to the dead end of 4th Street East. The watermain invert is about 2 m below existing grade.

Lastly, it is understood that the project will have several phases.

The purpose of this geotechnical investigation was to determine the subsurface conditions along the various alignments and provide a report with geotechnical engineering recommendations for the proposed service installations and pavement design for the road, along with general constructability recommendations.

An Assessment of Past Uses (APU) report and Soil Characterization report were also part of the scope of work and are completed under separate cover.

2. Procedures and Methodology

It is noted that all elevations in this report are metric/geodetic and expressed in meters (m). All measurements in this report are also in metric and expressed in millimetres (mm), metres (m) or kilometers (km).

The borehole locations were laid out in the field by GEI staff prior to commencement of drilling operations. The locations of underground utilities were co-ordinated with locating companies.

The drilling for the site was carried out between January 30 and February 3, 2023, and were drilled to 1.5 to 6.6 m depth (Elev. 227.0 and 264.2) along the various proposed alignments with some boreholes encountering auger refusal. Boreholes 1 to 12 were drilled on 9th Avenue East, Borehole 14 was east of 9th Avenue East near 4th Street East, Boreholes 15 to 17 and 19 to 25 drilled on the looping watermain alignment. It is noted that Boreholes 13, 18 and 26 could not be drilled due to access or permission to enter concerns.

Ground surface elevations of the boreholes and horizontal coordinates (referencing NAD 83 geodetic datum) were surveyed by GEI with a Topcon FC – 5000 GPS Survey unit. The elevations and coordinates are provided on the borehole logs in Appendix A. Borehole locations are shown on Figure 2.

Traffic control services for the project were provided by GEI. All traffic control set ups were executed in accordance with Ontario Traffic Manual – Book 7 Temporary Conditions (OTM Book 7).

Drilling and sampling of the boreholes was completed using truck mounted drilling equipment operated by a specialty drilling subcontractor retained and supervised by GEI. The boreholes were advanced to predetermined depths through the use of solid stem augers and sampling was conducted using a 51 mm O.D. Split Spoon (SS) sampler. Standard Penetration Test (SPT) "N" Values (N values) were recorded for the sampled intervals as the number of blows required to drive an SS sampler 305 mm into the soil using a 63.5 kg drop hammer falling 750 mm, in accordance with ASTM D1586. Soil sampling was conducted at 0.75 m intervals for the upper 3.0 m, and at 1.5 m intervals thereafter.

A monitoring well was installed in eleven (11) of the boreholes to facilitate the measurement of the stabilized groundwater level and for subsequent monitoring or testing purposes. The monitoring well installation was performed in accordance with Ontario Regulation (O.Reg.) 903. The boreholes without a well were backfilled in accordance with O.Reg. 903 and patched with cold mix asphalt, as required.

Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

The GEI field staff examined, and classified characteristics of the soils encountered in the boreholes, including the presence of fill materials, groundwater observations during and upon completion of the drilling, recorded observations of borehole advancement, and processed the recovered samples. All recovered soil samples were logged in the field, carefully packaged, and transported to the laboratory for more detailed examination and classification.

In the laboratory, the samples were classified as to their visual and textural characteristics. All samples were submitted for moisture content determination. Four (4) composite samples of pavement granular and seven (7) samples of the underlying strata were submitted for grain size analysis and two (2) samples were submitted for Atterberg limits testing. Laboratory testing results are provided in Figures B1 to B11 in Appendix B.

3. Subsurface Conditions

3.1 General Overview

Borehole locations are shown on Figure 2. Detailed soil profiles encountered in the boreholes are indicated on the attached borehole logs in Appendix A, with the results of geotechnical laboratory testing included in Appendix B.

It should be noted that the conditions indicated on the borehole logs are for specific locations only and can vary between and beyond the locations. It should be noted that the soil boundaries indicated on the borehole logs are inferred from non-continuous sampling and observations during drilling. These boundaries are intended to reflect approximate transition zones and should not be interpreted as exact planes of geological change.

In addition, the descriptions provided in the borehole logs are inferred from a variety of factors, including visual observations of the soil samples retrieved, laboratory testing, measurements prior to and after drilling, and the drilling process itself (speed of drilling, shaking/grinding of the augers, etc.). The passage of time also may result in changes in conditions interpreted to exist at locations where sampling was conducted.

3.2 Stratigraphy

3.2.1 Pavement Structure

Most boreholes were drilled through the various paved road surfaces, except Boreholes 14, 19, 20, 24 and 24. Component thicknesses are provided below.

Borehole	Asphalt (mm)	Granular Thickness (mm)	Total Thickness (mm)
1	220	120	340
2	220	580	800
3	260	500	760
4	150	650	800
5	300	360	660
6	130	290	420
7	120	200	320
8	150	450	600

Borehole	Asphalt (mm)	Granular Thickness (mm)	Total Thickness (mm)
9	170	590	760
10	100	660	760
11	120	650	770
12	160	600	760
15	90	520	610
16	210	400	610
17	100	660	760
21	125	625	750
22	100	660	760
23	125	-	

Distinction between granular base and subbase layers could not be determined.

Four (4) composite samples of granular material consisting of auger samples were submitted for sieve analysis and comparison to OPSS.MUNI 1010 standards for granular materials, with the results provided in Figure B1 to B8 in Appendix B. The samples analyzed did not satisfy gradation specifications for Granular A being finer on multiple sieves. The samples did not meet the specifications for Granular B Type I, due to excessive material passing the 75µm sieve (13 to 24% versus the 8% standard).

3.2.2 Topsoil

Boreholes 14, 19, 20, 24 and 25 encountered topsoil at the surface of the boreholes that was 75 to 100 mm in thickness.

3.2.3 Fill

A fill layer was encountered beneath the pavement structure and topsoil in all boreholes except 2,5, 8, 15 and 16 and was penetrated at 0.8 to 3.8 m depth (Elev. 231.4 to 261.2), locally extending to the 1.5 m depth of exploration in Boreholes 10 to 12 (Elev. 244.0 to 261.1). The fill consisted of silty sand in Boreholes 1, 3, 4, 6, 7, 10 and 12, sand and silt in Borehole 9 and sandy silt in Boreholes 14, 22 and 23. The sandy fill varied to clayey silt in Borehole 3 and 4 and sandy clayey silt in Borehole 7. In Boreholes 17, 19, 20, 21, 22, 24 and 25, fill consisted of clayey silt. Trace to some organics and rootlets were observed in Boreholes 14, 20, 23, 24, and 25. One (1) sample of the material was submitted for grain size analysis and the results are provided in Figure B9 in Appendix B. Atterberg Limits on the sample are shown in Figure 11



in Appendix B. The fill was moist, with moisture contents ranging from 5 to 22%. The fill had N values ranging from 3 to 49 blows, showing a loose to dense condition typically compact in cohesionless soil and soft to very stiff cohesive fill soil.

3.2.4 Sandy Silt

Underneath the topsoil and fill in Borehole 14 a local sandy silt layer (trace to some clay and trace gravel) was observed from 0.8 m to 2.3 m depth (Elev. 246.5 to 248.0). Beneath the pavement and fill in Borehole 21, another sandy silt layer was revealed from 1.5 to the 2.3 m depth of exploration (Elev. 243.0). The soil was moist to wet with moisture contents of 12 to 15. The material was loose with an N value of 7 in boreholes 21 and compact to dense in Borehole 14 with a N values of 26 and 31.

3.2.5 Glacial Till

A glacial till deposit was encountered in Boreholes 1 to 9, 14 to 17, 19 to 20 and 22 to 25 below the upper soil layers and extended below the 1.5 m to 6.6 m depth of exploration (Elev. 227.0 to 264.2). The till matrix was variable and predominantly consisted of sandy silt, sand and silt, silty sand and locally clayey silt and sandy clayey silt in Boreholes 7, 8, 19 and 20. Cobbles and boulders should be expected based on augers grinding during advancement of the boreholes. Six (6) samples of the material were submitted for grain size analysis and the results are provided in Figure B10 in Appendix B. Atterberg Limits on one sample are shown in Figure B11. The glacial till was brown to grey near the base, and was typically moist, with moisture contents ranging from 14 to 24%. N values were 7 to more than 50 blows, indicating a range of loose to very dense / stiff to hard conditions, but typically compact.

3.2.6 Auger Refusal

Auger refusals was observed in Boreholes 10, 11, 12, 15, 16, 17, 19 and 25 at depths noted below. An auger probe was advanced beside all theses boreholes to confirm the depth of refusal. The auger probes met with similar refusal depths. Auger refusal could have been due to the cobbles/boulders in the till and/or shallow bedrock common to the area. It is noted that the augers grinded at the borehole locations for several minutes and may have penetrated to some degree into the upper weathered bedrock. As such the, the depths noted below might be slightly lower than the top of the actual bedrock surface.

Borehole	Refusal Depth (m) / Elev.	Borehole	Refusal Depth (m) / Elev.
10	1.5/244.0	11	1.5/252.7
12	1.5/261.0	15	1.5/263.5
16	1.8/264.2	17	2.4/260.3

Borehole	Refusal Depth (m) / Elev.	Borehole	Refusal Depth (m) / Elev.
19	3.5/245.7	21	2.3/243.0
25	2.9/245.4		

3.3 Groundwater

Unstabilized groundwater level measurements and borehole sloughing (cave) measurements were taken upon completion of drilling of each borehole. These measurements were taken to provide an estimate of possible excavation and temporary groundwater control issues that may arise during construction. Eleven (11) boreholes were outfitted with a monitoring well with 50 mm diameter PVC pipe and 1.5 m long screens. Monitoring well configuration and groundwater observations are noted on the borehole logs in Appendix A.

A summary of the ground water level measurements is below:

Borehole	Depth of Cave (m) / Elev.	Unstabilized Groundwater Level Depth (m) / Elev.	Depth (m) / Elev. of Groundwater Table in Well, February 13, 2023
1	Open (5.0 / 229.3)	No Water	No Water
2	Open (5.0 / 232.3)	No Water	
3	Open (5.0 / 237.7)	No Water	No Water
4	Open (5.0 / 239.3)	No Water	
5	Open (5.0 / 232.0)	No Water	3.2 / 233.9
6	Open (5.0 / 230.2)	No Water	
7	Open (5.0 / 228.7)	4.4 / 229.3	1.4 / 232.3
8	Open (6.6 / 227.0)	No Water	
9	Open (5.0 / 232.3)	No Water	1.8 / 235.5
10	Open (1.5 / 227.0)	0.8 / 244.7	
11	Open (1.5 / 252.7)	No Water	
12	Open (1.5 / 261.0)	No Water	
14	Open (3.5 / 245.3)	No Water	0.6 / 248.2
15	Open (1.5 / 263.5)	No Water	
16	Open (1.8 / 264.2)	No Water	

Borehole	Depth of Cave (m) / Elev.	Unstabilized Groundwater Level Depth (m) / Elev.	Depth (m) / Elev. of Groundwater Table in Well, February 13, 2023
17	Open (2.4 / 260.3)	No Water	No Water
19	Open (3.5 / 245.7)	No Water	1.7 / 247.5
20	Open (3.5 / 244.5)	No Water	
21	Open (2.3 / 243.0)	No Water	1.2 / 244.0
22	Open (3.5 / 242.5)	No Water	
23	Open (3.5 / 243.7)	No Water	0.1 / 247.2
24	Open (3.5 / 243.9)	No Water	
25	Open (2.9 / 245.4)	No Water	0.2 / 248.1

Almost all boreholes were dry upon completion. About ten (10) days later, the stabilized groundwater levels in the wells were measured at 0.1 to 3.2 m (Elev. 232.3 and 248.2) below the existing ground surface. It is noted some groundwater is in the till and perched water is in the fill above the less pervious till.

The existing fill and sandy silt are permeable and will allow for the free flow of water when wet. The glacial till is generally not permeable.

Groundwater levels are expected to show seasonal fluctuations and vary in response to prevailing climate conditions.

3.4 Soil Corrosivity and Sulphate Attack on Concrete

The following soil samples were collected from the site and submitted to CALA-accredited Caduceon Laboratories for testing to determine the potential for soil corrosivity and sulphate attack on concrete:

- BH14 / SS2
- BH14 / SS4
- BH20 / SS2
- BH23 / SS4
- BH25 / SS2

The results of the chemical testing are provided in Appendix C.

The American Water Works Association (AWWA) has developed a scoring system in their C-105 Standard to determine the potential for soil to corrode cast iron alloys. The scoring system assigns points based on several soil parameters, including resistivity, pH, redox potential, sulfides, and moisture content. A rank of 10 or more indicates a potential for



Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

corrosion and suggests that corrosion protection measures should be considered. The results from the testing at this site is summarized below and the laboratory Certificate of Analysis is included as Appendix C.

Call Damanatan	AWWA Score					
Soil Parameter	BH14 / SS2	BH14 / SS3	BH20 / SS2	BH23 / SS4	BH25 / SS2	
Resistivity (ohm·cm)	0	0	0	0	0	
рН	0	0	0	0	0	
Redox Potential (mV)	0	0	0	0	0	
Sulfides (µg/g)	2	2	2	2	2	
Moisture	1	1	1	1	1	
TOTAL SCORE	3	3	3	3	3	

Based on the AWWA scoring system, samples scored less than 10 points which indicates a low potential for the soil corrosivity to affect cast iron alloys and corrosion protection measures are therefore not recommended for the site.

It should be noted that this ranking system provides a general indication of soil corrosivity potential only. Other external factors may increase corrosivity potential, such as stray electrical currents or the application of de-icing salts in the winter that can leach into the ground.

The samples were also tested for water-soluble sulphate content and compared to *Table 3:* Additional Requirements for Concrete Subjected to Sulphate Attack as found in CSA A23.1 Concrete Materials and Methods of Construction. Table 3 is used to determine the cementing materials required in concrete based on degree of exposure to sulphate attack. The testing shows the samples have less than 0.1% water-soluble sulphate, and therefore there will have negligible exposure to sulphate attack, as such no additives are required.

4. Engineering Design Parameters & Analysis

The City of Owen sound is proposing to replace the watermain water services on a section of 9th Avenue East in Owen Sound, Ontario from Superior Street to just north of 9th Street East approximately 1000 m in length. Some sections of sanitary and storm sewer may also be replaced along with all sanitary laterals. The current section of road is a four-lane road with curb and gutter and sidewalks. The road cross section will not change and the service trenches will be repaired after service installation (full road reconstruction is not required). It is understood that the inverts for the watermain would be about 2.0 m and inverts for the storm and sanitary sewer would be as deep as 3.5 m below the road grade.

Also, a looping watermain is part of the project. The alignment is about 1,350 m in length and extends from 8th Street East southerly to 6th Street East (through a Hydro One corridor), then west along 6th Street East for about 150 m, then south along private lands to Superior Street, then west along Superior Street to 9th Avenue East. then east to the dead end of 4th Street East. The watermain invert is about 2 m below existing grade.

Lastly, it is understood that the project will have several phases.

4.1 Service Installation

4.1.1 Bedding

The type of material and depth of granular bedding below the pipe will, to some extent, depend on the method of construction used by the contractor. Pipe bedding for flexible pipes should follow the requirements in Ontario Provincial Standard Drawing (OPSD) 802.010 or 802.013 or applicable municipal standards. Pipe bedding for rigid pipes should follow the requirements in OPSD 802.030 to 802.033 or applicable municipal standards.

The subgrade generally consisting of competent native soil at the site will provide adequate support for pipes with the bedding requirements as laid out in the above referenced OPS drawings. Earth fill was encountered in most boreholes which extended to 0.8 m to 3.8 m depth below the road grade. The fill below the invert level (if encountered) will need to be removed/sub-excavated and replaced with an increased thickness of granular bedding. On-site geotechnical inspections are required to verify encountered subgrade conditions and provide any required remedial recommendations on subgrade support for bedding materials.

Where disturbance of the trench base has occurred from ground water seepage, construction traffic, etc., the disturbed soils should be sub excavated and replaced with suitably compacted granular material. Details on temporary ground water control are provided in Section 5.2.



Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

Locally in the looping water alignment auger refusal was encountered shallower than the waterman invert at 1.5 to 1.8 m depth, Elev. 244.0 to 264.2 (Boreholes 10 to 12, 15 and 16), with refusal slightly deeper than the watermain invert at 2.3 to 2.9 m depth, Elev. 243.0 to 260.3 (Boreholes 17, 21 and 25). Where bedrock is present, rock excavation can be carried out to the proposed invert, or the pipes can be supported on the bedrock with insulation to provide the remaining frost protection. It is noted that 25 mm of insulation is equivalent to 300 mm of earth cover. The insulation will need to be placed in such a was such that the path for frost to the pipe is more than the 1.7 m of earth cover proposed.

Regardless of whether flexible or rigid pipes are implemented, granular bedding and cover material should consist of a well graded, free draining material, such as Granular "A" (OPSS.MUNI 1010). All granular bedding must be compacted to a minimum of 95% Standard Proctor maximum dry density (SPmdd).

4.1.2 Backfill

Excavated pavement structure granular soils, sandy inorganic earth fill, and native soils may be used as backfill in trenches, provided they are moisture conditioned so the moisture content is within 2% of optimum. The backfill should be compacted to a minimum of 95% SPmdd (see Section 5.3 for more details on soil compaction). In confined areas the layer thickness will have to be reduced to utilize smaller compaction equipment efficiently or by using granular material instead of locally sourced fill. Any backfill that is frozen, contains a high percentage of organic material (topsoil, peat, wood, etc.) or moisture, or has otherwise unsuitable deleterious inclusion should not be used as backfill. The maximum cobble or boulder size should not exceed half of the loose lift thickness (i.e., all particles with a diameter greater than 100 mm should be removed).

Where trenches are within the traveled portions of a roadway, backfill within the frost penetration depth of 1.5 m should consist of native, non-organic, excavated material consistent with the soils surrounding the trench. If this technique is not undertaken, then frequent problems arise with yearly differential frost heave movements between the trench backfill and the adjacent native soil. This would occur, for example, if imported granular material is used to backfill trenches which is less susceptible to frost effects compared to the native soils on site. Alternatively, if different soil is used as the backfill due to issues with achieving compaction, a frost taper of 10H:1V can be implemented to help mitigate the potential for differential settlement and frost heave.

4.2 Pavement Design and Construction

As noted earlier, over the service trenches, the pavement is to be repaired to match or slightly exceed the existing thicknesses.

Based on Boreholes 1 to 12 on 9th Avenue, 100 to 300 mm of asphalt (average 175 mm) is over a 120 to 660 mm of granular (average 470 mm) for a total thickness of 320 to 800 mm (average 645 mm). The recommended pavement reinstatement is as follows:

Pavement Layer	Compaction Requirements	Component Thickness
Surface Course Asphaltic Concrete: SP 12.5 (OPSS 1150, OPSS.MUNI 1151, and OPSS.MUNI 1101)		50 mm
Upper Binder Course Asphaltic Concrete: SP 19.0 (OPSS 1150, OPSS.MUNI 1151, and OPSS.MUNI 1101)	OPSS 310	75 mm
Lower Binder Course Asphaltic Concrete: SP 19.0 (OPSS 1150, OPSS.MUNI 1151, and OPSS.MUNI 1101)		75 mm
Base Course: Granular A (OPSS.MUNI 1010)	100% Standard	150 mm
Subbase Course: Granular B Type I (OPSS.MUNI 1010)	Proctor Maximum Dry Density (ASTM-D698)	500 mm

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Based on Boreholes 15 to 17 and 21 and 22, Superior Street and 6th Street East, 90 to 210 mm of asphalt (average 125 mm) is over a 400 to 660 mm of granular (average 573 mm) for a total thickness of 610 to 760 mm (average 700 mm). The recommended pavement reinstatement is as follows:

Pavement Layer	Compaction Requirements	Component Thickness
Surface Course Asphaltic Concrete: SP 12.5 (OPSS 1150, OPSS.MUNI 1151, and OPSS.MUNI 1101)	OPSS 310	40 mm
Binder Course Asphaltic Concrete: SP 19.0 (OPSS 1150, OPSS.MUNI 1151, and OPSS.MUNI 1101)	UP33 310	80 mm
Base Course: Granular A (OPSS.MUNI 1010)	100% Standard Proctor Maximum	150 mm
Subbase Course: Granular B Type I (OPSS.MUNI 1010)	Dry Density (ASTM-D698)	500 mm

Traffic volumes will be required to determine Categories for Superpave.

Subgrade preparation in road repair areas should involve proof rolling the exposed subgrade under supervision of geotechnical personnel to ensure the subgrade is compacted to a minimum 95% SPmdd. Any organic rich or deleterious soils are not a suitable subgrade and must be removed prior to placement of granular fill materials within reinstatement or widening areas. Zones with high moisture, deleterious materials, or excessive organics and, must be subexcavated and replaced with clean earth fill, placed and compacted following the specifications in Section 5.4 to a minimum of 95% SPmdd.

Special care should be taken to ensure that the elevation and slope of the pavement subgrade is maintained, so as to not create a sump within the pavement structure, at the edge of the pavement repair.

The long-term performance of the pavement structure is highly dependent upon the subgrade support conditions. Stringent construction control procedures must be maintained to ensure that uniform subgrade moisture and density conditions are achieved as much as and the subgrade is not disturbed or weakened after it is exposed.

The granular materials should be placed in lifts 200 mm thick or less and be compacted to a minimum of 100% SPmdd for both granular base and subbase. Asphalt materials should be

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rolled and compacted as per OPSS.MUNI 310. The granular and asphalt pavement materials and their placement should conform to OPSS.MUNI 1101, 1010, 1151 and 1150.

As discussed earlier in the report, the existing pavement structure granular material does not conform to OPSS.MUNI 1010 specifications for Granular A or B and cannot be re-used in a new pavement structure as the base or subbase courses but is suitable for re-use as bulk fill.

It should be noted that in addition to adherence of the above pavement design recommendations, a close control on the pavement construction process will also be required in order to obtain the desired pavement life. Therefore, it is recommended that regular inspection and testing should be conducted during the pavement construction to confirm material quality, thickness, and to ensure adequate compaction.

Longitudinal asphalt joints should be milled into the existing asphalt a minimum 0.5 m for each lift.

5. Constructability Considerations

5.1 Excavations

Excavation for the service installation is anticipated to extend as deep as approximately 2.0 to 3.5 m below the road grade to allow for pipe bedding. Excavation will encounter the pavement, fill, and underlying glacial till. Harder digging can be experienced in the glacial till. Boulders and cobbles may be encountered in the glacial till.

Locally, bedrock will be encountered in the watermain loop as noted earlier. Where blasting is employed to remove the bedrock below the pipe inverts, precondition surveys are recommended around the site. This document will assist in resolution of claims arising from complaints of construction related damage. A blasting monitoring program should be implemented to optimize the effectiveness of the blasting while monitoring/maintaining vibration to acceptable levels.

Excavations must be carried out in accordance with the Occupational Health and Safety Act, Ontario Regulation 213/91 (as amended), Construction Projects, Part III - Excavations, Section 222 through 242. Where workers must enter a trench or excavation the soil must be suitably sloped and/or braced in accordance with the OHSA.

These regulations designate four (4) broad classifications of soils to stipulate appropriate measures for trench safety. If more than one soil type is encountered in a trench, the soil type with the highest number will govern the trench/excavation sidewall geometry. Subject to adequate groundwater control, as required and discussed in the next section, trenches for utility installation/replacement shall be carried out with Type 3 Soil geometry, with sidewalls to be constructed no steeper than 1H:1V from the base of the excavation.

Minimum support system requirements for steeper excavations are stipulated in Sections 235 through 238 and 241 of the OHSA and include provisions for timbering, shoring and moveable trench boxes. To reduce the potential for instability of the trench excavations, materials excavated from the service trenches and/or other fill materials or heavy equipment should not be placed near the crest of the trench excavations.

It is important to note that soils encountered in the construction excavations may vary significantly across the site. Our preliminary soil classifications are based solely on the materials encountered in the boreholes advanced on site. The contractor should verify that similar conditions exist throughout the proposed area of excavation. If different subsurface conditions are encountered at the time of construction, it is recommended that GEI be contacted immediately to evaluate the conditions encountered.

5.2 Temporary Construction Excavation Groundwater Control

As noted in the last section, the trench excavation is anticipated to approximately 2.0 to 3.5 m depth below the road grade.

Almost all boreholes were dry upon completion. About ten (10) days later, the stabilized groundwater levels in the wells were measured at 0.1 to 3.2 m (Elev. 232.3 and 248.2) below the existing ground surface. It is noted some groundwater is in the till and perched water is in the fill above the less pervious till.

It is important to control the groundwater adequately. If the groundwater table is not controlled during construction, the base of the excavation/culvert foundation pipe bed may become unstable. For trench excavation as described above the excavation will extend through the pavement, fill and into the underlying glacial till deposits. No major groundwater problems are anticipated for the installation of services to the depths noted. Any water seepage should be controlled by the use of conventional sump pumping, for most excavations. Greater localized seepage may be encountered, and these areas may require pumping from keg wells or the like to control ground water.

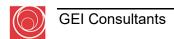
It is recommended to carry out the work during the dry time of the year when the ground water table is lowest, to mitigate groundwater control measures. Also reducing the size of the excavation that is open at any one time will aid in reducing groundwater control requirements.

The exact scenario where these groundwater control techniques will work are estimates only and are directly correlated to how coarse/fine the native soils are in an excavation, and both the lateral and vertical extent of the cohesionless deposits encountered. If the groundwater table is not controlled during construction, the base of the excavations will probably be unstable, leading to difficulties in excavating and placement of the service pipes.

A preliminary assessment on the amount of dewatering required for the service installations due to groundwater entering an open trench is likely less than 50,000 L/day. A Permit to Take Water (PTTW) from the MECP, is not required (dewatering greater than 400,000 L/day). Registry on the ESAR system may be prudent to allow for greater pumping, if required.

5.3 Compaction Specifications

Standard Proctor maximum dry density is the specification to indicate the degree to which soil or aggregate is compacted. To achieve the specified SPmdd as indicated in this report, all soils or aggregates must be placed in lift thicknesses no greater than 200 mm. If this is not the case, only the upper portion of the lift will be adequately compacted, and the lower portion of the lift has a high probability of not meeting compaction specifications. In addition, industry standard equipment used to determine the degree of compaction consists of nuclear



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densometers. These devices have an inherent limitation in that they cannot test beyond 300 mm in depth, and so the degree of compaction beyond this depth cannot be quantitatively determined.

Along with lift thickness, ensuring that the soil or aggregate is within 2% of its optimum moisture content ensures that the specified compaction can be reached. If the soil or aggregate is too dry/wet, it is either very difficult or impossible to reach the specified compaction. This is especially true for when higher compaction specifications such as 98% and 100% SPmdd are required.

Moisture can be increased by adding water and mixing the soil prior to re-use, or by importing soil to the site that is at optimum and can be readily compacted.

Moisture can be reduced by tilling or spreading out the soil to dry or blending it with drier material. In-situ moisture contents can change based on the season and local groundwater levels and can also change for stockpiled material due to precipitation. Zones of the fine-grained soil beneath the site have very high moisture contents and moisture conditioning may be difficult to accomplish.

In addition to the above compaction specifications, in any areas where compacted fill will be placed over the exposed native soil subgrade, any loose, soft, organic soil, wet or unstable areas should be sub-excavated, and backfilled with site inorganic soil or Granular 'B' (OPSS.MUNI 1010) compacted to a minimum of 95% SPmdd. This recommendation applies to site servicing and pavement subgrades.

5.4 Quality Verification Services

On-site quality verification services are an integral part of the geotechnical design function. Quality verification services are used to confirm that construction is being conducted in general conformance with the requirements as outlined in the drawings, reports and specifications prepared for the proposed development.

GEI Consultants can provide all the on-site quality verification services outlined below:

- Part-time monitoring of the subgrade support capabilities, material quality, lift thickness, moisture content, degree of compaction, etc. is recommended for the following areas to ensure the recommendations within this report are followed and they perform adequately in the long-term:
 - o Pavement structure (granular layers and asphalt); and
 - o Bedding/backfilling of culvert.
- Full-time monitoring of the subgrade support capabilities, material quality, lift thickness, moisture content, degree of compaction, etc. is recommended for engineered fill under structures;



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• Testing of the concrete (compressive strength, slump, air content, etc.) and testing of the asphalt (asphalt content and gradation) are recommended to ensure that the quality of the materials being brought to site meet the requirements of the project. This would only apply to poured in place foundations and not pre-cast structures.

6. Limitations and Conclusions

6.1 Limitations

The recommendations and comments provided are necessarily on-going as new information of underground conditions becomes available. More specific information with respect to the conditions between samples, or the lateral and vertical extent of materials may become apparent during excavation operations. The interpretation of the borehole information must, therefore, be validated during excavation operations. Consequently, conditions not observed during this investigation may become apparent. Should this occur, GEI should be contacted to assess the situation and additional testing and reporting may be required.

GEI should be retained for a general review of the final design drawings and specifications to verify that this report has been properly interpreted and implemented. If not accorded the privilege of making this review, GEI will assume no responsibility for interpretation of the recommendations in the report.

The comments given in this report are intended only for the guidance of the design engineers. The number of boreholes required to determine the localized underground conditions between boreholes affecting construction costs, techniques, sequencing, equipment, scheduling, etc. could be greater than has been carried out for design purposes. Contractors bidding on or undertaking the works should, in this light, decide on their own investigations, as well as their own interpretations of the factual borehole results, so that they may draw their own conclusions as to how the subsurface conditions may affect them.

This report was authorized by, and prepared by GEI for, the account of Tatham Engineering Limited (as provided the signed Agreement for Professional Consulting Services provided by Tatham Engineering Limited). Any use which a third party makes of this report, or any reliance on or decisions to be made based on it, are the responsibility of such third parties. GEI accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made, or actions based on this project.

6.2 Conclusion

It is recognized that municipal/regional governing bodies, in their capacity as the planning and building authority under Provincial statues, will make use of and rely upon this report, cognizant of the limitations thereof, both as are expressed and implied.

GEI trusts this report is complete within our terms of reference, and the information presented is sufficient for your present purposes. If you have any questions, or when we may be of further assistance, please do not hesitate to contact our office.

Yours Truly,

GEI Consultants

G.R. WHITE

Mar. 24, 2023

Mar. 24, 2023

Mar. 24, 2023

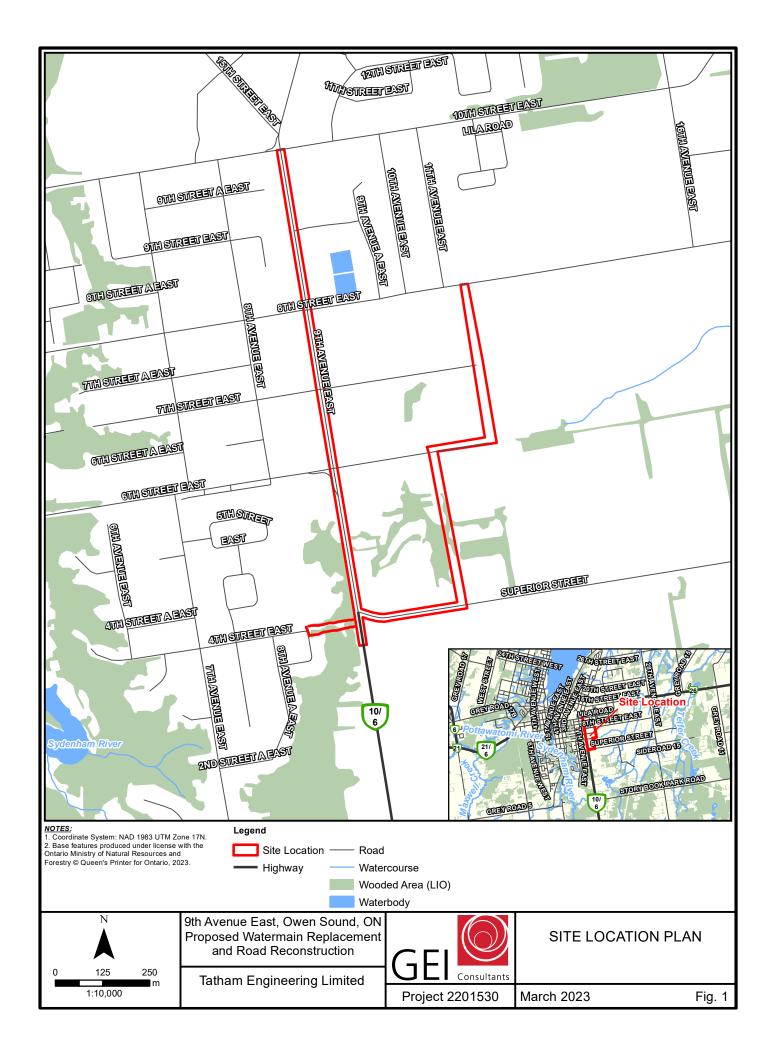
MohdRan

Mohammed Razeen Geotechnical E.I.T.

Geoffrey R. White, P.Eng. Geotechnical Practice Lead Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

Figures

Site Location Plan
Borehole Location Plan





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Appendix A

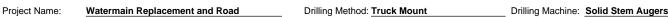
Borehole Logs

RECORD OF BOREHOLE No. 1 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4935009 Date Started: Feb 1/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505716 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL Sample Number DISTRIBUTION Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) EVATION 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Lithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 220 mm AS 1 GRANULAR FILL: 120 mm 234 FILL: Silty sand, trace gravel, dense, brown, moist 18 SS 2 100 49 1.5 SANDY SILT GLACIAL TILL: Some 17 SS 3 75 71 071 clay, trace to some gravel, trace shale 232.5 fragments, very dense, greyish brown, moist - - - Dense, brownish red - - -SS 4 100 31 31 C 10 32 40 18 - - - Very Dense - - -**18** ○ SS 5 100 51 O**5**1 231 45 18 - - - Dense, grey - - -**44** \Diamond SS 6 100 44 -229.5 229.3 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75

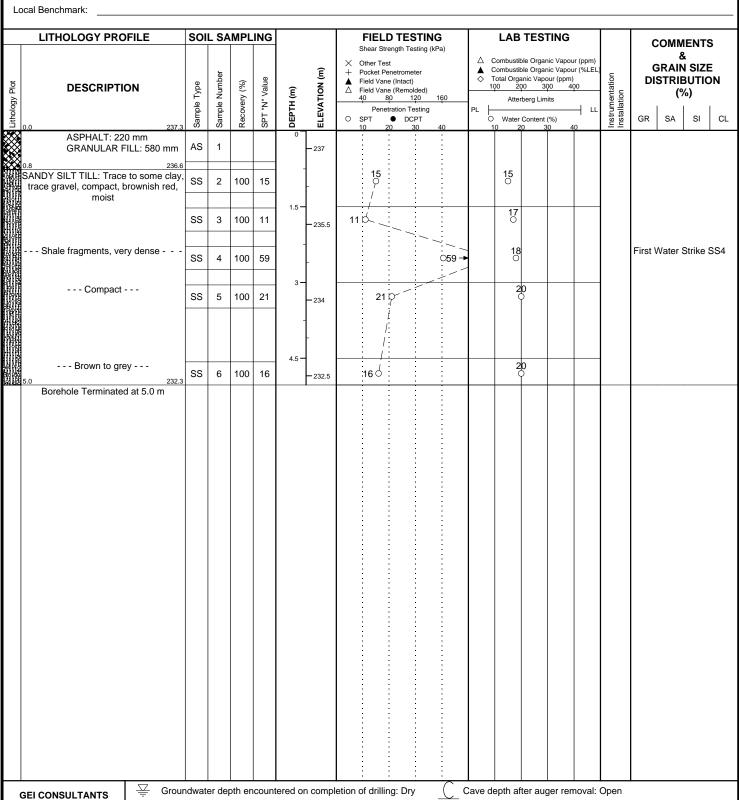
Page: 1 of 1

RECORD OF BOREHOLE No. 2

Project Number: 2201530 Project Client: Tatham Engineering Ltd.



9th Ave E, Owen Sound, ON Project Location: Logged By: MН Northing: 4934935 Date Started: Feb 1/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505727 Date Completed: _ Feb 3/23 Easting:



GEI CONSULTANTS 647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater Elevation:

Groundwater depth observed on:

RECORD OF BOREHOLE No. 3 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934850 Date Started: Feb 1/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505793 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number DISTRIBUTION Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Penetration Testing 6 GR 0 SA SI CL SPT Water Content (%) DCPT ASPHALT: 260 mm AS 1 GRANULAR FILL: 500 mm 16 FILL: Silty sand, trace gravel, compact, SS 2 75 13 brown, moist -241.5 1.5 15 SS 3 45 11 - - Clayey silt, some sand, trace 18 SS 4 10 3 gravel, soft - - -SS 5 25 4 SANDY SILT TILL: Some clay, trace SS 6 75 16 gravel, compact, brownish red, moist - 238.5 45 - - - Grey - - -SS 7 100 22 22:0 237.7 Borehole Terminated at 5.0 m Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 4 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934771 Date Started: Feb 1/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505757 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Sample Type Recovery (%) 200 300 Field Vane (Remolded) (%) Atterberg Limits Lithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 150 mm AS 1 GRANULAR FILL: 650 mm FILL: Silty sand, trace gravel, brownish 18 SS 2 35 44 red, dense, brown, moist -243 1.5 - - Clayey silt, trace sand, trace **16** SS 3 75 6 6 🔾 gravel, brownish red, firm - - -SS 4 35 7 SANDY SILT TILL: Some clay, trace 16 SS 5 100 37 gravel, dense, brownish red, moist -240 45 - - - Compact - - -17 SS 6 75 11 11 O 239.3 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75

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RECORD OF BOREHOLE No. 5 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934619 Date Started: Jan 31/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505781 Date Completed: __Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number DISTRIBUTION Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 100 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 300 mm AS 1 GRANULAR FILL: 360 mm SANDY SILT GLACIAL TILL: Trace to **15** some clay, trace to some gravel, SS 2 100 16 cobbles and boulders, compact, brown moist 1.5 - 235.5 17 3 100 18 18 Q: SILTY SAND GLACIAL TILL: Some 17 SS 4 100 30 30 \ gravel, some clay, cobbles and boulders, dense, brown, moist 234 SS 5 100 32 32:0 38 12 45 -232.5 14 33 0 SS 100 33 232.0 Borehole Terminated at 5.0 m Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 3.2 m. Groundwater Elevation: 233.9 m Barrie, Ontario L4N 0B7

Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

Scale: 1:75

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T: (705) 719-7994

RECORD OF BOREHOLE No. 6 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934545 Date Started: Jan 31/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505794 Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Lithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 130 mm GRANULAR FILL: 290 mm 234.8 AS 1 FILL: Silty sand, some clay, trace gravel, compact, brown, moist **15** SS 2 100 16 234 1.5 SANDY SILT GLACIAL TILL: Trace to 16 18 Q: SS 3 100 18 some clay, trace gravel, cobbles and boulders, compact, brown, moist - - - Dense - - -SS 4 100 30 30 \ 232.5 SS 5 100 32 32:0 -231 45 17 33 0 SS 6 100 33 230.2 Borehole Terminated at 5.0 m Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 7 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934433 Date Started: Jan 31/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505812 Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number DISTRIBUTION Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Sample Type Recovery (%) 100 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Lithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 120 mm AS 1 GRANULAR FILL: 200 mm FILL: Silty sand, some gravel, very loose, brown, wet 20 AS 2 232.5 1.5 - - Sandy clayey silt, trace gravel, SS 3 100 8 loose - - -SANDY CLAYEY SILT GLACIAL TILL: SS 4 100 13 13 Q Trace gravel, cobbles and boudlers, 231 stiff/compact, brown, moist - - - Very stiff, grey - - -SS 5 100 26 26 229 5 20 20 0 SS 6 100 20 228.7 Borehole Terminated at 5.0 m Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: 4.4 m. **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 1.4 m. Groundwater Elevation: 232.3 m Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 8 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934356 Date Started: Jan 31/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505826 Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL DISTRIBUTION Sample Number Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) EVATION 200 300 Field Vane (Remolded) (%) Atterberg Limits ithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 150 mm GRANULAR FILL: 450 mm AS 1 CLAYEY SILT GLACIAL TILL: Trace to 20 Some sand, trace gravel, cobbles and boulders, stiff, brown, wet SS 2 100 13 - 232.5 1.5 - - - Very stiff - - -SS 3 100 17 12 35 SS 4 100 27 231 27 - - - Hard - - -SS 5 100 31 229.5 45 SS 6 100 33 33 🗘 228 CLAYEY SANDY SILT GLACIAL TILL: 41 0 SS 7 100 41 6. Trace gravel, cobbles and boudle hard/very dense, brown, moist Borehole Terminated at 6.6 m Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS** Groundwater depth observed on:

647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater Elevation:

RECORD OF BOREHOLE No. 9 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934179 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505854 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Penetration Testing 6 GR 0 SA SI CL SPT Water Content (%) DCPT ASPHALT: 170 mm GRANULAR FILL: 590 mm AS 1 237 19 FILL: Sand and silt, trace gravel, SS 2 100 14 compact, dark color, moist 1.5 --- Loose ---SS 3 100 6 **6** \circlearrowleft 235.5 SANDY SILT GLACIAL TILL: Trace to SS 4 100 12 120 some clay, trace gravel, cobbles and boulders, compact, brown, wet SS 5 100 18 18 Q 234 45 - - - Very dense - - -24 SS 100 50 50 232.5 232.3 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 1.8 m. Groundwater Elevation: 235.5 m Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 10 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount MH Project Location: 9th Ave E, Owen Sound, ON Logged By: Northing: 4934057 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505861 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING COMMENTS** Shear Strength Testing (kPa) \triangle Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL .EVATION (m) Total Organic Vapour (ppm) 100 200 300 40 Sample Number DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) Field Vane (Remolded) (%) 160 80 Atterberg Limits Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 100 mm GRANULAR FILL: 660 mm AS 1 **15** FILL: Silty sand, some rock fragments, SS 2 35 13 compact, brown, moist Borehole Terminated at 1.5 m Upon Auger Refusal \subseteq Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: 0.8 m. **GEI CONSULTANTS** 647 Welham Road, Unit 14

Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

Groundwater Elevation:

Scale: 1:75

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Groundwater depth observed on:

Barrie, Ontario L4N 0B7 T: (705) 719-7994

RECORD OF BOREHOLE No. 11 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount 9th Ave E, Owen Sound, ON MH Project Location: Logged By: Northing: 4933944 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505883 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING COMMENTS** Shear Strength Testing (kPa) \triangle Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL .EVATION (m) Total Organic Vapour (ppm) 100 200 300 40 Sample Number DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 100 Field Vane (Remolded) (%) 160 80 Atterberg Limits Penetration Testing 6 O SPT GR SA SI CL Water Content (%) DCPT ASPHALT: 120 mm GRANULAR FILL: 650 mm AS 1 30 FILL: Silty sand, dense, brown, moist 14 SS 2 75 30 Borehole Terminated at 1.5 m Upon Auger Refusal \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 12 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount MH Project Location: 9th Ave E, Owen Sound, ON Logged By: Northing: 4933848 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 505897 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING COMMENTS** Shear Strength Testing (kPa) \triangle Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL .EVATION (m) Total Organic Vapour (ppm) 100 200 300 40 Sample Number DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle Recovery (%) **DESCRIPTION** 100 Field Vane (Remolded) (%) 160 80 Atterberg Limits Penetration Testing 6 O SPT GR SA SI CL Water Content (%) DCPT ASPHALT: 160 mm GRANULAR FILL: 600 mm AS 1 30 FILL: Silty sand, some gravel, dense, SS 2 55 30 brown, mosit Borehole Terminated at 1.5 m Upon Auger Refusal \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75

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RECORD OF BOREHOLE No. 14 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers MH Project Location: 9th Ave E, Owen Sound, ON Logged By: Northing: Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) \triangle Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle 둳 **DESCRIPTION** Recovery (%) 100 200 300 Field Vane (Remolded) (%) Lithology 80 Atterberg Limits Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT TOPSOIL: 75 mm SS 1 85 18 0 18 FILL: Sandy silt, trace gravel, trace organics and rootlets, compact, brown, moist SANDY SILT: Trace gravel, trace clay, 26 🔈 SS 2 100 26 compact, brown, moist - 247.5 1.5 - - - Dense - - -**13** SS 3 100 31 31 0 SAND AND SILT GLACIAL TILL: Trace 14 SS 4 100 60 O60 55 35 clay, trace gravel and clay, cobbles and boulders, very dense, grey 246 - - - Trace rock fragments - - -SS 5 40 50+ 50+ 245.3 Borehole Terminated at 3.5 m \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 0.6 m. Groundwater Elevation: 248.2 m Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 16 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4933912 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506070 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING COMMENTS** Shear Strength Testing (kPa) \triangle Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL .EVATION (m) Sample Number Total Organic Vapour (ppm) DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 100 300 Field Vane (Remolded) (%) 160 80 Atterberg Limits Lithology Penetration Testing 6 O SPT GR SA SI CL Water Content (%) DCPT ASPHALT: 210 mm GRANULAR FILL: 400 mm AS 1 265.5 SANDY SILT GLACIAL TILL: Some 16 clay, trace gravel, cobbles and SS 2 100 12 boulders, compact, brownish red, moist 1.5 SS 3 11 0 35 11 264.2 Borehole Terminated at 1.8 m Upon Auger Refusal \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open

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Groundwater Elevation:

Groundwater depth observed on:

RECORD OF BOREHOLE No. 17 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4933925 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506164 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 100 200 300 Field Vane (Remolded) (%) 80 160 Atterberg Limits Penetration Testing 6 GR 0 SA SI CL SPT Water Content (%) DCPT ASPHALT: 100 mm GRANULAR FILL: 660 mm 262.5 AS 1 **16** FILL: Clayey silt, some sand, trace SS 2 100 12 gravel, cobbles and boulbers, stiff, brown, moist 1.5 SANDY SILT GLACIAL TILL: Some **16** SS 3 0 22 -261 22.0 clay, trace gravel, cobbles and boulders, compact to very dense, 17 brown, moist 50÷ 260.3 ∖SS 4 100 50+, Borehole Terminated at 2.4 m Upon Auger Refusal \subseteq Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. Scale: 1:75

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RECORD OF BOREHOLE No. 19 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934148 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506120 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL Sample Number DISTRIBUTION Total Organic Vapour (ppm) Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) EVATION 100 200 300 Field Vane (Remolded) (%) 80 Atterberg Limits Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT TOPSOIL: 100 mm 249 SS 1 100 28 FILL: Clayey silt, trace sand, some rock fragments, very stiff to stiff, brown, moist 18 SS 2 100 9 SANDY CLAYEY SILT GLACIAL TILL trace gravel, cobbles and boulders. 1.5 **16** stiff/loose, brown SS 3 100 9 8 26 39 27 SS 4 45 9 - - - Trace rock fragments, hard/very SS 5 55 50+ 246 50+ Borehole Terminated at 3.5 m Upon Auger Refusal

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Groundwater depth encountered on completion of drilling: Dry

Groundwater depth observed on: Feb 13/23 at depth of: 1.7 m.

Cave depth after auger removal: Open

RECORD OF BOREHOLE No. 20 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934215 Date Started: Feb 2/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506110 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle Plot **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) Atterberg Limits Lithology Penetration Testing 6 O SPT GR SA SI CL Water Content (%) DCPT TOPSOIL: 150 mm SS 1 100 6 FILL: Clayey silt, trace to some sand, 0 24 trace organics, stiff, brown, moist 17 SS 2 100 7 1.5 SANDY CLAYEY SILT GLACIAL TILL: 19 SS 3 100 12 12.0 Trace gravel, cobbles and boulders, 246 stiff/ compact to loose, brown, moist **17** SS 4 100 9 70 SS 5 100 7 244. Borehole Terminated at 3.5 m \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

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RECORD OF BOREHOLE No. 21 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934337 Date Started: Jan 30/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506106 Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL .EVATION (m) Sample Number Total Organic Vapour (ppm) DISTRIBUTION Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 100 200 300 Field Vane (Remolded) (%) 80 160 Atterberg Limits Penetration Testing 6 GR O SPT SA SI CL Water Content (%) DCPT ASPHALT: 125 mm GRANULAR FILL: 625 mm AS 1 244 5 17 FILL: Clayey silt, trace gravel, stiff, SS 2 100 8 brownish red, moist 1.5 **16** SANDY SILT: Some clay, loose, brown, 3 100 7 70: wet Borehole Terminated at 2.3 m Upon Refusal to Aguer \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 1.2 m. Groundwater Elevation: 244.0 m Barrie, Ontario L4N 0B7 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

Scale: 1:75

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RECORD OF BOREHOLE No. 22

Project Number: 2201530



Project Client: Tatham Engineering Ltd.

9th Ave E, Owen Sound, ON

Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount

Logged By:

MН

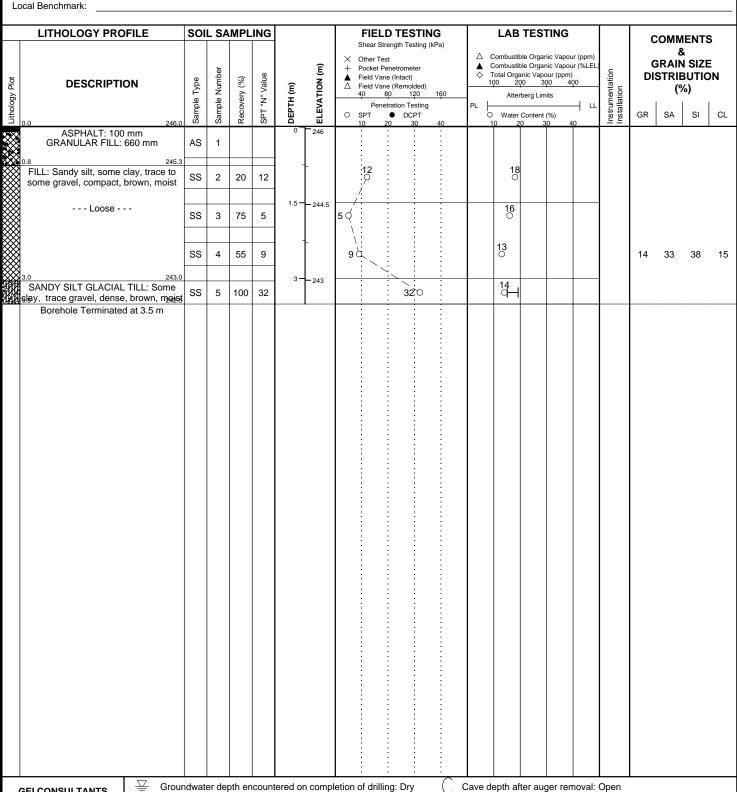
4934354 Date Started: Jan 30/23

Drilling Location: See Borehole Location Plan

Project Location:

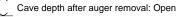
Reviewed By: GW 506237 Date Completed: Feb 3/23 Easting:

Northing:



GEI CONSULTANTS 647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater depth observed on:



Groundwater Elevation:

RECORD OF BOREHOLE No. 23 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934484 Date Started: Jan 30/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506228 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 100 200 300 Field Vane (Remolded) (%) Atterberg Limits Lithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT ASPHALT: 125 mm 1 100 SS 12 0 12 0 27 FILL: Sandy Silt, some clay strace organics, trace gravel, compact, brown, moist 18 140 SANDY SILT GLACIAL TILL: Trace to SS 2 100 14 Some clay, trace to some gravel, cobbles and boulders, compact, brown 1.5 **15** moist 3 100 15 15 Q 17 SS 4 100 23 23 0 244.5 **16** ○ - - - Very dense - - -SS 5 100 66 O66 18 32 39 243.7 Borehole Terminated at 3.5 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 0.1 m. Groundwater Elevation: 247.2 m Barrie, Ontario L4N 0B7

Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

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Page: 1 of 1

T: (705) 719-7994

RECORD OF BOREHOLE No. 24 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934562 Date Started: Jan 30/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506214 Date Completed: Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm) Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) Atterberg Limits ithology Penetration Testing 6 0 GR SA SI CL SPT Water Content (%) DCPT TOPSOIL: 150 mm SS 1 100 6 0 26 FILL: Clayey silt, trace organics, soft, brown, moist SANDY SILT TILL: Some clay, trace 18 19 7 SS 2 100 19 gravel, cobbles and boulders, compact, brown, moist 246 1.5 **17** SS 3 100 25 25 🗘 16 SS 4 100 23 23 🗘 - - - Dense - - -SS 5 100 44 440 243.9 Borehole Terminated at 3.5 m \subseteq Cave depth after auger removal: Open Groundwater depth encountered on completion of drilling: Dry **GEI CONSULTANTS**

647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater depth observed on: Groundwater Elevation:

RECORD OF BOREHOLE No. 25 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Project Name: Watermain Replacement and Road Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Location: 9th Ave E, Owen Sound, ON Logged By: MН Northing: 4934649 Date Started: Jan 31/23 Drilling Location: See Borehole Location Plan Reviewed By: GW 506201 Date Completed: _ Feb 3/23 Easting: Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING LAB TESTING **FIELD TESTING COMMENTS** Shear Strength Testing (kPa) Combustible Organic Vapour (ppm Other Test **GRAIN SIZE** Pocket Penetrometer Combustible Organic Vapour (%LEL EVATION (m) Sample Number Total Organic Vapour (ppm) **DISTRIBUTION** Field Vane (Intact) SPT "N" Value \triangle **DESCRIPTION** Recovery (%) 200 300 Field Vane (Remolded) (%) Lithology Atterberg Limits Penetration Testing 6 GR 0 SA SI CL SPT Water Content (%) DCPT TOPSOIL: 150 mm SS 1 100 8 FILL: Clayey silt, some organics, trace 8 O 23 rootlets, stiff, dark color, moist 247.5 SANDY SILT GLACIAL TILL: Trace to 17 SS 2 100 13 13 Þ some clay, trace gravel, cobbles and boulders, compact, brown, moist 1.5 19 3 100 12 120 246 - - - Very dense - - -SS 4 65 50+ 50+ Borehole Terminated at 2.9 m Upon Auger Refusal \subseteq Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 Groundwater depth observed on: Feb 13/23 at depth of: 0.2 m. Groundwater Elevation: 248.1 m

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

Appendix B

Geotechnical Laboratory Testing

GRAIN SIZE DISTRIBUTION REPORT GRANULAR A



Project Name: 9th Avenue East Project No.: 2201530 Client:

Tatham Engineering Limited

Supplier:

Sampled From: BH6, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

GEI Lab No. 5236 Figure No. B1

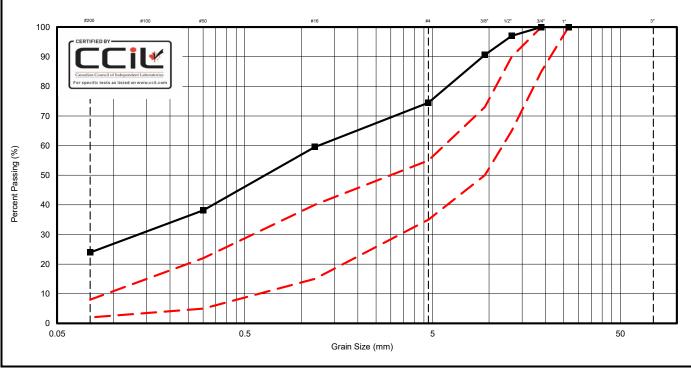
SAMPLE DATA

Total Mass of Sample (g):	2601.6	% Passing 75um by washing:	23.56	
Total Mass retained on the 4.75mm sieve (g):	664	Total Losses (%): (Maximum 0.3%)	0.00	
Total Mass passing the 4.75 mm sieve (g):	1937.6	Percent Crushed: (Min. 60% - Gran A)		
Percent Coarse Aggregate:	25.52	Not Applicable - Gran. "B" Type 1	-	
Percent Fine Aggregate:	74.48	Asphalt Coated Particles (%) (Max. 30%)	-	

	TOTAL SAME	PLE PERCENTA	AGES	COARSE AND FINE PORTION PERCENTAGES				
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	-	-	-	ı	150	-	-	
26.5	100.0	100	100	Υ	26.5	0.0	-	
19.0	100.0	85	100	Υ	19.00	0.0	-	
13.2	97.0	65	90	Ν	13.2	11.6	1	
9.5	90.6	50	73	Ν	9.5	36.8	1	
4.75	74.5	35	55	Ν	4.75	100.0	1	
1.18	59.5	15	40	Ν	1.18	-	20.1	
0.30	38.1	5	22	Ν	0.30	-	48.8	
0.15	-	ı	-	•	0.15	-	1	
0.075	23.9	2	8	N	0.075	-	67.9	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'A'



GRAIN SIZE DISTRIBUTION REPORT GRANULAR 'B' TYPE I



 Project Name:
 9th Avenue East

 Project No.:
 2201530

 Client:
 Tatham Engineering Limited

 Supplier:

 Sampled From:
 BH6, AS1, 0-2'

 GEI Lab No.
 5236

 Figure No.
 B2

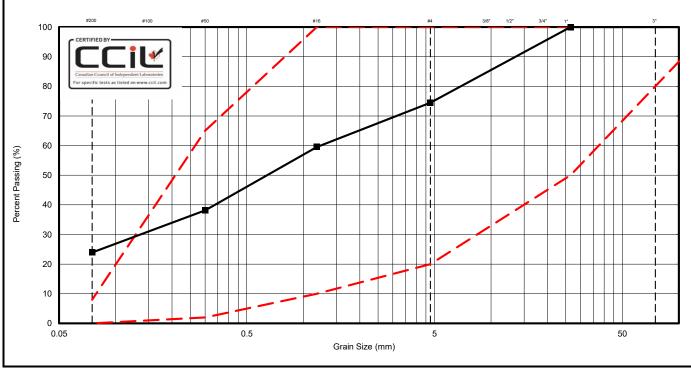
SAMPLE DATA

Total Mass of Sample (g):	2601.6	% Passing 75um by washing:	23.56	
Total Mass retained on the 4.75mm sieve (g):	664	Total Losses (%): (Maximum 0.3%)	0.00	
Total Mass passing the 4.75 mm sieve (g):	1937.6	1937.6 Percent Crushed: (Min. 60% - Gran A)		
Percent Coarse Aggregate:	25.52	Not Applicable - Gran. "B" Type 1	N/A	
Percent Fine Aggregate:	74.48	Asphalt Coated Particles (%) (Max. 30%)	-	

	TOTAL SAME	PLE PERCENTA	AGES	COARSE AND FINE PORTION PERCENTAGES				
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	100.0	100	100	Υ	150	0.0	-	
26.5	100.0	50	100	Υ	26.5	0.0	•	
19.0	-	-	-	-	19.00	-	-	
13.2	-	-	-	-	13.2	-	•	
9.5	-	-	-	-	9.5	-	•	
4.75	74.5	20	100	Υ	4.75	100.0	-	
1.18	59.5	10	100	Υ	1.18	-	20.1	
0.30	38.1	2	65	Υ	0.30	-	48.8	
0.15	-	-	-	-	0.15	-	-	
0.075	23.9	0	8	N	0.075	-	67.9	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'B' Type I



GRAIN SIZE DISTRIBUTION REPORT GRANULAR A



Project Name: 9th Avenue East Project No.: 2201530 Client:

Tatham Engineering Limited

Supplier:

Sampled From: BH9, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

GEI Lab No. 5237 Figure No.

В3

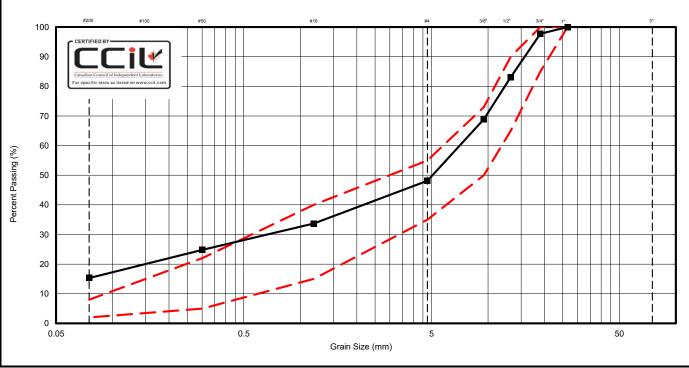
Total Mass of Sample (g):	1468.6	% Passing 75um by washing:	14.93
Total Mass retained on the 4.75mm sieve (g):	761.8	Total Losses (%): (Maximum 0.3%)	0.00
Total Mass passing the 4.75 mm sieve (g):	706.8	Percent Crushed: (Min. 60% - Gran A)	
Percent Coarse Aggregate:	51.87	Not Applicable - Gran. "B" Type 1	-
Percent Fine Aggregate:	48.13	Asphalt Coated Particles (%) (Max. 30%)	-

SAMPLE DATA

	TOTAL SAM	PLE PERCENTA	AGES	COARSE AND FINE PORTION PERCENTAGES				
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	-	-	-	-	150	-	-	
26.5	100.0	100	100	Υ	26.5	0.0	-	
19.0	97.7	85	100	Υ	19.00	4.4	-	
13.2	83.1	65	90	Υ	13.2	32.6	•	
9.5	68.9	50	73	Υ	9.5	59.9	•	
4.75	48.1	35	55	Υ	4.75	100.0	-	
1.18	33.7	15	40	Υ	1.18	-	30.0	
0.30	24.8	5	22	N	0.30	-	48.5	
0.15	1	ı	-	-	0.15	-	•	
0.075	15.3	2	8	N	0.075	-	68.2	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'A'



GRAIN SIZE DISTRIBUTION REPORT GRANULAR 'B' TYPE I



 Project Name:
 9th Avenue East
 I

 Project No.:
 2201530
 I

 Client:
 Tatham Engineering Limited
 0

Supplier: -

Sampled From: BH9, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

 GEI Lab No.
 5237

 Figure No.
 B4

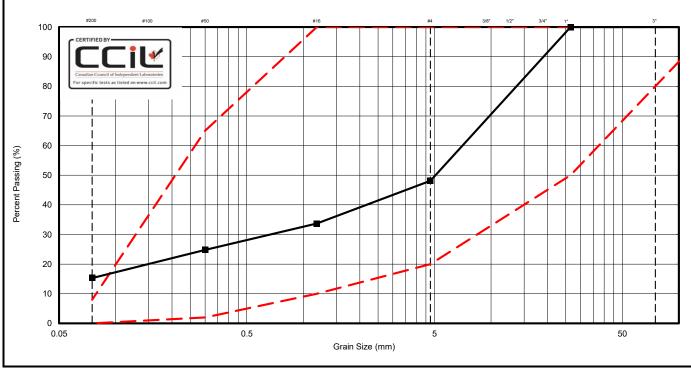
SAMPLE DATA

Total Mass of Sample (g):	1468.6	% Passing 75um by washing:	14.93	
Total Mass retained on the 4.75mm sieve (g):	761.8	Total Losses (%): (Maximum 0.3%)	0.00	
Total Mass passing the 4.75 mm sieve (g):	706.8	Percent Crushed: (Min. 60% - Gran A)	N/A	
Percent Coarse Aggregate:	51.87	Not Applicable - Gran. "B" Type 1	IN/A	
Percent Fine Aggregate:	48.13	Asphalt Coated Particles (%) (Max. 30%)	-	

TOTAL SAMPLE PERCENTAGES					COARSE AND FINE PORTION PERCENTAGES			
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	100.0	100	100	Υ	150	0.0	-	
26.5	100.0	50	100	Υ	26.5	0.0	-	
19.0	-	-	-	-	19.00	-	-	
13.2	-	-	-	-	13.2	-	-	
9.5	-	-	-	-	9.5	-	ı	
4.75	48.1	20	100	Υ	4.75	100.0	ı	
1.18	33.7	10	100	Υ	1.18	-	30.0	
0.30	24.8	2	65	Υ	0.30	-	48.5	
0.15	-	-	-	-	0.15	-	ı	
0.075	15.3	0	8	Ν	0.075	-	68.2	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'B' Type I



GRAIN SIZE DISTRIBUTION REPORT GRANULAR A



 Project Name:
 9th Avenue East

 Project No.:
 2201530

 Client:
 Tatham Engineering Limited

Supplier: - ratham Engineering Limited

Sampled From: BH16, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

 GEI Lab No.
 5238

 Figure No.
 B5

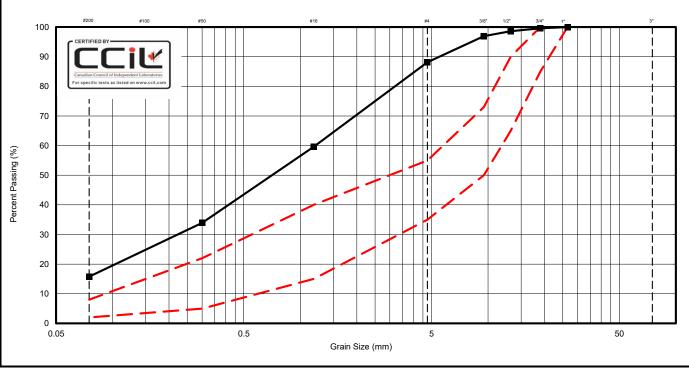
SAMPLE DATA

Total Mass of Sample (g):	3447.4	% Passing 75um by washing:	15.31
Total Mass retained on the 4.75mm sieve (g):	409.1	Total Losses (%): (Maximum 0.3%)	0.00
Total Mass passing the 4.75 mm sieve (g):	3038.3	Percent Crushed: (Min. 60% - Gran A)	
Percent Coarse Aggregate:	11.87	Not Applicable - Gran. "B" Type 1	_
Percent Fine Aggregate:	88.13	Asphalt Coated Particles (%) (Max. 30%)	-

TOTAL SAMPLE PERCENTAGES					COARSE AND FINE PORTION PERCENTAGES			
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	-	-	-	-	150	-	-	
26.5	100.0	100	100	Υ	26.5	0.0	-	
19.0	99.6	85	100	Υ	19.00	3.7	-	
13.2	98.6	65	90	N	13.2	12.0	-	
9.5	96.9	50	73	N	9.5	25.7	-	
4.75	88.1	35	55	N	4.75	100.0	-	
1.18	59.6	15	40	N	1.18	-	32.4	
0.30	33.9	5	22	N	0.30	-	61.5	
0.15	-	1	-	-	0.15	-	-	
0.075	15.8	2	8	Ν	0.075	-	82.1	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'A'



GRAIN SIZE DISTRIBUTION REPORT GRANULAR 'B' TYPE I



 Project Name:
 9th Avenue East

 Project No.:
 2201530

 Client:
 Tatham Engineering Limited

Client: Tatham Engineering Limited
Supplier: -

Sampled From: BH16, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

 GEI Lab No.
 5238

 Figure No.
 B6

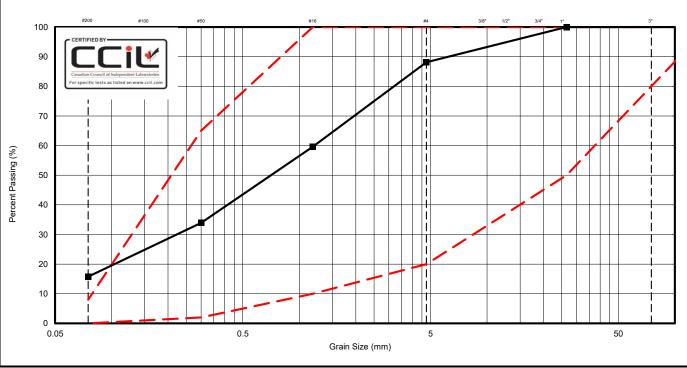
SAMPLE DATA

Total Mass of Sample (g):	3447.4	% Passing 75um by washing:	15.31
Total Mass retained on the 4.75mm sieve (g):	409.1	Total Losses (%): (Maximum 0.3%)	0.00
Total Mass passing the 4.75 mm sieve (g):	3038.3	Percent Crushed: (Min. 60% - Gran A)	N/A
Percent Coarse Aggregate:	11.87	Not Applicable - Gran. "B" Type 1	IN/A
Percent Fine Aggregate:	88.13	Asphalt Coated Particles (%) (Max. 30%)	-

	TOTAL SAMPLE PERCENTAGES					COARSE AND FINE PORTION PERCENTAGES			
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **		
150	100.0	100	100	Υ	150	0.0	-		
26.5	100.0	50	100	Υ	26.5	0.0	-		
19.0	-	-	-	-	19.00	-	-		
13.2	-	-	-	-	13.2	-	-		
9.5	-	-	-	-	9.5	-	-		
4.75	88.1	20	100	Υ	4.75	100.0	-		
1.18	59.6	10	100	Υ	1.18	-	32.4		
0.30	33.9	2	65	Υ	0.30	-	61.5		
0.15	-	-	-	-	0.15	-	-		
0.075	15.8	0	8	N	0.075	-	82.1		

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'B' Type I



GRAIN SIZE DISTRIBUTION REPORT GRANULAR A



 Project Name:
 9th Avenue East

 Project No.:
 2201530

 Client:
 Tatham Engineering Limited

Supplier: -

Sampled From: BH22, AS1, 0-2'

Date Sampled: -

Date Tested: March 20, 2023

 GEI Lab No.
 5239

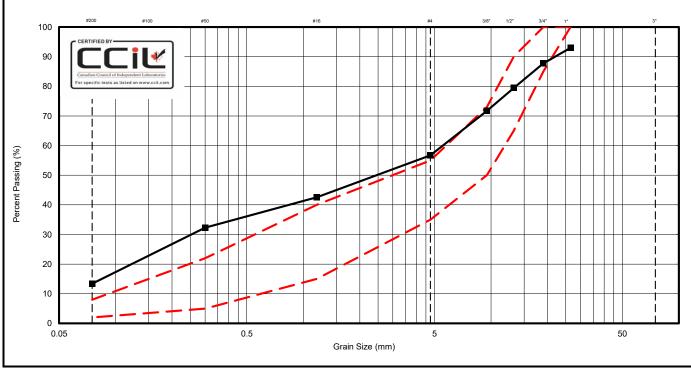
 Figure No.
 B7

Total Mass of Sample (g):	2341	% Passing 75um by washing:	13.06
Total Mass retained on the 4.75mm sieve (g):	1013.6	Total Losses (%): (Maximum 0.3%)	0.00
Total Mass passing the 4.75 mm sieve (g):	1327.4	Percent Crushed: (Min. 60% - Gran A)	
Percent Coarse Aggregate:	43.30	Not Applicable - Gran. "B" Type 1	-
Percent Fine Aggregate:	56.70	Asphalt Coated Particles (%) (Max. 30%)	-

	TOTAL SAMPLE PERCENTAGES					COARSE AND FINE PORTION PERCENTAGES			
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **		
150	-	-	-	-	150	-	-		
26.5	93.0	100	100	Ν	26.5	16.1	-		
19.0	87.8	85	100	Υ	19.00	28.2	-		
13.2	79.5	65	90	Υ	13.2	47.5	-		
9.5	71.7	50	73	Υ	9.5	65.4	-		
4.75	56.7	35	55	N	4.75	100.0	-		
1.18	42.6	15	40	N	1.18	-	24.9		
0.30	32.3	5	22	N	0.30	-	43.1		
0.15	-	-	-	-	0.15	-	-		
0.075	13.4	2	8	Ν	0.075	-	76.3		

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'A'



GRAIN SIZE DISTRIBUTION REPORT GRANULAR 'B' TYPE I



 Project Name:
 9th Avenue East

 Project No.:
 2201530

 Client:
 Tatham Engineering Limited

 GEI Lab No.
 5239

 Figure No.
 B8

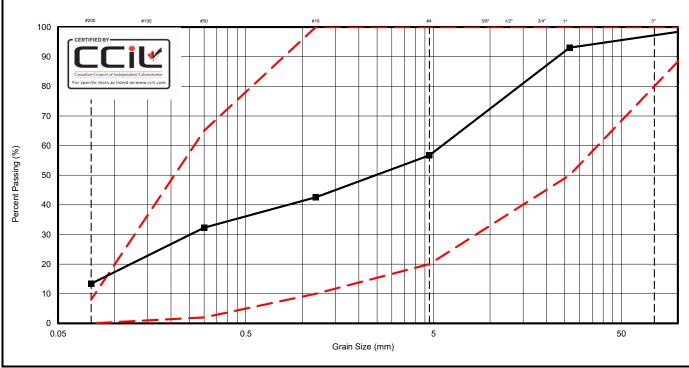
SAMPLE DATA

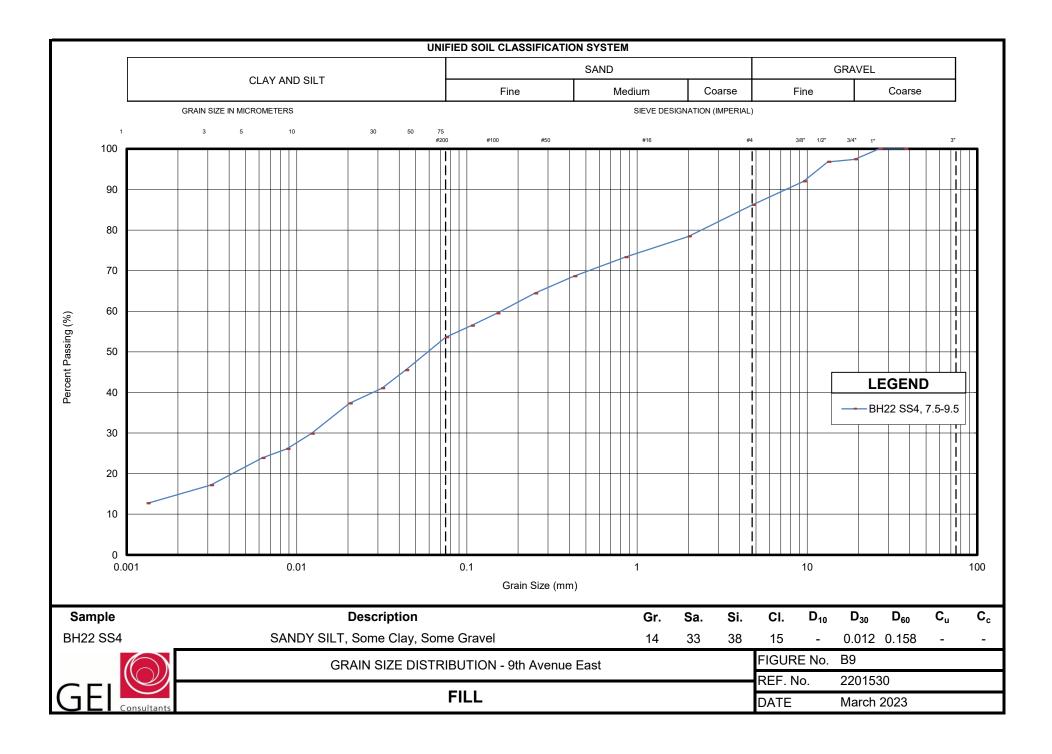
Total Mass of Sample (g):	2341	% Passing 75um by washing:	13.05
Total Mass retained on the 4.75mm sieve (g):	1013.6	Total Losses (%): (Maximum 0.3%)	0.00
Total Mass passing the 4.75 mm sieve (g):	1327.4	Percent Crushed: (Min. 60% - Gran A)	N/A
Percent Coarse Aggregate:	43.30	Not Applicable - Gran. "B" Type 1	IN/A
Percent Fine Aggregate:	56.70	Asphalt Coated Particles (%) (Max. 30%)	-

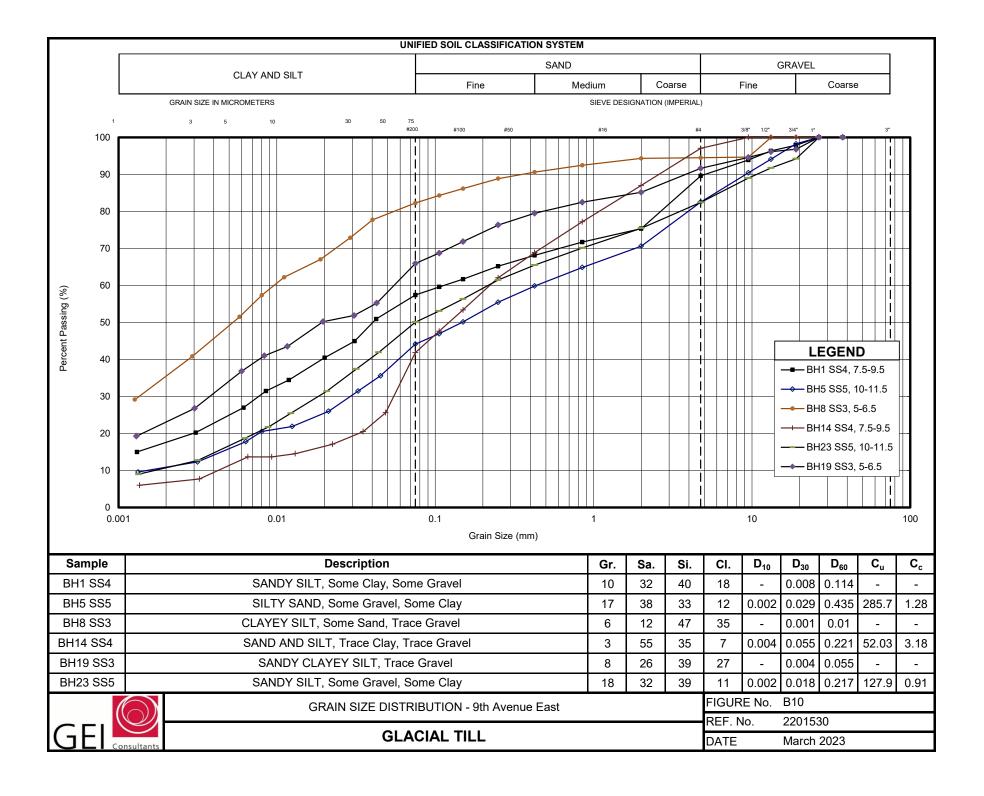
	TOTAL SAM	PLE PERCENTA	AGES		COARSE AND FINE PORTION PERCENTAGES			
Sieve Size (mm)	Percent Passing	Min Spec. (%)	Max Spec. (%)	Pass?	Sieve Size	Percent Retained *	Percent Retained **	
150	100.0	100	100	Υ	150	0.0	-	
26.5	93.0	50	100	Υ	26.5	16.1	-	
19.0	-	-	-	-	19.00	-	-	
13.2	-	-	-	-	13.2	-	-	
9.5	-	-	-	-	9.5	-	-	
4.75	56.7	20	100	Υ	4.75	100.0	-	
1.18	42.6	10	100	Υ	1.18	-	24.9	
0.30	32.3	2	65	Υ	0.30	-	43.1	
0.15	-	1	-	-	0.15	-	-	
0.075	13.4	0	8	N	0.075	-	76.3	

* Based on Coarse Portion only ** Based on Fine Portion only

Material Does Not Meet OPSS.MUNI 1010 Specifications for Granular 'B' Type I









Atterberg Limits Report

Project Name: 9th Avenue East

Project No.: 2201530

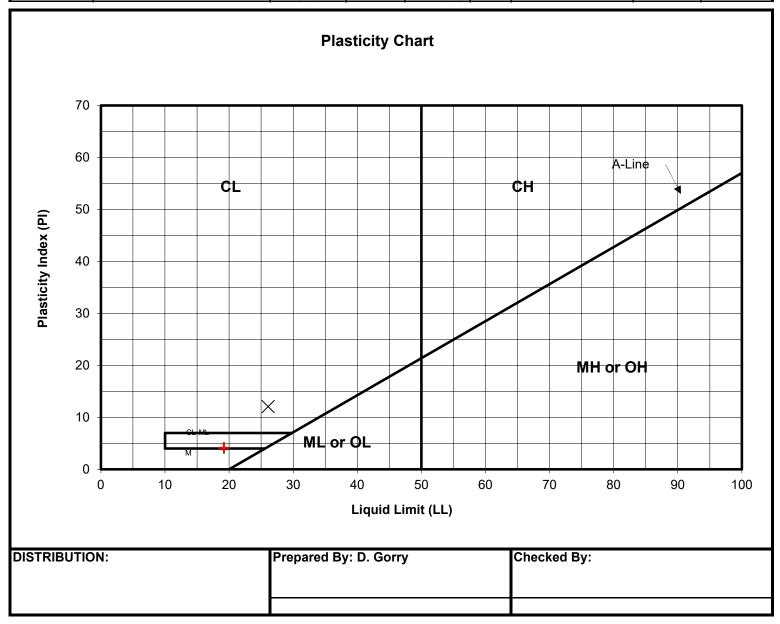
Client: Tatham Engineering Limited

Figure No.: B11

Date Tested: March 20, 2023

Date Sampled: -

	0 0				•					
	SAMPLE INFORMATION									
SAMPLE ID	BH8 SS3, 5-6.5	LIQUID LIMIT (LL):	26.1	PLASTIC LIMIT (PL)	14.1	PLASTIC INDEX (PI)	12.0	X		
SAMPLE ID	BH22 SS4, 7.5-9.5	LIQUID LIMIT (LL):	19.2	PLASTIC LIMIT (PL)	15.1	PLASTIC INDEX (PI)	4.1	+		



Report No.	

Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

Appendix C

Corrosivity Laboratory Testing Results



CERTIFICATE OF ANALYSIS

Final Report

C.O.C.: --- REPORT No. B23-01723

Rev. 2

Report To:

GEI Consultants

647 Welham Rd, Unit 14, Barrie ON L4N 0B7 Canada **Attention:** Matthew Hobson

DATE RECEIVED: 07-Feb-23

DATE REPORTED: 20-Mar-23

SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories

112 Commerce Park Drive

Barrie ON L4N 8W8

Tel: 705-252-5743

Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER: 2201530

WATERWORKS NO.

			Client I.D.		BH14-SS2	BH14-SS4	BH20-SS2	BH23-SS4
			Sample I.D.		B23-01723- 16	B23-01723- 17	B23-01723- 20	B23-01723-23
			Date Collecte	ed	03-Feb-23	03-Feb-23	30-Jan-23	31-Jan-23
Parameter	Units	R.L.	Reference Method	Date/Site Analyzed				
pH @25°C	pH Units		MOEE3530	10-Feb-23/R	7.81	7.92	7.50	7.97
Conductivity @25°C	mS/cm	0.001	SM 2510B	14-Feb-23/O	0.201	0.293	0.198	0.131
Resistivity	ohms-cm		SM 2510B	20-Mar-23/O	4970	3420	5060	7620
Chloride	μg/g	5	SM4110C	13-Feb-23/O	55	50	9	12
Sulphate	μg/g	10	SM4110C	13-Feb-23/O	< 10	180	< 10	30
Sulfide	μg/g	0.3	In-House	16-Feb-23	< 0.3	< 0.3	< 0.3	1 < 0.3 1
REDOX potential	mV		In-House	14-Feb-23/R	413	203	264	256

¹ Subcontracted to Testmark Labs

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an * Site Analyzed=K-Kingston,W-Windsor,O-Ottawa,R-Richmond Hill,B-Barrie

Christine Burke Lab Manager

² Revised report to include resistivity reuslts as per client request



CERTIFICATE OF ANALYSIS

Final Report

C.O.C.: --- REPORT No. B23-01723

Rev. 2

Report To:

GEI Consultants 647 Welham Rd, Unit 14,

Barrie ON L4N 0B7 Canada

Attention: Matthew Hobson

DATE RECEIVED: 07-Feb-23

DATE REPORTED: 20-Mar-23

SAMPLE MATRIX: Soil

Caduceon Environmental Laboratories

112 Commerce Park Drive

Barrie ON L4N 8W8

Tel: 705-252-5743

Fax: 705-252-5746

JOB/PROJECT NO.:

P.O. NUMBER: 2201530

WATERWORKS NO.

			Client I.D.		BH25-SS2			
			Sample I.D.		B23-01723-			
					25	1	1	
			Date Collecte	ed	31-Jan-23			
Parameter	Units	R.L.	Reference Method	Date/Site Analyzed				
pH @25°C	pH Units		MOEE3530	10-Feb-23/R	7.59			
Conductivity @25°C	mS/cm	0.001	SM 2510B	14-Feb-23/O	0.173			
Resistivity	ohms-cm		SM 2510B	20-Mar-23/O	5770			
Chloride	μg/g	5	SM4110C	13-Feb-23/O	9			
Sulphate	μg/g	10	SM4110C	13-Feb-23/O	10			
Sulfide	μg/g	0.3	In-House	16-Feb-23	< 0.3			
REDOX potential	mV		In-House	14-Feb-23/R	269			

¹ Subcontracted to Testmark Labs

R.L. = Reporting Limit

Test methods may be modified from specified reference method unless indicated by an * Site Analyzed=K-Kingston,W-Windsor,O-Ottawa,R-Richmond Hill,B-Barrie

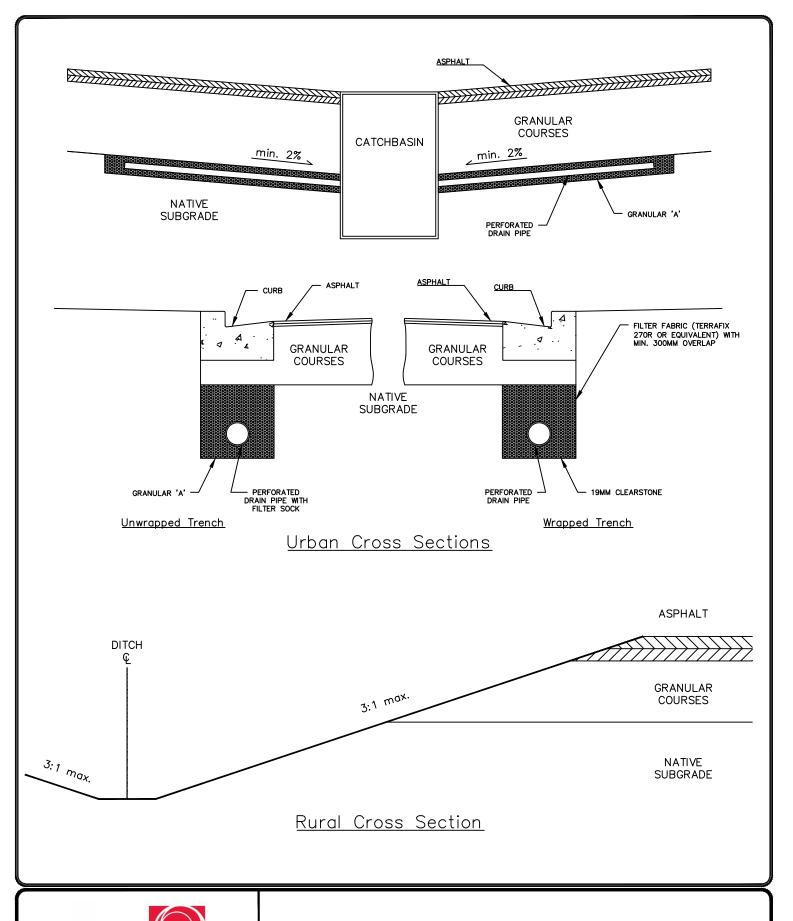
Christine Burke Lab Manager

² Revised report to include resistivity reuslts as per client request

Geotechnical Investigation, Proposed Watermain Replacement and Road Reconstruction 9th Avenue East, Owen Sound, ON Project No. 2201530, March 24, 2023

Appendix D

Typical Details





PAVEMENT DRAINAGE ALTERNATIVES
TYPICAL DETAILS

Appendix F: Hydrogeological Assessment Report



Enhancing our communities



9th Avenue East Watermain Replacement and Road Reconstruction

HYDROGEOLOGICAL ASSESSMENT

City of Owen Sound

Document Control

File: Prepared by: Prepared for:

121387 Tatham Engineering Limited City of Owen Sound

115 Sanford Fleming Drive, Suite 200 808 2nd Avenue East

Date: Collingwood, Ontario L9Y 5A6 Owen Sound, Ontario N4K 2H4

May T 705-444-2565 11, 2023 tathameng.com

Authored by:	Reviewed by:
	ALICIA KIMBERLEY PRACTISING MEMBER 2949 May 11, 2023 ON T A R 10
Kimberly Gardner, B.Eng., EIT	Alicia Kimberley, MSc. P.Geo.
Engineer Intern	Team Leader - Hydrogeology

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Issue	Date	Description
1	May 11, 2023	Final Report

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1 Introduction

Tatham Engineering Limited (Tatham) has been retained by the City of Owen Sound (City) to complete a Hydrogeological Investigation for the proposed watermain replacement and road reconstruction of 9th Avenue East, in Owen Sound, Ontario.

The proposed watermain replacement and road reconstruction program will be completed in three Phases of construction:

- Phase 1 consists of the replacement of approximately 650 m of existing watermain along 6th
 Street East, and within the utility corridor from 6th Street East to 8th Street East.
- Phase 2 consists of new watermain installation extending approximately 420 m through a utility corridor from 6th Street East to Superior Street, replacement and upsizing of approximately 280 m of watermain along Superior Street from the corridor to approximately 160 m west of 9th Avenue East.
- Phase 3 consists of the replacement of approximately 1,000 m of watermain along 9th Avenue East from Superior Street to just north of 9th Street East. Approximately 140 m of existing clay sanitary sewer will also be replaced during the proposed reconstruction along 9th Avenue East north of 7th Street East, and approximately 865 m of existing storm sewers may be replaced along 9th Avenue East between 9th Street East and Superior Street.

It is understood Phase 1 is to be carried out in 2023 and Phase 2 and 3 will be carried out at a later date. A site location plan and site layout illustrating the three Phases are enclosed as Figures 1 and 2, respectively.

The geotechnical investigation for the project has been completed by GEI (2023) and has been relied upon for the hydrogeological assessment.

1.1 PURPOSE AND SCOPE OF WORK

The main objectives of the Hydrogeological Investigation were to:

- Establish local and regional geology and hydrogeology.
- Determine potential construction dewatering requirements and provide an assessment of anticipated construction dewatering flow rates for a generic construction scenario.
- Assess groundwater quality and compare the results to the applicable City of Owen Sound Sewer Use By-Law Criteria, Provincial Water Quality Objectives (PWQO), and O.Reg.153/04, as amended, Table 1 Site Condition Standards.



- Qualitatively assess the potential impacts to the nearby structures, water bodies and water uses, if any, and comment on future regulatory agency involvement.
- Prepare a Hydrogeological Investigation report.

To achieve the above objectives, Tatham proposed the following scope of work:

- Complete a desktop review of pertinent geological and hydrogeological resources, Ministry
 of the Environment, Conservation and Parks (MECP) water well records, previous
 geotechnical reports completed by others, and proposed site plan drawings.
- Visit the site to note existing site conditions, topography, drainage, water features, neighboring land uses, and/or existing water supply or monitoring wells.
- Complete groundwater level monitoring of all accessible and functional wells installed onsite during the 2023 geotechnical investigation completed by GEI.
- Perform borehole permeability testing at selected monitoring wells to determine hydraulic conductivity of the screen soil deposits.
- Determine baseline groundwater quality by collecting and analysis of one representative groundwater sample.
- Evaluate the background information, field, and laboratory data to evaluate the construction dewatering requirements.
- Prepare a Hydrogeological Investigation report.

1.2 WATER TAKING - TEMPORARY

Temporary construction dewatering is governed by the Environmental Protection Act, and the following water taking limits and requirements are outlined in O.Reg.63/16:

- Construction dewatering less than 50,000 L/day: the taking of both groundwater and stormwater does not require a hydrogeological report nor a water taking permit.
- Construction dewatering greater than 50,000 L/day but less than 400,000 L/day: the taking
 of both groundwater and stormwater does require a hydrogeological report and registration
 on the Environmental Activity and Sector Registry (EASR).
- Construction dewatering greater than 400,000 L/day: the taking of groundwater and stormwater requires a hydrogeological report and an approved MECP Category 3 Permit-To-Take-Water (PTTW).



This hydrogeological assessment was carried out to assess the potential construction dewatering volumes to proceed in accordance with the applicable water taking regulatory requirements and to obtain the applicable water taking permit.



2 Site Setting

The site is comprised of municipal roadway including 9th Avenue East from Superior Street to just north of 9th Street East, the western portion of 6th Street East from the corridor to the western limit, and Superior Street from the utility corridor to about 160 m west of 9th Avenue East as well as two utility corridors. The site is located in a mixed residential, commercial and industrial setting, with primarily residential properties to the north, west and south, and commercial and industrial land uses to the east.

2.1 PHYSIOGRAPHY, SURFICIAL AND BEDROCK GEOLOGY

Most of the site lies within the physiographic region known as the Cape Rich Steps comprising of shale plains, and the southern portion of the site lies within the physiographic region known as the Bruce Peninsula comprising of limestone plains (Chapman and Putnam, 1984). Ontario Geological Survey (OGS) quaternary geology mapping indicates the site consists primarily of glaciolacustrine deposits comprised of sand, gravelly sand and gravel. OGS surficial geology mapping indicates the site consists primarily of Till comprised of stone-poor sandy silt to silty sand texture till on Paleozoic terrain; however, the southern portion is mapped as bedrock. These findings are generally consistent with the subsurface conditions encountered during GEI's 2023 geotechnical investigation where sandy silt/sand overburden soils were encountered and bedrock was encountered towards the southern portion of the site. Local clayey silt to silty clay till was also encountered

The bedrock at the site primarily consists of Cabot Head shale, Manitoulin/Cabot Head/Fossil Hill dolostone of the Clinton-Cataract Group, or Amabel Dolostone. Bedrock was encountered during the geotechnical investigation towards the southern portion of the site at depths of 1.5 to 3.5 m below existing grade.

2.2 TOPOGRAPHY AND DRAINAGE

The topography of the site includes rolling hills with elevations ranging from 230 meters above sea level (m asl) to 265 m asl. Drainage and runoff is expected to follow the local topography towards the existing storm sewers throughout the roadway and to lower lying areas grassed areas within the utility corridors. It is anticipated regional groundwater flow will be to the northwest towards Georgian Bay.

2.3 MECP WATER WELL RECORDS

To assess the nature of the groundwater resources as well as the history of the current well usage in the area, MECP water well records were reviewed for a 500 m radius surrounding the site. The



approximate MECP water well locations are shown on Figure 3, and a summary of the MECP water well records are provided in Appendix A.

A total of 32 MECP well records were reviewed within a 500 m boundary of the site. Six of the water well records indicated domestic or commercial water supply use, 15 records indicated test hole and monitoring well use, two records indicated the wells were not in use, and the remaining water well records did not specify water well use.

In general, the well records indicated subsurface layers of sand, silt and clay overlying limestone or shale bedrock. Bedrock was noted at depths of 1.5 to 18.3 m below existing grade.

2.4 SOURCE WATER PROTECTION MAPPING

The site is located in the Grey Sauble Source Protection Area (SPA). The site does not lie within a Municipal Well Head Protection Area (WHPA); however, the northern portion of the site does lie within an Intake Protection Zone (IPZ), as shown on Figures 4 and 5. The southern boundary of the site borders a Significant Groundwater Recharge Area (SGRA) and the entire site lies within a Highly Vulnerable Aguifer (HVA), as shown on Figures 6 and 7, respectively.

2.5 SITE INSPECTION

A visual site inspection was completed on April 21, 2023. The site was primarily comprised of municipal roadways, and two grassed utility corridors. The topography was hilly throughout the site, and the site was surrounded by residential properties to the north, west and south, and industrial and commercial land uses to the east.

No water bodies were noted to cross the site. Georgian Bay is approximately 1.5 km north of the site and the Sydenham River lies approximately 1.3 km west of the site.



3 Procedures and Methodology

Boreholes (BH1 through BH25) were advanced during the geotechnical investigation (GEI, 2023). Monitoring wells were installed in 11 of the boreholes (BH/MWs 1, 3, 5, 7, 9, 14, 17, 19, 21, 23 and 25).

The geotechnical borehole logs and laboratory testing are discussed further in section 4.1 and are provided in Appendix B and C, respectively.

3.1 BOREHOLE PERMEABILITY TESTING

Borehole permeability testing was completed in three monitoring wells (BH/MWs 21, 23 and 25) on April 21, 2023. Water was purged from the well using low density polyethylene (LDPE) tubing and a foot valve. Following the removal of three well volumes of groundwater or the well going dry, and after 95% recovery, the test was initiated. The static water level was measured prior to the start of the testing and the change in water level was manually recorded following purging. The change in water level was recorded on regular intervals for a total of 30 minutes. The test was completed to estimate the hydraulic conductivity (K) of the soils at the well screen depth. The plot for drawdown versus time is presented in Appendix D.

3.2 GROUNDWATER SAMPLING

To establish baseline conditions and assess the suitability for discharge of pumped groundwater to surface during potential construction dewatering, a representative groundwater sample was collected from BH/MW25 on April 21, 2023.

The sample was collected using low-flow sampling methods to reduce sediment content within the sample. The sample was directly placed into pre-cleaned laboratory-supplied vials and/or bottles, with analytical test group specific preservatives. Dedicated nitrile gloves were used during sampling and non-dedicated equipment was sanitized between monitoring wells.

Samples were field filtered for select parameters and submitted for chemical analysis of the City of Owen Sound Sewer Use By-Law Criteria, PWQO metals, and O.Reg. 153/04, as amended, Petroleum Hydrocarbons (PHCs) and Volatile Organic Compounds (VOCs). Samples were analyzed by Caduceon Environmental Laboratories, a CALA accredited lab. Groundwater chemistry results are included in the laboratory Certificates of Analysis, provided in Appendix E.



4 Subsurface Conditions

The Geotechnical Investigation (GEI, 2023) was reviewed for this study. The borehole and monitoring well locations are shown on Figure 2, detailed subsurface borehole logs are presented in Appendix B, and the geotechnical laboratory results are included in Appendix C.

In general, the boreholes encountered pavement structure or topsoil, over a silty sand to clay silt/sandy clayey silt fill, over a glacial till comprising of sandy silt, sand and silt, silty sand and locally clayey silt to sandy clayey silt.

Towards the southern portion of the site borehole drilling refusal at depths of 1.5 to 3.5 m below existing grade was interpreted as probable bedrock.

4.1 GROUNDWATER

4.1.1 Groundwater Levels

Unstabilized groundwater level measurements and cave measurements were taken upon drilling completion of each borehole in 2023, as presented in the borehole logs in Appendix B. These measurements provide a rough estimate of the possible excavation and temporary groundwater control constructability considerations that may arise. Upon completion of the boreholes, all boreholes were open and almost all boreholes were dry upon completion; with the exception of BH/MW7 and BH10 where water was noted at 4.4 m and 0.8 m, respectively.

Monitoring wells were installed in 11 boreholes (BH/MWs 1, 3, 5, 7, 9, 14, 17, 19, 21, 23 and 25) to facilitate measurements of stabilized groundwater levels across the site. The monitoring wells were installed with 50-mm PVC riser pipe and slotted 1.5-meter-long screens. A summary of the monitoring well installations is presented in Table 1. Stabilized groundwater measurements are presented in Table 2.

Table 1: Monitoring Well Installation Details

MONITORING	GROUND	LOCATION	STRATA	
WELL ID	SURFACE	Depth (m)	Elevation (m asl)	SCREENED
BH/MW1	234.4	3.1 - 4.6	229.8 - 231.3	Sandy Silt Glacial Till
BH/MW3	242.7	3.1 - 4.6	238.1 - 239.6	Silty Sand Fill to Sandy Silt Till
BH/MW5	237.1	3.1 - 4.6	232.5 - 234.0	Silty Sand Glacial Till



MONITORING	GROUND	LOCATION	STRATA	
WELL ID	LL ID SURFACE Depth (n		Elevation (m asl)	SCREENED
BH/MW7	233.7	3.1 - 4.6	229.1 - 230.6	Sandy Clayey Silt Glacial Till
BH/MW9	237.3	3.1 - 4.6	232.7 - 234.2	Sandy Silt Glacial Till
BH/MW14	248.8	1.6 - 3.1	245.7 - 247.2	Sandy Silt to Sand and Silt Glacial Till
BH/MW17	262.7	0.9 - 2.4	260.3 - 261.8	Clayey Silt Fill to Sandy Silt Glacial Till
BH/MW19	249.2	1.6 - 3.1	246.1 - 247.6	Sandy Clayey Silt Glacial Till
BH/MW21	245.2	0.8 - 2.3	242.9 - 244.4	Clayey Silt Fill to Sandy Silt
BH/MW23	247.3	1.6 - 3.1	244.2 - 245.7	Sandy Silt Glacial Till
BH/MW25	248.3	1 - 2.5	245.8 - 247.3	Sandy Silt Glacial Till

Table 2: Groundwater Levels

MONITORING WELL ID	GROUNDWATER DEPTH (M) / ELEVATION (m asl)			
MONITORING WELL ID	FEBRUARY 13, 2023	APRIL 21, 2023		
BH/MW1	Dry	_*		
BH/MW3	Dry	_*		
BH/MW5	3.2 / 233.9	_*		
BH/MW7	1.4 / 232.3	_*		
BH/MW9	1.8 / 235.5	_*		
BH/MW14	0.6 / 248.2	_*		



MONITORING WELL ID	GROUNDWATER DEPTH (M) / ELEVATION (m asl)			
	FEBRUARY 13, 2023	APRIL 21, 2023		
BH/MW17	Dry	Dry		
BH/MW19	1.7 / 247.5	1.76 / 247.4		
BH/MW21	1.3 / 243.9	1.22 / 244.0		
BH/MW23	0.1 / 247.2	-0.07** / 247.4		
BH/MW25	0.2 / 248.1	0.21 / 248.1		

Note:

Stabilized groundwater levels on February 13, 2023 ranged from 0.1 to 3.2 m below exiting grade (elevation 232.2 to 248.2 m asl). Local groundwater flow is anticipated to flow to the northwest/west towards Georgian Bay and/or Syndenham River as shown on Figure 8.

4.2 IN-SITU PERMEABILITY

Borehole permeability testing was conducted at BH/MWs 21, 23 and 25 and the hydraulic conductivities were calculated using Dagan (1978) solution which accounts for the groundwater table straddling the well screen. The semi-log plot for drawdown versus time is provided in Appendix D and summarized in Table 3, below.

Table 3: Hydraulic Conductivity

MONITORING WELL ID	WELL DEPTH (m)	STRATA SCREENED	HYDRAULIC CONDUCTIVITY (m/s)
BH/MW21	2.3	Clayey Silt Fill to Sandy Silt	1.5×10 ⁻⁶
BH/MW23	3.1	Sandy Silt Glacial Till	2.2×10 ⁻⁷
BH/MW25	2.5	Sandy Silt Glacial Till	4.3x10 ⁻⁷

According to Freeze and Cherry (1979), the typical hydraulic conductivity of the strata investigated are:

Glacial Till: 10⁻⁶ m/s to 10⁻¹² m/s

Silt: 10⁻⁶ m/s to 10⁻⁹ m/s

• Silty Sand: 10^{-3} m/s to 10^{-7} m/s



^{*} Monitoring well could not be safely accessed and groundwater level was unable to be collected.

^{**}value indicates water level measured above the ground surface.

The actual measured hydraulic conductivity of the deposits generally, were within the expected range; however, for design purposes the hydraulic conductivity was assumed to be $1.5 \times 10^{-6} \, \text{m/sec}$.

4.3 **BASELINE GROUNDWATER CHEMISTRY**

To establish baseline conditions and assess the suitability for discharge of pumped groundwater to surface during potential future construction dewatering, a groundwater sample was collected and analyzed for select parameters.

The groundwater sample met the Owen Sound Storm Sewer ByLaw Criteria for the parameters tested with the exception of Total Suspended Solids with a measured concentration of 32 mg/L compared to a Sewer Use Bylaw Criteria of 15 mg/L. Similarly, the groundwater sample met the PWQO and O.Reg. 153/04 (as amended) Table 1 Site Condition Standards for the parameters tested with the exception of Iron with a measured concentration of 1,160 μg/L compared to a PWQO of 300 µg/L. It is noted the E.Coli and pesticides were not tested for as part of the Owen Sound Sewer ByLaw testing.

The above chemical results suggest the dewatering discharge may not meet the applicable Owen Sound Storm Sewer Use By-Law Criteria and PWQO during construction dewatering without first being discharged to a silt bag and/or sediment tank before being discharged to the land surface. Treatment of dewatering discharge water by filtration or sedimentation to reduce the concentration of TSS will likely reduce the concentration of non-dissolved metals to achieve compliance with the PWQO; however, other treatment methods may be required still to reduce the concentration of dissolved analytes.

It is expected during dewatering pumped, water will first be discharged to a silt bag and/or sediment tank at minimum before being discharged to land and/or storm sewer.



5 Discussion and Analysis

It is understood the proposed watermain replacement and road construction will occur in three Phases of construction:

- Phase 1 consists of the replacement of approximately 650 m of existing watermain along 6th
 Street East, and within the utility corridor from 6th Street East to 8th Street East.
- Phase 2 consists of new watermain installation extending approximately 420 m through a utility corridor from 6th Street East to Superior Street, replacement and upsizing of approximately 280 m of watermain along Superior Street from the corridor to approximately 160 m west of 9th Avenue East.
- Phase 3 consists of the replacement of approximately 1,000 m of watermain along 9th Avenue East from Superior Street to just north of 9th Street East. Approximately 140 m of existing clay sanitary sewer will also be replaced during the proposed reconstruction along 9th Avenue East north of 7th Street East, and approximately 865 m of existing storm sewers may be replaced along 9th Avenue East between 9th Street East and Superior Street.

Based on the current design details it is assumed watermain inverts will be approximately 2.5 m bgs and the proposed storm and sanitary sewers inverts will be approximately 3.5 m bgs.

It is anticipated construction dewatering will be required during the construction works.

5.1 TEMPORARY CONSTRUCTION DEWATERING

To calculate the estimated dewatering rate for the proposed on-site construction works, the following assumptions have been made:

- Groundwater is to be drawn down 1.0 m below the anticipated excavation depths.
- The water-bearing soils that may be exposed during construction primarily consist of sandy silt glacial till with variable clay contents, with an assumed K-value of 1.5x10⁻⁶ m/s for calculation purposes.
- Saturated soils will be encountered from depths ranging from surface to 2.8 m below existing grade (Elevation 232.2 to 248.2m asl).
- The excavation depths for the Phase 1 construction zone are inferred from the 9th Avenue East Looping Watermain Phase 1 Tender Design drawings dated March 2023 prepared by Tatham and are expected to range between 2.0 to 2.5 m below the existing ground surface. At the time of this report the design details for Phase 2 and 3 were not available and for



design purposes watermain inverts were assumed to be similar to those proposed within Phase 1, and up to 3.5 m for the proposed sanitary and/or storm sewer inverts.

- For calculation purposes the site has been separated into three zones based on the proposed phasing; however, the dewatering contractor may use smaller dewatering zones to limit the dewatering discharge rates.
- It is assumed all measures will be implemented to ensure the 400,000 L/day EASR threshold will not be exceeded. This includes completing the work in smaller sections.

5.1.1 Radius of Influence

The Radius of Influence (ROI) for construction dewatering refers to the distance at which the drawdown resulting from pumping becomes negligible. The ROI is calculated using the empirical Sichardt Equation. The equation is empirical and provides representative flow rates using the steady state flow dewatering equations. The Sichardt Equation is used to provide representative flow calculations; however, it is not precise in determining the actual radius influence by pumping since during steady state conditions, the ROI of pumping will extend until boundary flow conditions are reached and provide sufficient water inputs to the aquifer, such as recharge and surface water bodies.

The Sichardt equation is expressed as the following equation:

$$R_o = 3000(H - h)\sqrt{K}$$

Where:

K = hydraulic conductivity (m/s)

H = Static Saturated Head (m)

h = Dynamic Saturated Head (m)

Ro= Radius of Influence (m)

Based on the Sichardt equation and the design K value, the ROI from the centre of the excavation for radial flow for each zone is tabulated below. Calculation details are provided in Appendix F and the locations of the Zones 1, 2 and 3 are shown on Figure 2.

Table 4: Radius of Influence

ZONE	DESCRIPTION	ROI (m)
1	Phase 1	13
2	Phase 2	11



ZONE	DESCRIPTION	ROI (m)
3	Phase 3	8

The ROI calculation is a conservative methodology. It should be noted most of the water will be pumped during the first stage of construction or when a rain event occurs.

Although the ROI is calculated as 8 to 13 m from the centre of the excavation, over a period of time, the amount of settlement will decrease exponentially to zero towards the ROI limit. The likelihood for impacts to the nearby structures are negligible given the distance of the neighbouring dwellings and the anticipated excavations; however, a settlement analysis should be completed by the geotechnical engineer prior to construction dewatering activities.

5.1.2 **Temporary Dewatering Flow Rate Equation**

The Dupuit method for linear flow in an unconfined aquifer for a fully penetrating excavation was used within Zone 1, 2 and 3 and is expressed as:

$$Q = Kx \frac{H^2 - h^2}{L_0}$$

Where:

Q = rate of pumping (m^3/s)

x = length of excavation (m)

L = length of excavation (m)

K = hydraulic conductivity (m/s)

H = head beyond the influence of pumping (static groundwater elevation) (m)

h = head above base of aguifer at the excavation (m)

It is anticipated the initial dewatering rate will be higher to remove groundwater from within the overburden formation. As the water level reaches its target elevation, dewatering rates are expected to decrease as the local groundwater storage will have been removed and lessen seepage rates into the excavation.

Using the assumptions and equations outlined above, the estimated dewatering rates were determined and summarized below. Calculation details are provided in Appendix F.



Table 5: Construction Dewatering Estimated Daily Flow Rate

ZONE	DESCRIPTION	CONSTRUCTION DEWATERING FLOW RATE (L/day)	CONSTRUCTION DEWATERING FLOW RATE INLCUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT (L/day)	CONSTRUCTION DEWATERING FLOW RATE INCLUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT PER 100 m LENGTH TRENCH (L/day/100 m)
1	Phase 1	165,100	356,200	54,800
2	Phase 2	175,900	386,200	44,900
3	Phase 3	162,300	364,600	36,460

To account for seasonal fluctuations of the groundwater table and variation in the hydrogeological properties beyond those encountered during this study, a safety factor of 2.0 was applied. Further to account for surface water infiltration within the excavation footprint, a 10 mm rain event was applied. This rate can be considered a contingency volume subject to the timing and season of construction.

The estimates provided in this report are based on proposed reconstruction information available at the time of the investigation. If design changes are implemented, additional dewatering estimation will be required to reflect the design changes.

The estimated dewatering volumes range between 356,200 and 386,200 L/day; however, it is anticipated construction will be completed in smaller sections. Considering typical construction practices dewatering volumes are anticipated to range between 36,460 and 54,800 L/day per 100 m length of trench. As the estimated dewatering rates are over 50,000 L/day but remain below 400,000 L/day it is recommended the anticipated water taking be registered on the MECP EASR.

In accordance with O.Reg. 63/19 a water taking and discharge plan have been prepared for the site and are provided in Appendix G and H, respectively.

It is the responsibility of the contractor to ensure dry conditions are maintained within excavations at all times. If dewatering does exceed the 400,000 L/day volume during construction, a PTTW with the MECP will be required. Dewatering volumes should be closely monitored during construction in order to stay below the threshold of 400,000 L/day which may require construction being carried out in smaller sections.

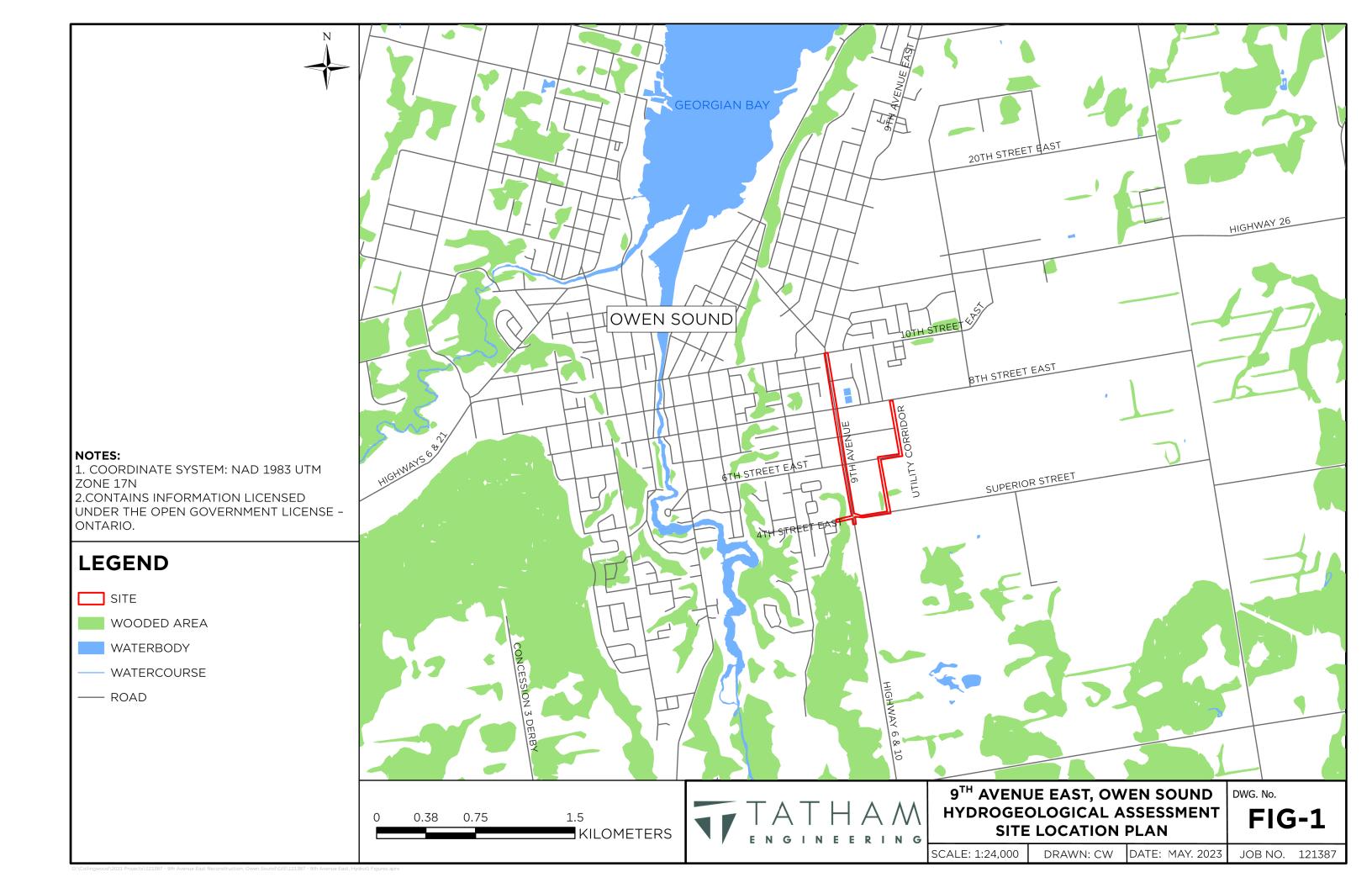


References 6

Chapman, L.J. and Putnam, D.F. 2007. The Physiography of Southern Ontario; Ontario Geological Survey, Miscellaneous Release - Data 228.

GEI Consulting Engineers and Scientists. March 24, 2023. Proposed Watermain Replacement and Road Reconstruction, 9th Avenue East, Owen Sound, Ontario.







NOTES:

1. COORDINATE SYSTEM: NAD 1983 UTM ZONE 17N

2.CONTAINS INFORMATION LICENSED UNDER THE OPEN GOVERNMENT LICENSE - ONTARIO.

LEGEND

♦ MONITORING WELL, 2023

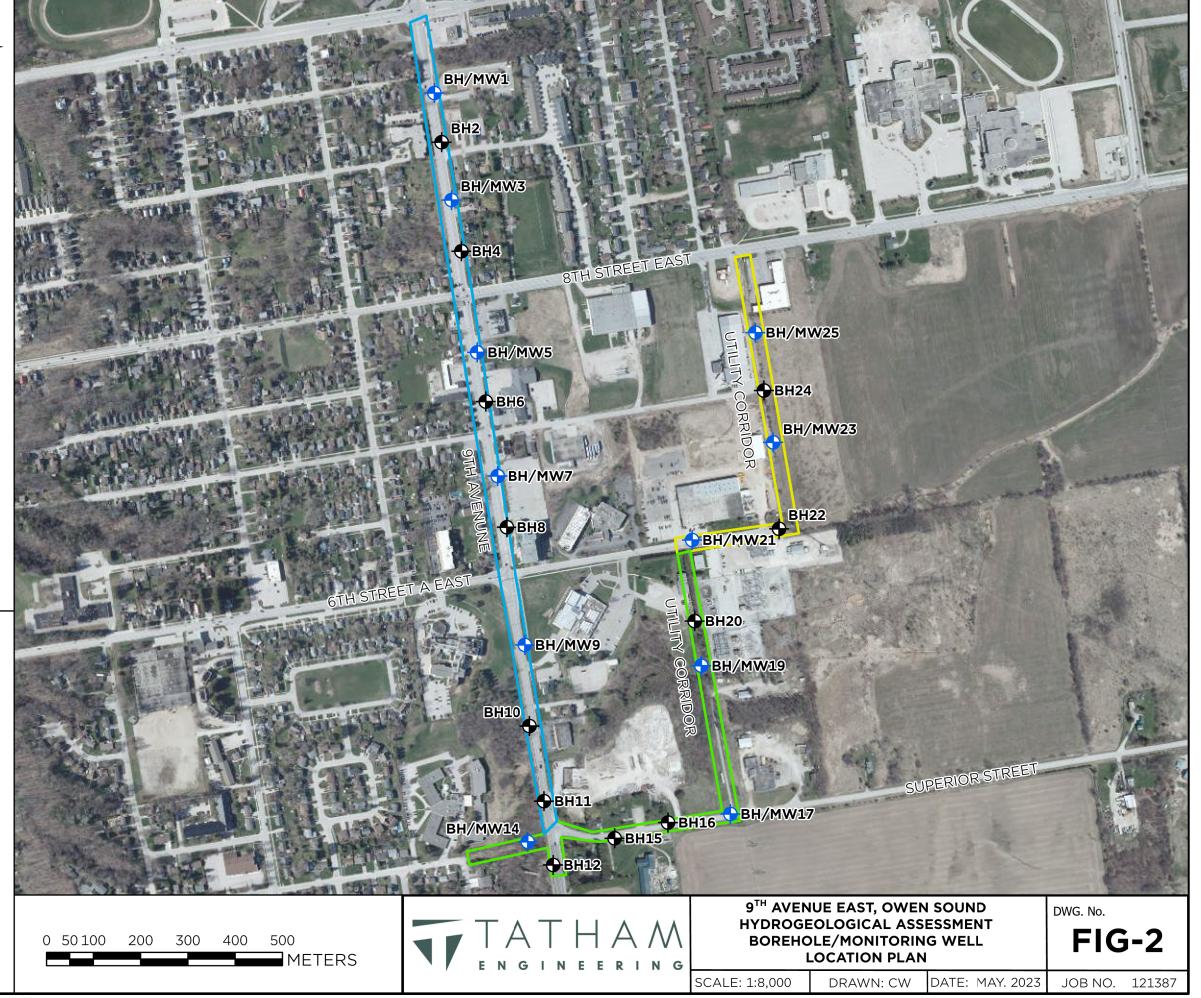
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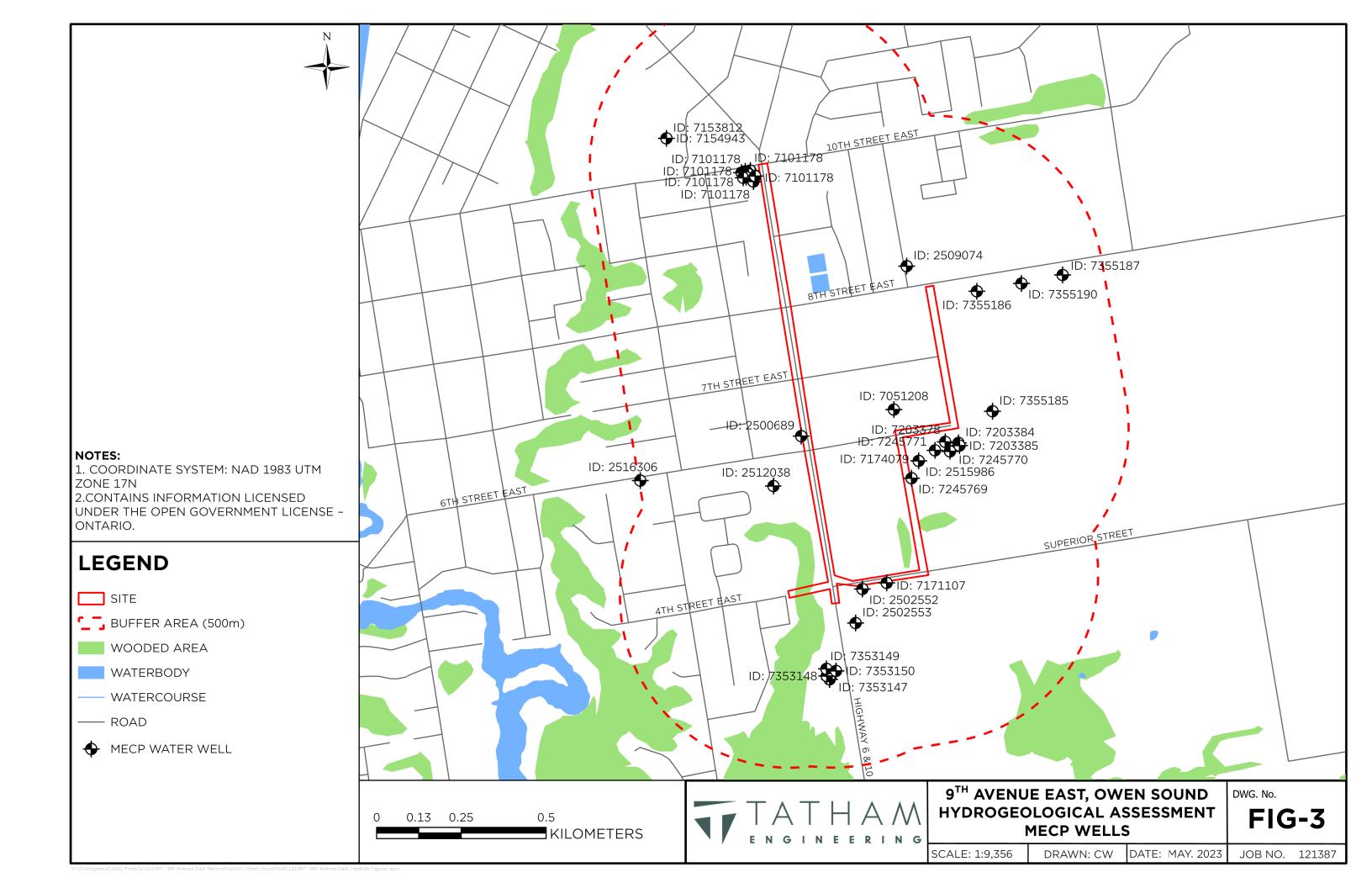
DEWATERING ZONES

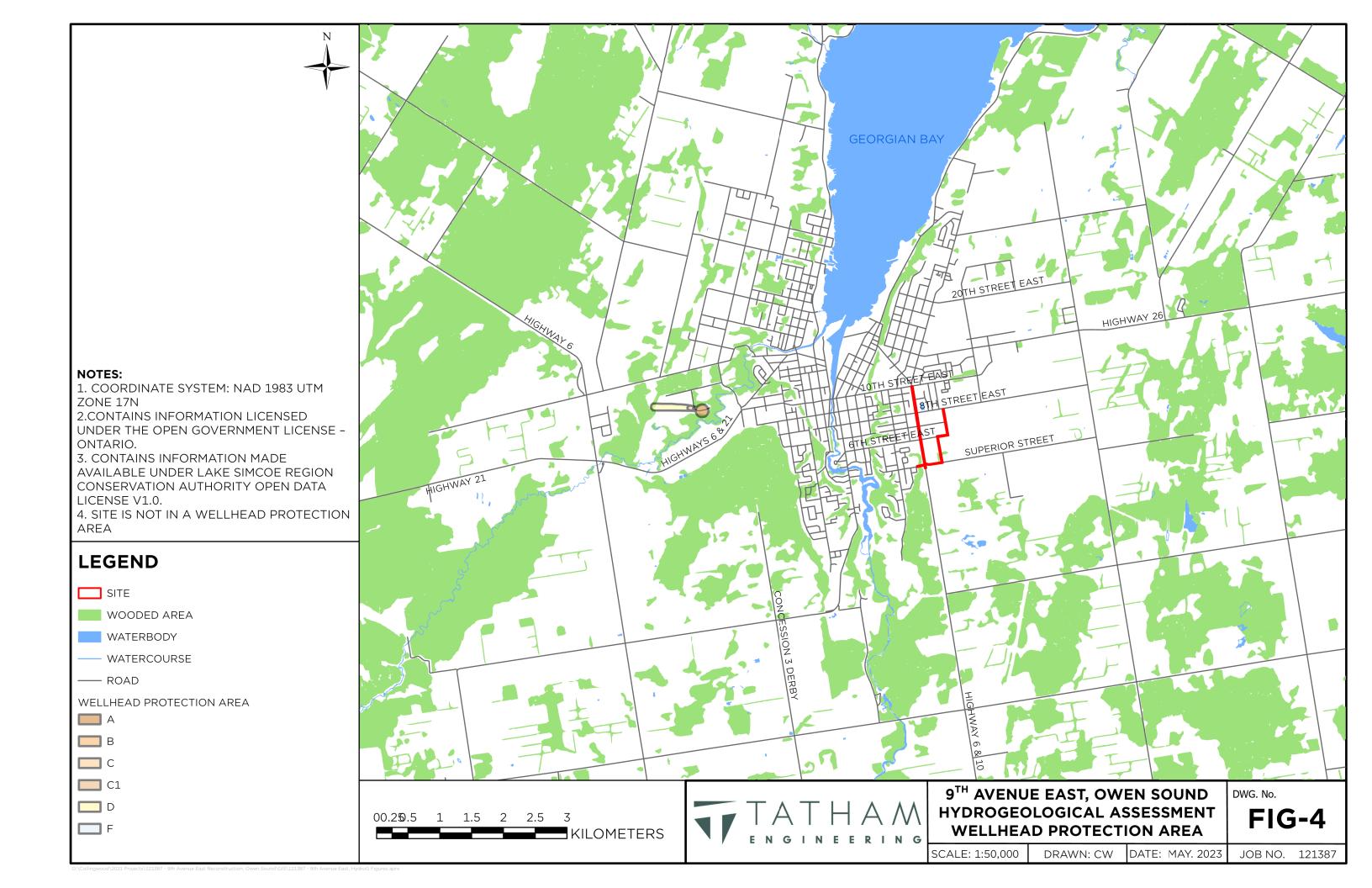
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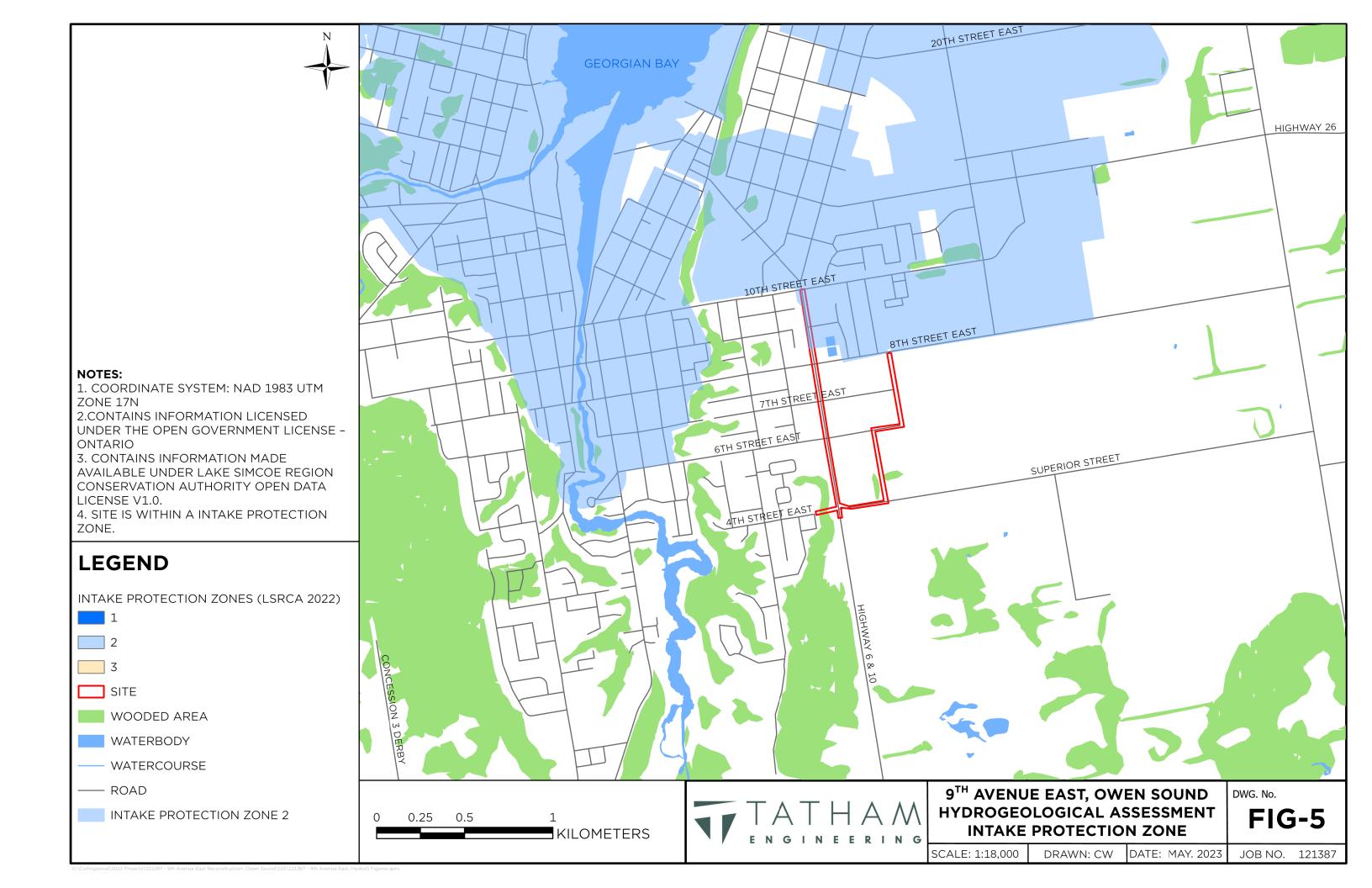
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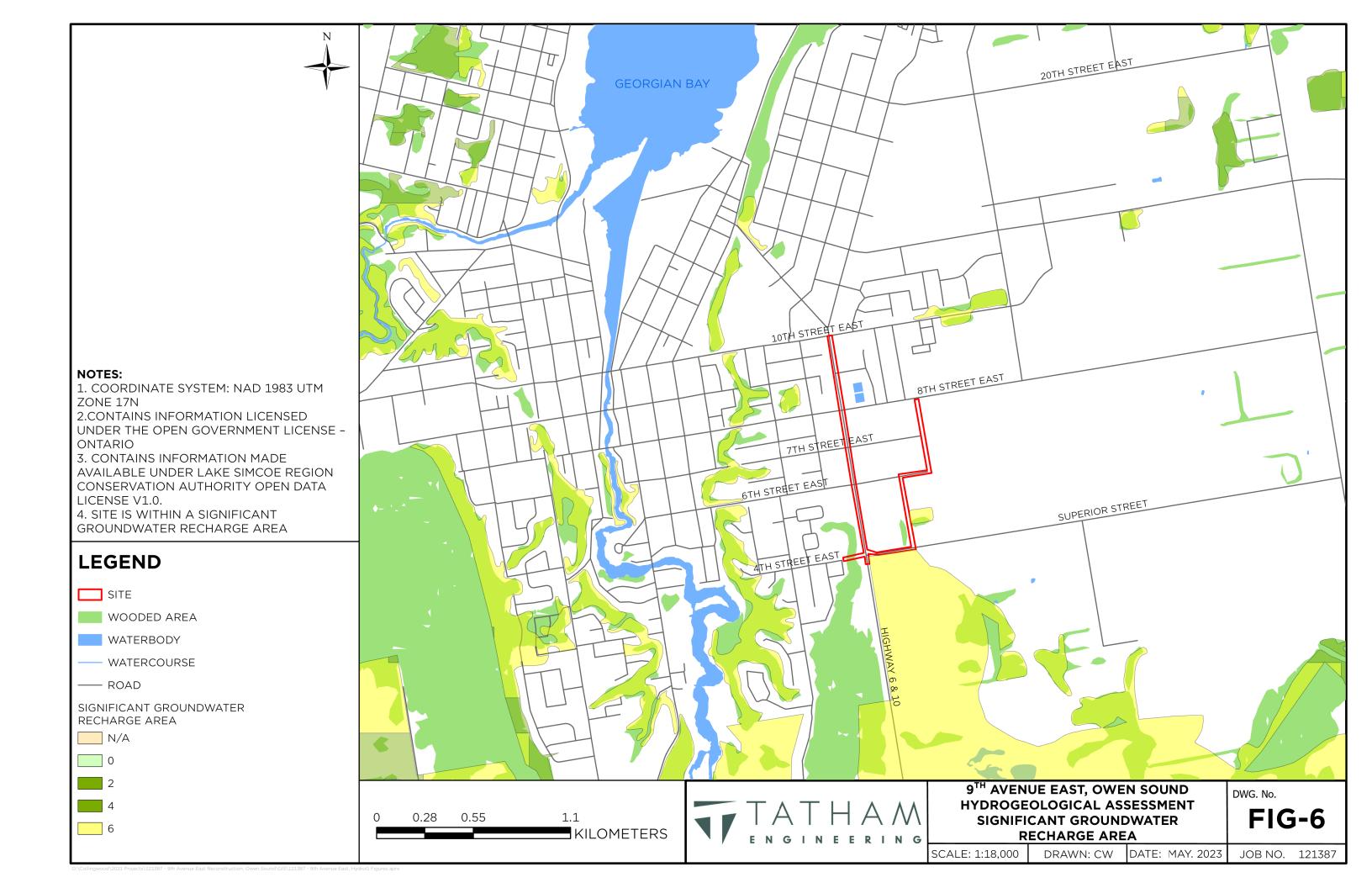
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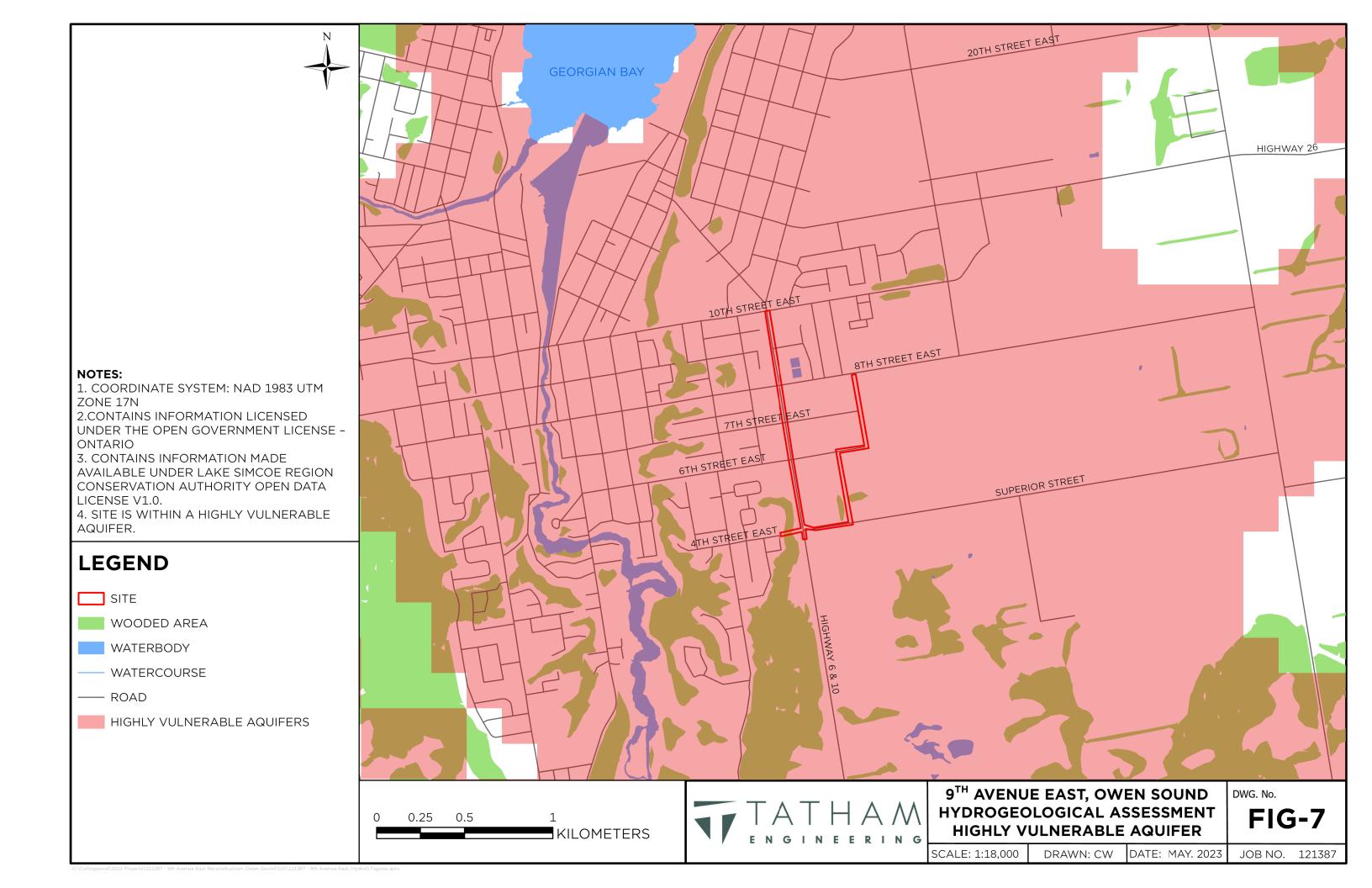


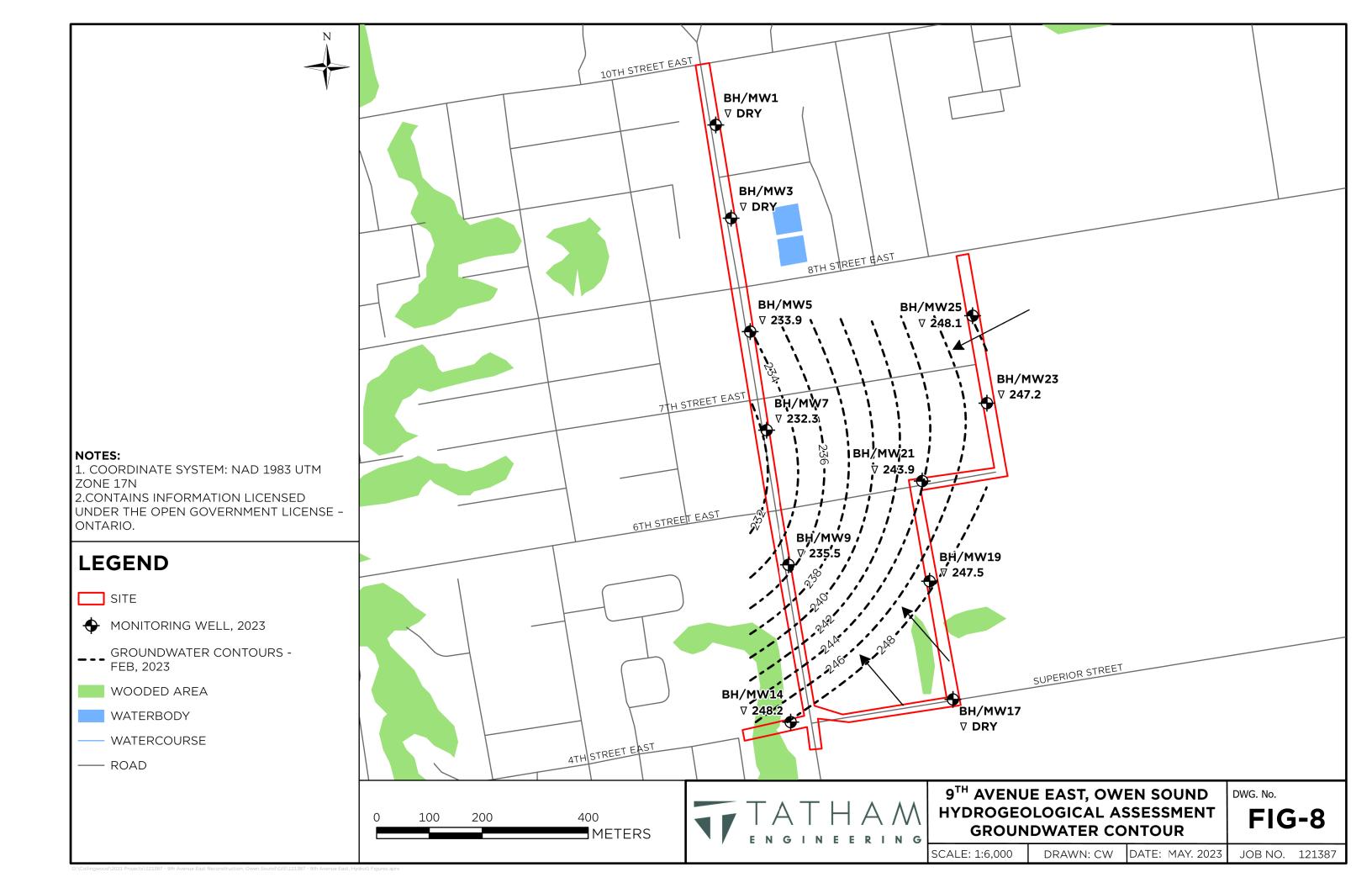












Appendix A: MECP Water Well Records



Township Con Lot	UTM	Date Centr	Casing Dia	Water	Pump Test	Well Use	Screen Depth	Well	Formation
ARTEMESIA TOWNSHIP	17 505660 4935080 W	2004/02 6607	19.6	FR 0013			0016 10	2515913 (Z07616) A007477	BRWN FILL 0003 BRWN SILT STNS CLAY 0013 GREY SHLE LMSN SILT 0026
OWEN SOUND CITY	17 505722 4934176 W	1992/05 5507	6	FR 0042 FR 0112	20/123/4/1:	DO		2512038 (106144)	RED SHLE 0027 BLUE SHLE 0042 RED SHLE 0123
OWEN SOUND CITY	17 506129 4934199 W	2015/07 7148						7245769 (Z209684) A	
OWEN SOUND	17 505660 4935080 W	2006/09 6607	2	FR 0005		NU	0005 12	2516956 (Z54927) A046463	RED SAND SLTY 0005 GREY SHLE LMSN 0017
OWEN SOUND	17 506242 4934278 W	2015/07 7148						7245770 (Z209683) A	
OWEN SOUND	17 506198 4934281 W	2015/07 7148						7245771 (Z209682) A	
OWEN SOUND	17 505330 4934192 W	2005/01 6607	1.97	FR 0010			0008 5	2516306 (Z21657) A019250	BRWN SILT SAND 0010 BRWN SILT CLAY 0011 BRWN CLAY SILT 0013
OWEN SOUND	17 506150 4934250 W	2004/04 7201	2			NU	0003 10	2515986 (Z09757) A008823	GREY CSND DRY 0002 BLUE UNKN 0006 BRWN SAND SILT WBRG 0013
OWEN SOUND	17 506150 4934250 W	7303				МО		7174079 (Z132409) A	
OWEN SOUND	17 505240 4933801 W	2010/10 6809	0.5 0.5 0.5			ТН	0070 1 0022 1 0052 1	7173660 (Z121108) A100816	BLCK LOAM 0001 BRWN SAND 0020 BRWN CLAY 0040 GREY CLAY 0060 RED SHLE 0070
OWEN SOUND	17 506228 4934306 W	2012/04 7201		3		МО		1,	BRWN SAND GRVL 0005 GREY SILT WBRG SAND 0012



Township Con Lot	UTM	Date Centr	Casing Dia	Water	Pump Test	Well Use	Screen Depth	Well	Formation
OWEN SOUND	17 506267 4934303 W	7201	1.5			мо	0002 10	7203384 (Z141592) A125032	BRWN SAND CLAY FILL 0001 BRWN CLAY SILT TILL 0009 GREY CLAY SILT TILL 0015
OWEN SOUND	17 506270 4934295 W	2012/01 7201						7203385 (M08327) A125035 P	
OWEN SOUND	17 505306 4934077 W	2010/03 7215				ТН	0026 10	A097586	BRWN FILL WBRG 0006 BRWN CLAY SLTY 0020 GREY CLAY SLTY WBRG 0036
OWEN SOUND CITY	17 505307 4934075 W	2010/03 7215						7144745 (Z112534) A	
OWEN SOUND	17 505299 4934031 W	2010/05 7215				тн	0017 10	7146075 (Z112571) A095340	BRWN FILL WBRG 0002 BRWN CLAY WBRG 0020 BRWN SAND WBRG 0026 GREY CLAY WBRG 0027
OWEN SOUND	17 505660 4935080 W	2006/07 6607		FR 0015				2516864 (Z49099) A007977 A	
OWEN SOUND	17 506367 4934396 W	2018/10 7644	2			тн мо	0015 10	7355185 (Z301298) A260228	
OWEN SOUND	17 505907 4933632 W	2019/10 7190	6 1.25			МО	0033 10	7353150 (4SLGP6LK) A281484	BRWN CLAY SAND 0010 GREY LMSN 0043
OWEN SOUND	17 505879 4933638 W	2019/10 7190	6 1.25			МО	0028 10	7353149 (NXNA9Q A9) A281483	BRWN CLAY SAND 0010 GREY LMSN 0038
OWEN SOUND	17 506321 4934749 W	2018/10 7644	2			тн мо	0005 10	7355186 (Z301285) A249645	



Township Con Lot	UTM	Date Centr	Casing Dia	Water	Pump Test	Well Use	Screen Depth	Well	Formation
OWEN SOUND	17 506573 4934797 W	2018/10 7644		2		тн мо	0005 10	7355187 (Z301284) A249744	
OWEN SOUND	17 506452 4934772 W	2018/10 7644		2		тн мо	0010 10	7355190 (Z301286) A249768	
OWEN SOUND	17 505888 4933607 W	2019/10 7190	6 1.2	5		мо	0026 10	7353147 (IZMSOOO 6) A281481	BRWN CLAY SAND 0008 GREY LMSN 0036
OWEN SOUND	17 505880 4933617 W	2019/10 7190	6 1.2	5		МО	0028 10	7353148 (O99VQYA 2) A281482	BRWN CLAY SAND 0010 GREY LMSN 0038
OWEN SOUND CITY	17 505805 4934323 W	1947/06 5514	4 4	FR 0040 FR 0070	40//1/1:0	DO CO		1 ''	LOAM CLAY 0008 ROCK 0058 SHLE 0142
OWEN SOUND	17 506077 4934401 W	2007/09 7241	1	5		МО		7051208 (Z63648) A063679	BRWN LOAM LOOS 0001 BRWN CLAY SILT DNSE 0012 GREY CLAY SILT WBRG 0023
OWEN SOUND	17 505165 4933870 W	1952/06 1319		FR 0060 4 UK 0091	52/55/5/1:0	DO		2501937 ()	LOAM 0006 ROCK 0046 BLUE CLAY 0061 RED CLAY 0091
SYDENHAM TOWNSHIP	17 506056 4933891 W	7303						7171107 (Z132388) A	
SYDENHAM TOWNSHIP RANGE 02 003	17 506115 4934823 W	1987/08 5507		5 FR 0158	24/168/5/2:0	DO		2509074 (14857)	HPAN STNS 0058 LMSN 0158 BLUE SHLE 0163 RED SHLE 0168
SYDENHAM TOWNSHIP RANGE A 004	17 505965 4933773 W	1957/02 5502	6 6	FR 0125 FR 0180	71/170/5/3:0	СО		2502553 ()	CLAY 0005 LMSN 0070 BLUE SHLE 0080 RED SHLE 0150 ROCK 0180 BLUE SHLE 0206
SYDENHAM TOWNSHIP RANGE A 004	17 505985 4933873 W	1954/10 5506	4 4	FR 0075 FR 0080	40/115/10/1:0	DO		2502552 ()	LOAM 0010 LMSN 0085 BLUE SHLE 0115



UTM: UTM in Zone, Easting, Northing and Datum is NAD83; L: UTM estimated from Centroid of Lot; W: UTM not from Lot Centroid

DATE CNTR: Date Work Completed and Well Contractor Licence Number

CASING DIA: Casing diameter in inches

WATER: Unit of Depth in Feet. See Table 4 for meanign of code.

PUMP TEST: Static Water Level in Feet / Water Level After Pumping in Feet / Pump Test Rate in GPM / Pump Test Duration in Hr : Min

WELL USE: See Table 3 for Meaning of Code

SCREEN: Screen Depth and Length in feet

WELL: WEL (AUDIT #) Well Tag. A: Abandonment; P: Partial Data Entry Only

FORMATION: See Table 1 and 2 for Meaning of Code

Table 1: Core Material and Descriptive Terms										
BLDR BOULDERS	FCRD FRACTURED	IRFM IRON FORMATION	PORS POROUS	SOFT SOFT						
BSLT BASALT	FGRD FINE-GRAINED	LIMY LIMY	PRDG PREVIOUSLY DUG	SPST SOAPSTONE						
CGRD COARSE-GRAINED	FGVL FINE GRAVEL	LMSN LIMESTONE	PRDR PREV. DRILLED	STKY STICKY						
CGVL COARSE GRAVEL	FILL FILL	LOAM TOPSOIL	QRTZ QUARTZITE	STNS STONES						
CHRT CHERT	FLDS FELDSPAR	LOOS LOOSE	QSND QUICKSAND	STNY STONEY						
CLAY CLAY	FLNT FLINT	LTCL LIGHT-COLOURED	QTZ QUARTZ	THIK THICK						
CLN CLEAN	FOSS FOSILIFEROUS	LYRD LAYERED	ROCK ROCK	THIN THIN						
CLYY CLAYEY	FSND FINE SAND	MARL MARL	SAND SAND	TILL TILL						
CMTD CEMENTED	GNIS GNEISS	MGRD MEDIUM-GRAINED	SHLE SHALE	UNKN UNKNOWN TYPE						
CONG CONGLOMERATE	GRNT GRANITE	MGVL MEDIUM GRAVEL	SHLY SHALY	VERY VERY						
CRYS CRYSTALLINE	GRSN GREENSTONE	MRBL MARBLE	SHRP SHARP	WBRG WATER-BEARING						
CSND COARSE SAND	GRVL GRAVEL	MSND MEDIUM SAND	SHST SCHIST	WDFR WOOD FRAGMENTS						
DKCL DARK-COLOURED	GRWK GREYWACKE	MUCK MUCK	SILT SILT	WTHD WEATHERED						
DLMT DOLOMITE	GVLY GRAVELLY	OBDN OVERBURDEN	SLTE SLATE							
DNSE DENSE	GYPS GYPSUM	PCKD PACKED	SLTY SILTY							
DRTY DIRTY	HARD HARD	PEAT PEAT	SNDS SANDSTONE							
DRY DRY	HPAN HARDPAN	PGVL PEA GRAVEL	SNDY SANDYOAPSTONE							

Table 2: Core Color

WHIT WHITE
GREY GREY
BLUE BLUE
GREN GREEN
YLLW YELLOW
BRWN BROWN
RED RED
BLCK BLACK
BLGY BLUE-GREY

Table 3: Well Use

AC Cooling And A/C NU Not Used

PS Public

Table 4:Water Detail

FR Fresh GS Gas SA Salty IR Iron SU Sulphur

MN Mineral UK Unknown

Appendix B: Borehole Logs

RECORD OF BOREHOLE No. 1 2201530 Project Number: Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4935009 Date Started: Feb 1/23 See Borehole Location Plan GW 505716 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits -ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 220 mm AS GRANULAR FILL: 120 mm 234 FILL: Silty sand, trace gravel, dense, brown, moist 18 SS 2 100 49 SANDY SILT GLACIAL TILL: Some 17 0 3 75 71 071 SS clay, trace to some gravel, trace shale 232.5 fragments, very dense, greyish brown moist 200 --- Dense, brownish red ---SS 4 100 31 ℃ 31 10 18 32 40 3 - - - Very Dense - - -18 0 SS 5 100 51 051 231 45 18 - - - Dense, grey - - -440 SS 6 100 44 229.5 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation:

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from

2201530 Project Number:

Project Client: Tatham Engineering Ltd.

9th Ave E, Owen Sound, ON

Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Logged By:

See Borehole Location Plan GW 505727 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23

MH

Northing:

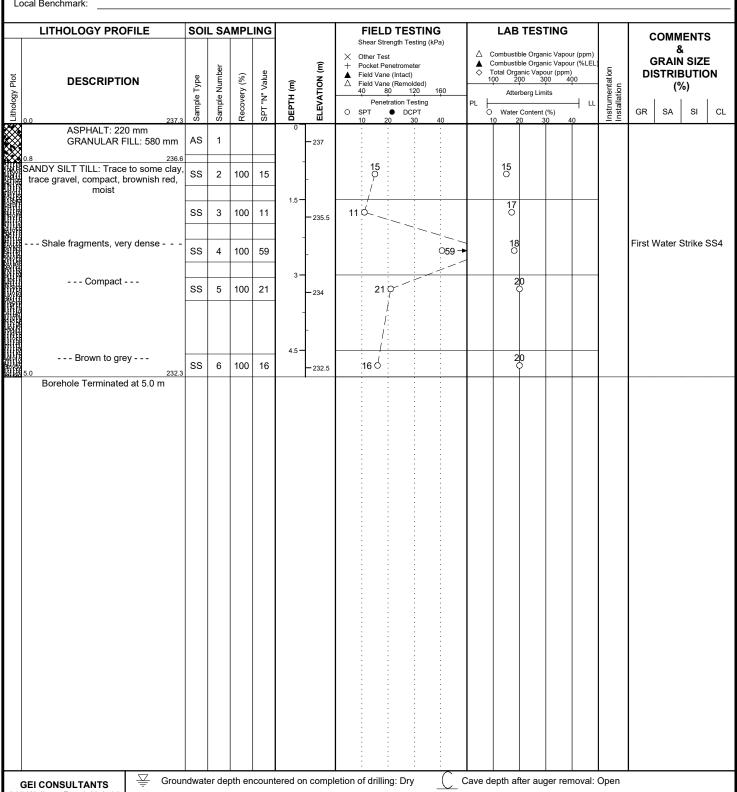
4934935

Date Started:

Feb 1/23

Local Benchmark:

Project Location:



647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

 \mathbf{Z} Groundwater depth observed on:

RECORD OF BOREHOLE No. 3 2201530 Project Number: Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934850 Date Started: Feb 1/23 See Borehole Location Plan GW 505793 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 260 mm AS 1 GRANULAR FILL: 500 mm 16 FILL: Silty sand, trace gravel, compact, SS 2 75 13 brown, moist 241.5 1.5 15 3 110 SS 45 11 - - - Clayey silt, some sand, trace 18 SS 4 10 3 ďЗ gravel, soft - - -3 SS 5 25 4 SANDY SILT TILL: Some clay, trace 6 75 16 :16 🔾 gravel, compact, brownish red, moist - 238.5 45 - - - Grey - - -SS 7 100 22 22:0 237.7 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation: Barrie, Ontario L4N 0B7 T: (705) 719-7994 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from Scale: 1:75

a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'.

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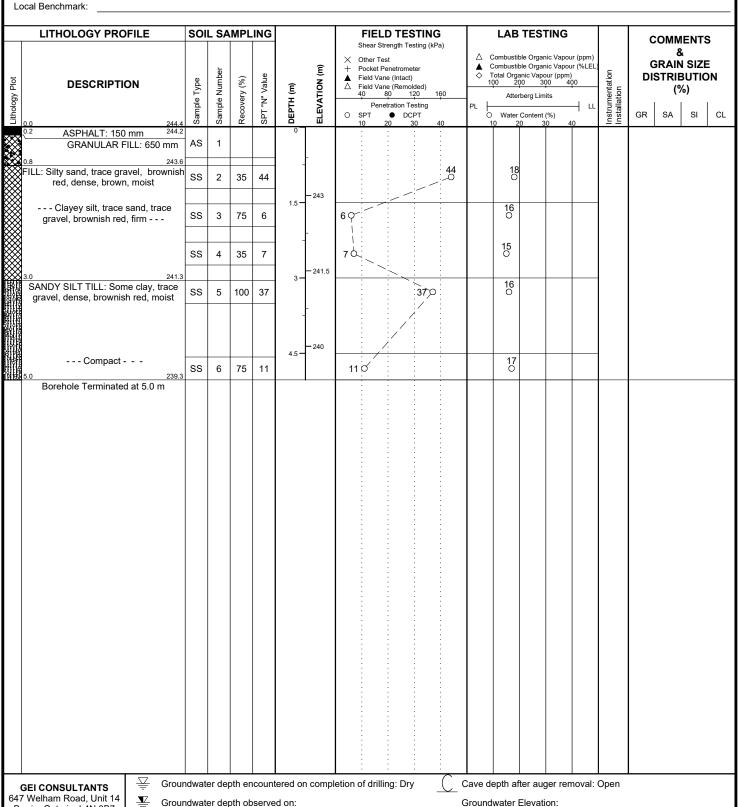
www.geiconsultants.com

Project Number: 2201530

Project Client: Tatham Engineering Ltd.

Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road

Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934771 Date Started: Feb 1/23 See Borehole Location Plan GW 505757 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23



647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 5 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934619 Date Started: Jan 31/23 See Borehole Location Plan GW 505781 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ **DESCRIPTION** Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 300 mm 237 AS GRANULAR FILL: 360 mm SANDY SILT GLACIAL TILL: Trace to 15 16 some clay, trace to some gravel, SS 2 100 16 cobbles and boulders, compact, brown, moist - 235.5 17 3 100 SS 18 18 Q 17 SILTY SAND GLACIAL TILL: Some SS 4 100 30 🔈 30 gravel, some clay, cobbles and boulders, dense, brown, moist 3 -234 SS 5 100 32 32:0 17 38 33 12 4.5 -232.5 14 SS 6 100 33 33 0 232.0 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 3.2 m. Groundwater Elevation: 233.9 m

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 6 2201530 Project Number: Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934545 Date Started: Jan 31/23 See Borehole Location Plan GW 505794 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits -ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 130 mm GRANULAR FILL: 290 mm 234.8 AS 1 FILL: Silty sand, some clay, trace gravel, compact, brown, moist 15 **16** SS 2 100 16 - 234 1.5 SANDY SILT GLACIAL TILL: Trace to <u>16</u> 3 100 SS 18 18 Q some clay, trace gravel, cobbles and boulders, compact, brown, moist --- Dense ---15 SS 4 100 30 🔈 30 232.5 3 18 O SS 5 100 32 32:0 -231 45 17 SS 6 100 33 33 0 230.2 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Groundwater Elevation:

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 7 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934433 Date Started: Jan 31/23 See Borehole Location Plan GW 505812 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits -ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 120 mm GRANULAR FILL: 200 mm AS 1 FILL: Silty sand, some gravel, very loose, brown, wet 20 AS 2 - 232.5 1.5 - - - Sandy clayey silt, trace gravel, SS 3 100 8 loose - - -SANDY CLAYEY SILT GLACIAL TILL: SS 4 100 13 Q 13 Trace gravel, cobbles and boudlers, 231 stiff/compact, brown, moist 3 --- Very stiff, grey ---SS 5 100 26 26 Ç 229 5 4.5 20 SS 6 100 20 200 228.7 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: 4.4 m. Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 1.4 m.

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Groundwater Elevation: 232.3 m

Project Number: 2201530

Project Location:

Project Client: Tatham Engineering Ltd.

9th Ave E, Owen Sound, ON

Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Logged By:

See Borehole Location Plan GW 505826 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23

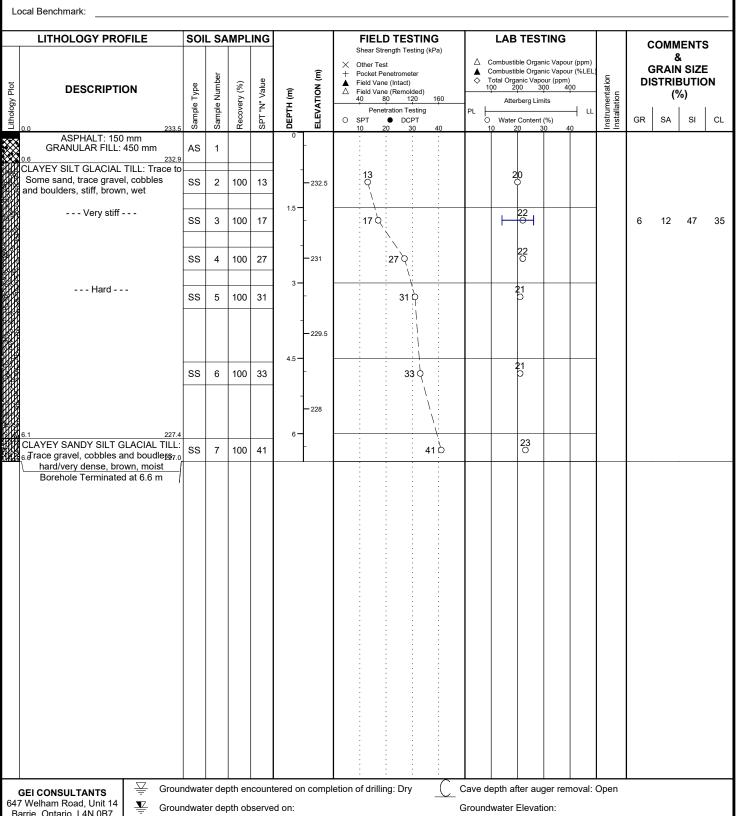
MH

Northing:

4934356

Date Started:

Jan 31/23



Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 9 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934179 Date Started: Feb 2/23 See Borehole Location Plan GW 505854 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 170 mm GRANULAR FILL: 590 mm AS 1 237 FILL: Sand and silt, trace gravel, SS 2 100 14 compact, dark color, moist --- Loose ---3 100 6 6 ¢ SS 235.5 SANDY SILT GLACIAL TILL: Trace to 12:0 SS 4 100 12 some clay, trace gravel, cobbles and boulders, compact, brown, wet 3 SS 5 100 18 18 Q: -234 45 - - - Very dense - - -24 SS 6 100 50 50 232.5 Borehole Terminated at 5.0 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 1.8 m. Groundwater Elevation: 235.5 m

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RECORD OF BOREHOLE No. 10 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934057 Date Started: Feb 2/23 See Borehole Location Plan GW 505861 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing 0 O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 100 mm GRANULAR FILL: 660 mm AS 1 13 15 FILL: Silty sand, some rock fragments, SS 2 35 13 compact, brown, moist 244.5 Borehole Terminated at 1.5 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: 0.8 m. Cave depth after auger removal: Open **GEI CONSULTANTS** \mathbf{Z} Groundwater depth observed on:

647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 11 2201530 Project Number: Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4933944 Date Started: Feb 2/23 See Borehole Location Plan GW 505883 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **FIELD TESTING LAB TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing 0 O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 120 mm GRANULAR FILL: 650 mm AS 1 253.5 30 FILL: Silty sand, dense, brown, moist 14 SS 2 75 30 Borehole Terminated at 1.5 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7

T: (705) 719-7994 www.geiconsultants.com

RECORD OF BOREHOLE No. 12 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4933848 Date Started: Feb 2/23 See Borehole Location Plan GW 505897 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **FIELD TESTING LAB TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing 0 O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 160 mm 262.5 GRANULAR FILL: 600 mm AS 1 30 FILL: Silty sand, some gravel, dense, SS 2 55 30 brown, mosit Borehole Terminated at 1.5 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. T: (705) 719-7994 Scale: 1:75 www.geiconsultants.com

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RECORD OF BOREHOLE No. 14 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: МН Northing: Date Started: Feb 2/23 See Borehole Location Plan GW **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits -ithology Penetration Testing 0 O SPT DCPT Water Content (%) GR SA SI CL TOPSOIL: 75 mm SS 1 85 18 0: FILL: Sandy silt, trace gravel, trace organics and rootlets, compact, brown, moist SANDY SILT: Trace gravel, trace clay, SS 2 100 26 260 compact, brown, moist 247.5 1.5 --- Dense ---3 100 SS 31 31 b SAND AND SILT GLACIAL TILL: Trace 14 SS 4 100 60 060 7 35 55 clay, trace gravel and clay, cobbles and boulders, very dense, grey 246 3 -- - - Trace rock fragments - - -15 O SS 5 40 50+ 50+ Borehole Terminated at 3.5 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open

GEI CONSULTANTS 647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 0.6 m.

RECORD OF BOREHOLE No. 15 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Method: Truck Mount Drilling Machine: Solid Stem Augers Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: Date Started: Feb 2/23 See Borehole Location Plan GW **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **FIELD TESTING LAB TESTING** COMMENTS \triangle Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing 6 O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 90 mm GRANULAR FILL: 520 mm AS SANDY SILT GLACIAL TILL: Some 14 clay, trace gravel, very dense, brown, SS 2 100 50+ - 264 moist Borehole Terminated at 1.5 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Groundwater Elevation: Barrie, Ontario L4N 0B7 Borehole details presented do not constitute a thorough understanding of all potential conditions present and require interpretative assistance from a qualified geotechnical engineer. Also, borehole information should be read in conjunction with the geotechnical report for which it was commissioned and the accompanying 'Explanation of Boring Log'. T: (705) 719-7994 Scale: 1:75 www.geiconsultants.com Page: 1 of 1

RECORD OF BOREHOLE No. 16 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4933912 Date Started: Feb 2/23 See Borehole Location Plan GW 506070 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 210 mm GRANULAR FILL: 400 mm AS 265.5 SANDY SILT GLACIAL TILL: Some 12 16 clay, trace gravel, cobbles and SS 2 100 12 boulders, compact, brownish red, moist 1.5 15 0 11 0 SS 3 35 11 264.2 Borehole Terminated at 1.8 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** \mathbf{Z}

647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater depth observed on:

RECORD OF BOREHOLE No. 17 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4933925 Date Started: Feb 2/23 See Borehole Location Plan GW 506164 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 100 mm 262.5 GRANULAR FILL: 660 mm AS 1 16 FILL: Clayey silt, some sand, trace SS 2 100 12 gravel, cobbles and boulbers, stiff, brown, moist <u>16</u> 0 SANDY SILT GLACIAL TILL: Some -261 22:0 SS 3 0 22 clay, trace gravel, cobbles and boulders, compact to very dense, 17 brown, moist 260.3 50÷ 4 100 50+ $_{\lambda}$ SS Borehole Terminated at 2.4 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: Dry Groundwater Elevation: Barrie, Ontario L4N 0B7

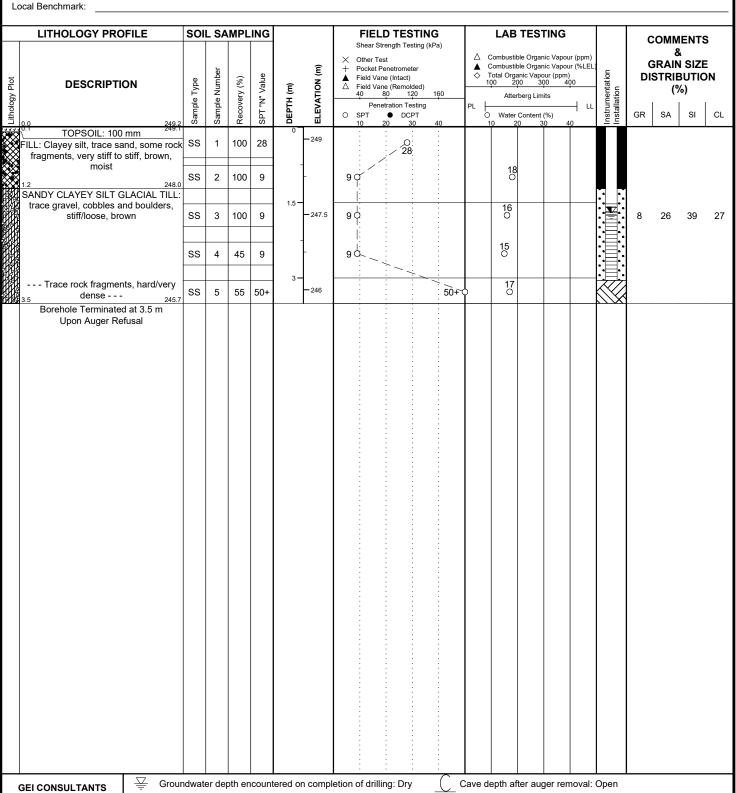
T: (705) 719-7994 www.geiconsultants.com

Tatham Engineering Ltd.

Project Number: 2201530 Project Client:

Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road

Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934148 Date Started: Feb 2/23 See Borehole Location Plan GW 506120 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23



647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater depth encountered on completion of drilling: Dry \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 1.7 m. Cave depth after auger removal: Open

RECORD OF BOREHOLE No. 20 2201530 Project Number: Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934215 Date Started: Feb 2/23 See Borehole Location Plan GW 506110 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits -ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL TOPSOIL: 150 mm SS 1 100 6 0 24 FILL: Clayey silt, trace to some sand, trace organics, stiff, brown, moist 247.5 17 SS 2 100 7 7 Q 1.5 SANDY CLAYEY SILT GLACIAL TILL: SS 3 100 12 12:0 Trace gravel, cobbles and boulders, stiff/ compact to loose, brown, moist - 246 17 9 \$ SS 4 100 9 3 -SS 5 100 7 70 Borehole Terminated at 3.5 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater Elevation:

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Groundwater depth observed on:

RECORD OF BOREHOLE No. 21 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934337 Date Started: Jan 30/23 See Borehole Location Plan GW 506106 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 DEPTH (m) (%) 160 Atterberg Limits ithology Penetration Testing O SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 125 mm GRANULAR FILL: 625 mm AS 1 244.5 17 FILL: Clayey silt, trace gravel, stiff, SS 2 100 8 brownish red, moist 1.5 <u>16</u> SANDY SILT: Some clay, loose, brown, SS 3 100 7 70 wet Borehole Terminated at 2.3 m Upon Refusal to Aguer Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 1.2 m. Groundwater Elevation: 244.0 m

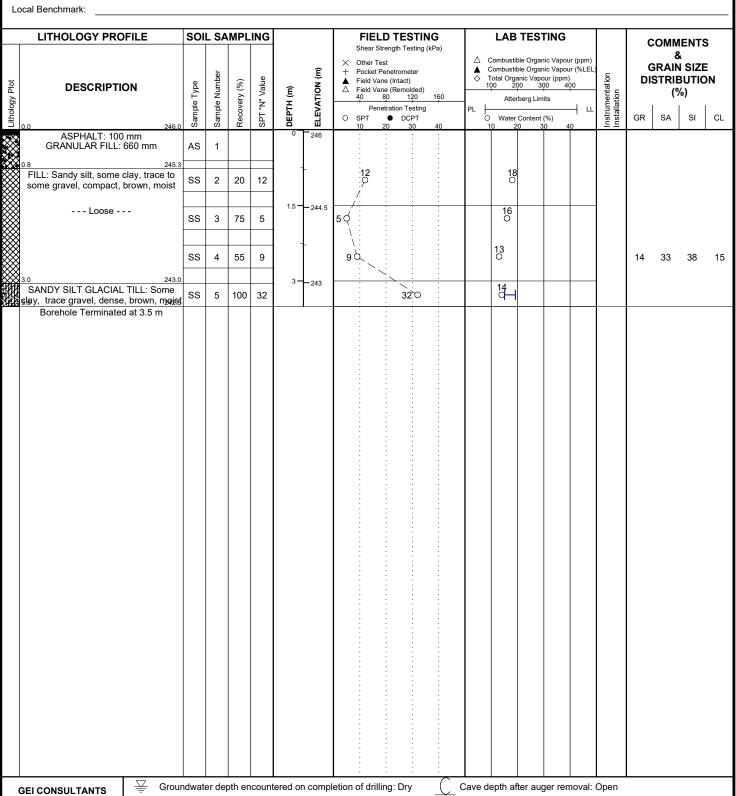
Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Project Name:

2201530 Project Number: Project Client: Tatham Engineering Ltd.



Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934354 Date Started: Jan 30/23 See Borehole Location Plan GW 506237 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23



647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

 \mathbf{Z} Groundwater depth observed on:

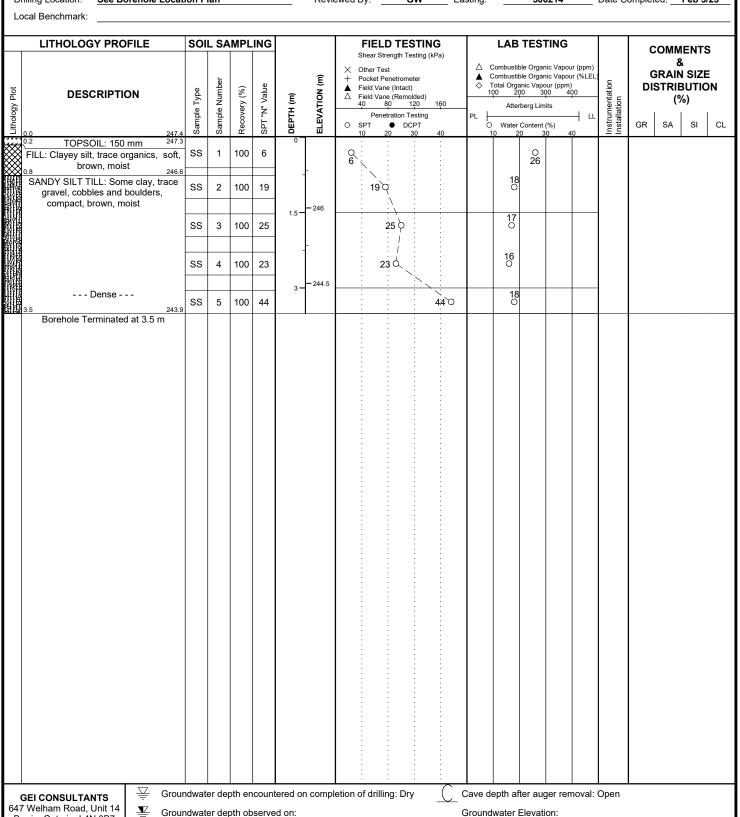
RECORD OF BOREHOLE No. 23 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934484 Date Started: Jan 30/23 See Borehole Location Plan GW 506228 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Sample Type Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits -ithology Penetration Testing 0 SPT DCPT Water Content (%) GR SA SI CL ASPHALT: 125 mm SS 1 100 12 0 12 0 27 FILL: Sandy Silt, some clay, gtrace organics, trace gravel, compact, brown, moist 18 SANDY SILT GLACIAL TILL: Trace to SS 2 100 14 140 Some clay, trace to some gravel, 246 cobbles and boulders, compact, brown 1.5 15 moist 3 100 SS 15 15 Q 17 SS 4 100 23 230 244 5 3 - - - Very dense - - -16 0 SS 5 100 66 O66 18 32 39 11 Borehole Terminated at 3.5 m Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open **GEI CONSULTANTS** 647 Welham Road, Unit 14 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 0.1 m.

Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

Project Number: 2201530 Project Client: Tatham Engineering Ltd.



Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934562 Date Started: Jan 30/23 See Borehole Location Plan GW 506214 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23



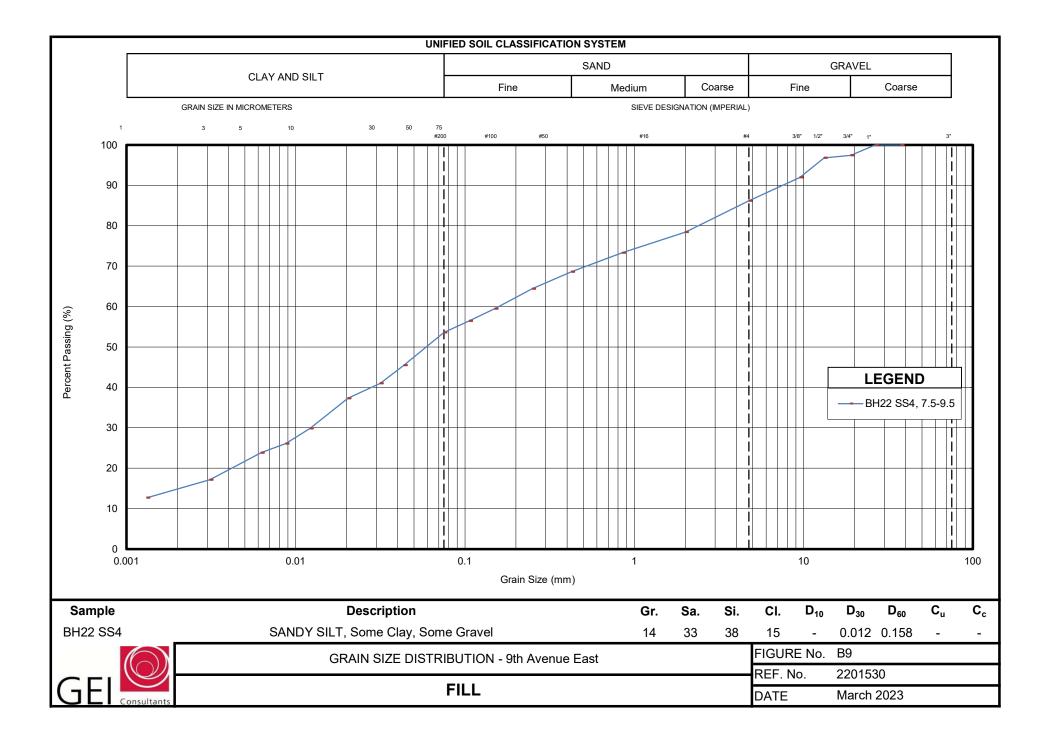
647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

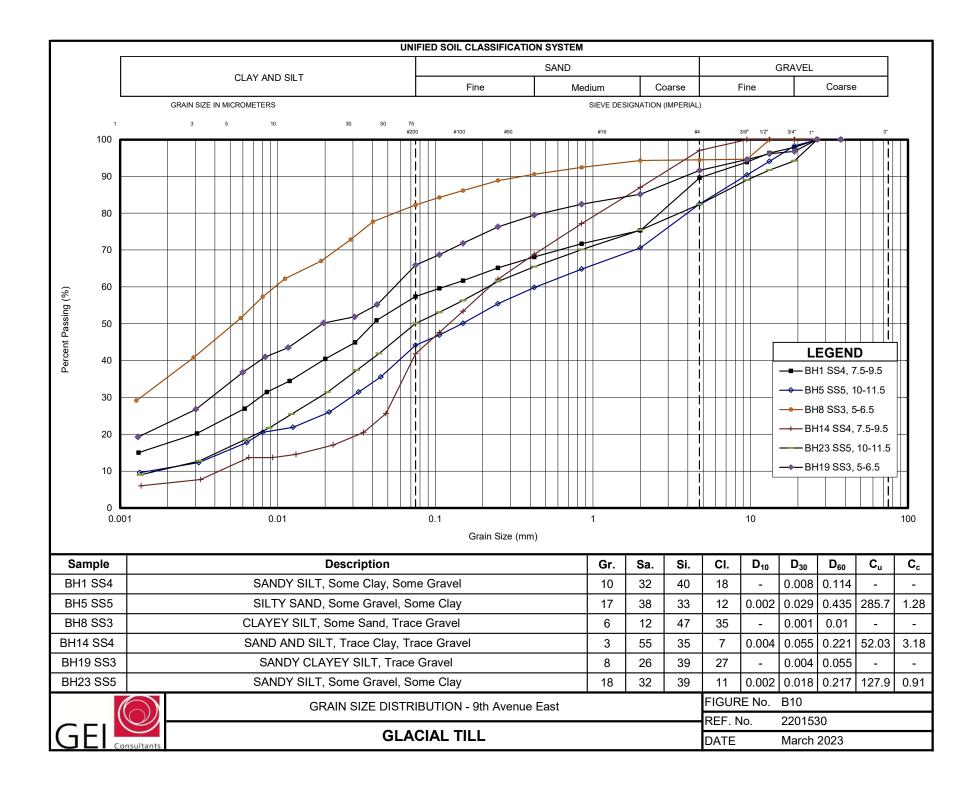
RECORD OF BOREHOLE No. 25 Project Number: 2201530 Project Client: Tatham Engineering Ltd. Drilling Machine: Solid Stem Augers Drilling Method: Truck Mount Project Name: Watermain Replacement and Road Project Location: 9th Ave E, Owen Sound, ON Logged By: MH Northing: 4934649 Date Started: Jan 31/23 See Borehole Location Plan GW 506201 **Drilling Location:** Reviewed By: Easting: Date Completed: Feb 3/23 Local Benchmark: LITHOLOGY PROFILE SOIL SAMPLING **LAB TESTING FIELD TESTING** COMMENTS Combustible Organic Vapour (ppm) **GRAIN SIZE** Combustible Organic Vapour (%LEL Pocket Penetrometer ELEVATION (m) Sample Number Total Organic Vapour (ppm) 100 200 300 40 nstrumentation Field Vane (Intact) DISTRIBUTION SPT "N" Value Δ Plot **DESCRIPTION** Field Vane (Remolded) 40 80 120 (%) 160 Atterberg Limits -ithology Penetration Testing 0 SPT DCPT Water Content (%) GR SA SI CL TOPSOIL: 150 mm SS 1 100 8 O 23 FILL: Clayey silt, some organics, trace 8 rootlets, stiff, dark color, moist 247.5 17 SANDY SILT GLACIAL TILL: Trace to SS 2 100 13 13 Þ some clay, trace gravel, cobbles and boulders, compact, brown, moist 1.5 3 100 SS 12 12:0 246 - - - Very dense - - -SS 4 50+ 65 50+ Borehole Terminated at 2.9 m Upon Auger Refusal Groundwater depth encountered on completion of drilling: Dry Cave depth after auger removal: Open

GEI CONSULTANTS 647 Welham Road, Unit 14 Barrie, Ontario L4N 0B7 T: (705) 719-7994 www.geiconsultants.com

 \mathbf{Z} Groundwater depth observed on: Feb 13/23 at depth of: 0.2 m.

Appendix C: Geotechnical Laboratory Data







Atterberg Limits Report

Project Name: 9th Avenue East

Project No.: 2201530

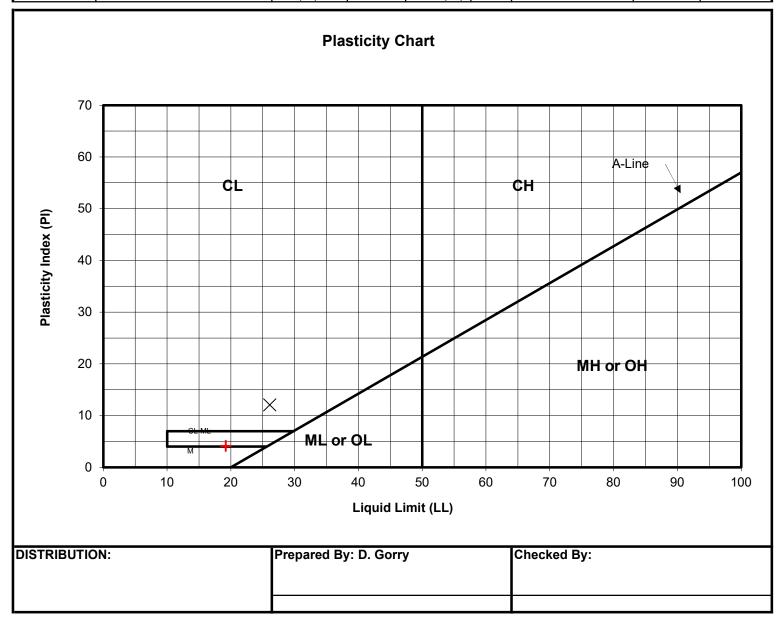
Client: Tatham Engineering Limited

Figure No.: B11

Date Tested: March 20, 2023

Date Sampled: -

	SAMPLE INFORMATION								
SAMPLE ID	SAMPLE ID BH8 SS3, 5-6.5 LIQUID LIMIT (LL): 26.1 PLASTIC LIMIT (PL) 14.1 PLASTIC INDEX (PI) 12.0 X								
SAMPLE ID	BH22 SS4, 7.5-9.5	LIQUID LIMIT (LL):	19.2	PLASTIC LIMIT (PL)	15.1	PLASTIC INDEX (PI)	4.1	+	



Report No.	
Report No.	

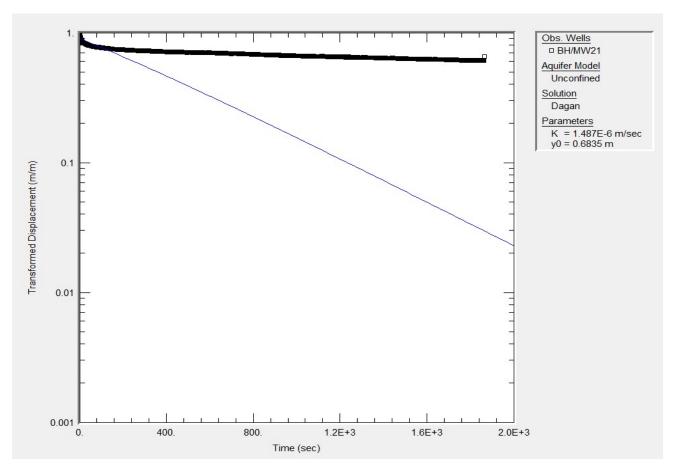
Appendix D: Borehole Permeability Test Results



Estimated Hydraulic Conductivity - Slug Test Dagan Equation

Date Completed:	21-Apr-23
Conducted by:	JM/NT

Well Number:	BH/MW21	
Well Screen Bottom:		mbgs
Top of Pipe:	0.09	mbgs
Well Casing Diameter:	5	cm
Well Elevation:	245.2	masl
Static Water Level:	1.4	mbgs
K:	1.49E-06	m/s



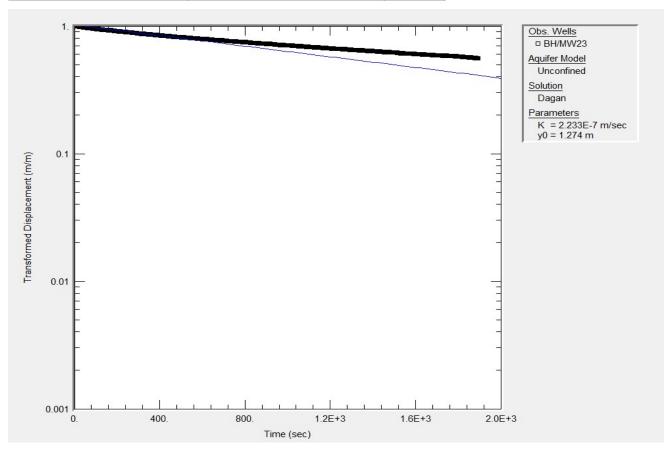
Dagan, G., 1978. A note on packer, slug, and recovery tests in unconfined aquifers, Water Resources Research, vol. 14, no. 5. pp. 929-934.



Estimated Hydraulic Conductivity - Slug Test Dagan Equation

Date Completed:	21-Apr-23
Conducted by:	JM/NT

Well Number:	BH/MW23	
Well Screen Bottom:	3	mbgs
Top of Pipe:	0.91	mags
Well Casing Diameter:	5	cm
Well Elevation:	247.3	masl
Static Water Level:	0.07	mags
K:	2.23E-07	m/s



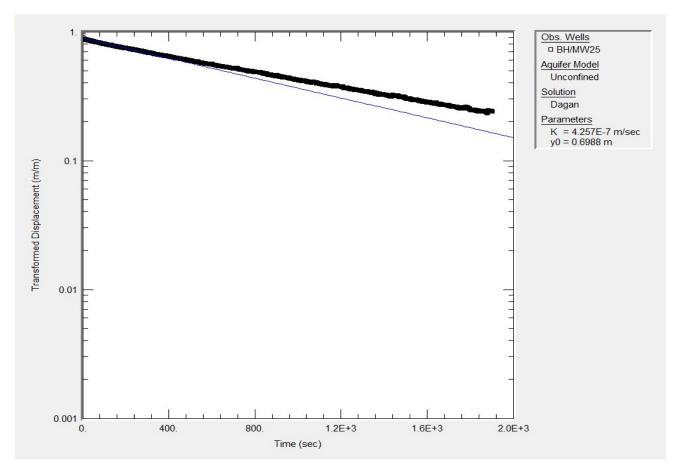
Dagan, G., 1978. A note on packer, slug, and recovery tests in unconfined aquifers, Water Resources Research, vol. 14, no. 5. pp. 929-934.



Estimated Hydraulic Conductivity - Slug Test Dagan Equation

Date Completed:	21-Apr-23
Conducted by:	JM/NT

Well Number:	BH/MW25	
Well Screen Bottom:	2.7	mbgs
Top of Pipe:	0.93	mags
Well Casing Diameter:	5	cm
Well Elevation:	248.3	masl
Static Water Level:		mbgs
K:	4.26E-07	m/s



Dagan, G., 1978. A note on packer, slug, and recovery tests in unconfined aquifers, Water Resources Research, vol. 14, no. 5. pp. 929-934.

Appendix E: Groundwater Quality

CERTIFICATE OF ANALYSIS



Final Report

C.O.C.: G115006 REPORT No: 23-008175 - Rev. 0

Report To:

Tatham Engineering 115 Sandford Fleming Drive Suite 200

Collingwood, ON L9Y 5A6

20.....g. 100 a, 0.11 20 1 0/10

CADUCEON Environmental Laboratories

112 Commerce Park Dr Unit L Barrie, ON L4N 8W8

Attention: Alicia Kimberley

DATE RECEIVED: 2023-Apr-22 CUSTOMER PROJECT: 121387

DATE REPORTED: 2023-May-08 P.O. NUMBER: 9th Ave E Owen Sound

SAMPLE MATRIX: Ground Water

Analyses	Qty	Site Analyzed	Authorized	Date Analyzed	Lab Method	Reference Method
Anions (Liquid)	1	OTTAWA	PCURIEL	2023-Apr-25	A-IC-01	SM 4110B
BOD5 (Liquid)	1	KINGSTON	MDUBIEN	2023-Apr-26	BOD-001	SM 5210B
Cond/pH/Alk Auto (Liquid)	1	OTTAWA	SBOUDREAU	2023-Apr-25	COND-02/PH-02/A	SM 2510B/4500H/
					LK-02	2320B
Cyanide Total (Liquid)	1	KINGSTON	KWELCH	2023-Apr-27	CN-001	SM 4500-CN-E
Chromium VI (Liquid)	1	OTTAWA	CBURKE	2023-May-05	D-CRVI-01	MECP E3056
ICP/MS Total (Liquid)	1	OTTAWA	TPRICE	2023-Apr-28	D-ICPMS-01	EPA 6020
ICP/OES Total (Liquid)	1	OTTAWA	NHOGAN	2023-Apr-26	D-ICP-01	SM 3120B
Mercury (Liquid)	1	OTTAWA	APRUDYVUS	2023-Apr-27	D-HG-02	SM 3112B
Nonylphenols (Subcontracted)	1	SGS_LAKEFIELD	CBURKE	2023-May-05		Subcontracted
OC Pesticides (Liquid)	1	KINGSTON	CSUMMERHAYS	2023-Apr-28	PESTCL-001	EPA 8081
Oil & Grease (Liquid)	1	KINGSTON	MTYMCHUK	2023-Apr-26	O&G-001	SM 5520
PCB's (Liquid)	1	KINGSTON	CSUMMERHAYS	2023-Apr-27	PCB-001	EPA 8081
PHC F1 (Liquid)	1	RICHMOND_HILL	FLENA	2023-Apr-27	C-VPHW-01	MECP E3421
PHC F2-4 (Liquid)	1	KINGSTON	KPARKER	2023-Apr-26	PHC-W-001	MECP E3421
Phenols (Liquid)	1	KINGSTON	KWELCH	2023-Apr-28	PHEN-01	MECP E3179
SVOC - Semi-Volatiles (Liquid)	1	KINGSTON	EASIEDU	2023-Apr-27	NAB-W-001	EPA 8270D
TP & TKN (Liquid)	1	KINGSTON	KDIBBITS	2023-May-03	TPTKN-001	MECP E3516.2
TSS (Liquid)	1	KINGSTON	JMACINNES	2023-Apr-26	TSS-001	SM 2540D
VOC-Volatiles (Liquid)	1	RICHMOND_HILL	FLENA	2023-Apr-27	C-VOC-02	EPA 8260

μg/g = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in $\mu g/g$, (F1-btex if requested)

F2 C10-C16 hydrocarbons in µg/g, (F2-napth if requested)

F3 C16-C34 hydrocarbons in $\mu g/g$, (F3-pah if requested)

F4 C34-C50 hydrocarbons in μg/g

This method complies with the Reference Method for the CWS PHC and is

validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

nC6 and nC10 response factor is within 30% of response factor for toluene: $\label{eq:c6} % \begin{center} \end{constraint} \begin{center} \end{center} \begin{center} \$

nC10,nC16 and nC34 response factors within 10% of each other:

C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

R.L. = Reporting Limit

NC = Not Calculated

Test methods may be modified from specified reference method unless indicated by an $\,^\star$

Unless otherwise noted all extraction, analysis, QC requirements and limits for holding time were met. If analyzed for F4 and F4G they are not to be summed but the greater of the two numbers are to be used in application to the CWS PHC

QC will be made available upon request.

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
Demonstra	11	D.I	Limita	Date Collected	2023-Apr-21
Parameter pH @25°C	Units pH units	R.L.	10.5, 8.5	SAN, STORM	8.00
Fluoride	mg/L	0.1	10	SAN	<0.1
BOD5	mg/L	3	300, 15	SAN, STORM	<3
Total Suspended Solids	mg/L	3	350, 15	SAN, STORM	32
Phosphorus (Total)	mg/L	0.01	10, 0.4	SAN, STORM	0.03
Total Kjeldahl Nitrogen	mg/L	0.1	100	SAN	0.1
Cyanide (Total)	mg/L	0.005	2, 0.02	SAN, STORM	<0.005
Phenolics	mg/L	0.001	1.0, 0.008	SAN, STORM	<0.001
Hardness (as CaCO3)	mg/L	-			412
Aluminum (Total)	mg/L	0.01	50	SAN	0.81
Barium (Total)	mg/L	0.001			0.034
Beryllium (Total)	mg/L	0.001			<0.001
Iron (Total)	mg/L	0.005			1.16
Manganese (Total)	mg/L	0.001	5, 0.05	SAN, STORM	0.037
Tin (Total)	mg/L	0.05	5	SAN	<0.05
Titanium (Total)	mg/L	0.005	5	SAN	0.025
Tungsten (Total)	mg/L	0.01			<0.01
Zinc (Total)	mg/L	0.005	2, 0.04	SAN, STORM	0.013
Zirconium (Total)	mg/L	0.003			<0.003
Antimony (Total)	mg/L	0.0001	5	SAN	0.0006
Arsenic (Total)	mg/L	0.0001	1, 0.02	SAN, STORM	0.0004

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
Parameter	Units	R.L.	Limits	Sample I.D. Date Collected	23-008175-1 2023-Apr-21
Cadmium (Total)	mg/L	0.000015	2, 0.008	SAN, STORM	0.000016
Chromium (Total)	mg/L	0.001	2, 0.08	SAN, STORM	<0.001
Cobalt (Total)	mg/L	0.0001	5	SAN	0.0005
Copper (Total)	mg/L	0.0001	2, 0.04	SAN, STORM	0.0019
Lead (Total)	mg/L	0.00002	1, 0.12	SAN, STORM	0.00050
Molybdenum (Total)	mg/L	0.0001	5	SAN	0.0015
Nickel (Total)	mg/L	0.0002	2, 0.08	SAN, STORM	0.0025
Selenium (Total)	mg/L	0.001	1, 0.02	SAN, STORM	<0.001
Silver (Total)	mg/L	0.0001	5, 0.12	SAN, STORM	<0.0001
Thallium (Total)	mg/L	0.00005			<0.00005
Uranium (Total)	mg/L	0.00005			0.00147
Vanadium (Total)	mg/L	0.0001			0.0007
Chromium (VI)	mg/L	0.001	0.04	STORM	<0.001
Mercury	mg/L	0.00002	0.01, 0.0004	SAN, STORM	<0.00002

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
Parameter	Units	R.L.	Limits	Sample I.D. Date Collected	23-008175-1 2023-Apr-21
Acetone	μg/L	30			<30
Benzene	mg/L	0.0005	0.01, 0.002	SAN, STORM	<0.0005
Bromodichloromethane	μg/L	2			<2
Bromoform	μg/L	5			<5
Bromomethane	μg/L	0.5			<0.5
Carbon Tetrachloride	μg/L	0.2			<0.2
Chlorobenzene	μg/L	0.5			<0.5
Chloroform	mg/L	0.001	0.04, 0.002	SAN, STORM	<0.001
Dibromochloromethane	μg/L	2			<2
Ethylene Dibromide	μg/L	0.2			<0.2
Dichlorobenzene,1,2-	mg/L	0.0005	0.05, 0.0056	SAN, STORM	<0.0005
Dichlorobenzene,1,3-	μg/L	0.5			<0.5
Dichlorobenzene,1,4-	mg/L	0.0005	0.08, 0.0068	SAN, STORM	<0.0005
Dichlorodifluoromethane (Freon 12)	μg/L	2			<2
Dichloroethane,1,1-	μg/L	0.5			<0.5
Dichloroethane,1,2-	μg/L	0.5			<0.5
Dichloroethylene,1,1-	μg/L	0.5			<0.5
Dichloroethylene,1,2-cis-	mg/L	0.0005	0.0056	STORM	<0.0005
Dichloroethylene,1,2-trans-	μg/L	0.5			<0.5
Dichloropropane,1,2-	μg/L	0.5			<0.5
Dichloropropene,1,3-cis-	µg/L	0.5			<0.5

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits		-
Dichloropropene,1,3-cis+trans- (Calculated)	μg/L	0.5			<0.5
Dichloropropene,1,3-trans-	mg/L	0.0005	0.14, 0.0056	SAN, STORM	<0.0005
Ethylbenzene	mg/L	0.0005	0.16, 0.002	SAN, STORM	<0.0005
Hexane	μg/L	5			<5
Dichloromethane (Methylene Chloride)	mg/L	0.005	2, 0.0052	SAN, STORM	<0.005
Methyl Ethyl Ketone	μg/L	20			<20
Methyl Isobutyl Ketone	μg/L	20			<20
Methyl tert-Butyl Ether (MTBE)	μg/L	2			<2
Styrene	μg/L	0.5			<0.5
Tetrachloroethane,1,1,1,2-	μg/L	0.5			<0.5
Tetrachloroethane,1,1,2,2-	mg/L	0.0005	1.4, 0.017	SAN, STORM	<0.0005
Tetrachloroethylene	mg/L	0.0005	1, 0.0044	SAN, STORM	<0.0005
Toluene	mg/L	0.0005	0.016, 0.002	SAN, STORM	<0.0005
Trichloroethane,1,1,1-	μg/L	0.5			<0.5
Trichloroethane,1,1,2-	μg/L	0.5			<0.5
Trichloroethylene	mg/L	0.0005	0.4, 0.0076	SAN, STORM	<0.0005
Trichlorofluoromethane (Freon 11)	μg/L	5			<5
Vinyl Chloride	μg/L	0.2			<0.2
Xylene, m,p-	μg/L	1			<1
Xylene, m,p,o-	mg/L	0.0011	0.0044	STORM	<0.0011
Xylene, o-	μg/L	0.5			<0.5

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits		-
PHC F1 (C6-C10)	μg/L	25			<25
PHC F2 (>C10-C16)	μg/L	50			<50
PHC F3 (>C16-C34)	μg/L	400			<400
PHC F4 (>C34-C50)	μg/L	400			<400
Oil and Grease (Mineral)	mg/L	1.0	15	SAN	<1.0
Oil and Grease (Anim/Veg)	mg/L	1.0	150	SAN	3.6

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
Parameter	Units	R.L.	Limits	Sample I.D. Date Collected	23-008175-1 2023-Apr-21
Acenaphthene	μg/L	0.05			<0.05
Acenaphthylene	μg/L	0.05			<0.05
Anthracene	μg/L	0.05			<0.05
Benzo[a]anthracene	μg/L	0.05			<0.05
Benzo(a)pyrene	μg/L	0.01			<0.01
Benzo(b)fluoranthene	μg/L	0.05			<0.05
Benzo(g,h,i)perylene	μg/L	0.05			<0.05
Benzo(k)fluoranthene	μg/L	0.05			<0.05
Bis(2-ethylhexyl) Phthalate	mg/L	0.005	0.012, 0.0088	SAN, STORM	<0.005
Chrysene	μg/L	0.05			<0.05
Dibenzo(a,h)anthracene	μg/L	0.05			<0.05
Di-n-Butyl Phthalate	mg/L	0.001	0.08, 0.015	SAN, STORM	<0.001
Dichlorobenzidine,3,3'-	mg/L	0.0005	0.002, 0.0008	SAN, STORM	<0.0005
Fluoranthene	μg/L	0.05			<0.05
Fluorene	μg/L	0.05			<0.05
Indeno(1,2,3,-cd)Pyrene	μg/L	0.05			<0.05
Methylnaphthalene,1-	μg/L	0.05			<0.05
Methylnaphthalene,2-(1-)	μg/L	1			<1
Methylnaphthalene,2-	μg/L	0.05			<0.05
Naphthalene	μg/L	0.05			<0.05
Pentachlorophenol	mg/L	0.0002	0.005, 0.002	SAN, STORM	<0.0002 (Ph)

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D. Date Collected	23-008175-1 2023-Apr-21
Parameter	Units	R.L.	Limits		-
Phenanthrene	μg/L	0.05			<0.05
Pyrene	μg/L	0.05			<0.05
Total PAH	mg/L	0.0001	0.005, 0.002	SAN, STORM	<0.0001
				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits		-
Poly-Chlorinated Biphenyls (PCB's)	mg/L	0.00005	0.001, 0.0004	SAN, STORM	<0.00017
Identification Comment	-	-			-
Hexachlorobenzene	mg/L	0.00001	0.0001, 0.00004	SAN, STORM	<0.00001
Lindane (Hexachlorocyclohexane, Gamma)	mg/L	0.0004	0.1, 0.04	SAN, STORM	<0.0004
Mirex	mg/L	0.001	0.1, 0.04	SAN, STORM	<0.001
DDT (Total)	mg/L	0.00001	0.0001, 0.00004	SAN, STORM	<0.00001
Chlordane (Alpha + Gamma)	mg/L	0.00005	0.1, 0.04	SAN, STORM	<0.00005
Aldrin + Dieldrin	mg/L	0.00002	0.0002, 0.00008	SAN, STORM	<0.00002

REPORT No: 23-008175 - Rev. 0

Subcontracted Analyses				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits		-
Nonylphenol Monoethoxylate	μg/L	-			<10
Nonylphenol Diethoxylate	μg/L	-			<10
Nonylphenols	mg/L	-	0.001, 0.001	SAN, STORM	<0.001
Nonylphenol Ethoxylates	mg/L	-	0.01, 0.01	SAN, STORM	<0.01

Comments:

Phenol (SS) fails low

Chromium (VI) result is based on total Chromium

: City of Owen Sound Sewer Use By-Law SAN: Sanitary Sewer By Law STORM: Storm Sewer By Law

Summary of Exceedances		
Storm Sewer By Law		
BH/MW 25	Found Value	Limit
Total Suspended Solids	32	15



CERTIFICATE OF ANALYSIS

Final Report

C A D U C E N I R O N M E N T A L LA B O R A T O R E S

Client committed. Quality assured. Canadian owned.

C.O.C.: G115006 REPORT No: 23-008175 - Rev. 0

Report To:

Tatham Engineering 115 Sandford Fleming Drive

Suite 200

Collingwood, ON L9Y 5A6

CADUCEON Environmental Laboratories

112 Commerce Park Dr Unit L

Barrie, ON L4N 8W8

Attention: Alicia Kimberley

DATE RECEIVED: 2023-Apr-22 CUSTOMER PROJECT: 121387

DATE REPORTED: 2023-May-08 P.O. NUMBER: 9th Ave E Owen Sound

SAMPLE MATRIX: Ground Water

Analyses	Qty	Site Analyzed	Authorized	Date Analyzed	Lab Method	Reference Method
Chromium VI (Liquid)	1	OTTAWA	CBURKE	2023-May-05	D-CRVI-01	MECP E3056
ICP/MS Total (Liquid)	1	OTTAWA	TPRICE	2023-Apr-28	D-ICPMS-01	EPA 6020
ICP/OES Total (Liquid)	1	OTTAWA	NHOGAN	2023-Apr-26	D-ICP-01	SM 3120B
ICP/OES (Liquid)	1	OTTAWA	NHOGAN	2023-Apr-25	D-ICP-01	SM 3120B
Mercury (Liquid)	1	OTTAWA	APRUDYVUS	2023-Apr-27	D-HG-02	SM 3112B

R.L. = Reporting Limit

NC = Not Calculated

Test methods may be modified from specified reference method unless indicated by an $\,^\star$

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits		-
Aluminum	μg/L	10	75	INTERIM	41
Hardness (as CaCO3)	mg/L	-			412
Aluminum (Total)	mg/L	0.01			0.81
Boron (Total)	μg/L	5	200	INTERIM	53
Calcium (Total)	mg/L	0.02			81.3
Iron (Total)	μg/L	5	300	PWQO	1160
Magnesium (Total)	mg/L	0.02			50.9
Manganese (Total)	mg/L	0.001			0.037
Tin (Total)	mg/L	0.05			<0.05
Titanium (Total)	mg/L	0.005			0.025
Tungsten (Total)	μg/L	10	30	INTERIM	<10
Zinc (Total)	μg/L	5	20, 30	INTERIM, PWQO	13
Zirconium (Total)	μg/L	3	4	INTERIM	<3
Antimony (Total)	μg/L	0.1	20	INTERIM	0.6
Arsenic (Total)	μg/L	0.1	5, 5	INTERIM, PWQO	0.4
Beryllium (Total)	μg/L	0.1	11	PWQO	<0.1
Cadmium (Total)	μg/L	0.015	0.1, 0.2	INTERIM, PWQO	0.016
Chromium (Total)	mg/L	0.001			<0.001
Cobalt (Total)	μg/L	0.1	0.9	INTERIM	0.5
Copper (Total)	μg/L	0.1	5	INTERIM	1.9
Lead (Total)	μg/L	0.02	1, 5	INTERIM, PWQO	0.50

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
Parameter	Units	R.L.	Limits	Sample I.D. Date Collected	23-008175-1 2023-Apr-21
Molybdenum (Total)	μg/L	0.1	40	INTERIM	1.5
Nickel (Total)	μg/L	0.2	25	PWQO	2.5
Selenium (Total)	μg/L	1	100	PWQO	<1
Silver (Total)	μg/L	0.1	0.1	PWQO	<0.1
Thallium (Total)	μg/L	0.05	0.3, 0.3	INTERIM, PWQO	<0.05
Uranium (Total)	μg/L	0.05	5	INTERIM	1.47
Vanadium (Total)	μg/L	0.100	6	INTERIM	0.700
Chromium (VI)	μg/L	1.0	1	PWQO	<1.0
Mercury	μg/L	0.02	0.2	PWQO	<0.02

Chromium (VI) result is based on total Chromium

: PWQO Limits INTERIM: Interim PWQO

PWQO: PWQO

 Summary of Exceedances

 PWQO
 Found Value
 Limit

 Iron (Total)
 1160
 300



CERTIFICATE OF ANALYSIS

121387

Final Report

C.O.C.: G115006 REPORT No: 23-008175 - Rev. 0

Report To:

Tatham Engineering 115 Sandford Fleming Drive Suite 200

Collingwood, ON L9Y 5A6

Attention: Alicia Kimberley

DATE RECEIVED:

on. Alicia Miliberiey

DATE REPORTED: 2023-May-08 P.O. NUMBER: 9th Ave E Owen Sound

SAMPLE MATRIX: Ground Water

Analyses Qty Site Analyzed Authorized Date Analyzed Lab Method Reference Method PHC F1 (Liquid) RICHMOND HILL **FLENA** 2023-Apr-27 C-VPHW-01 **MECP E3421** 1 PHC F2-4 (Liquid) 1 **KINGSTON KPARKER** 2023-Apr-26 PHC-W-001 **MECP E3421** VOC-Volatiles (Liquid) RICHMOND HILL 2023-Apr-27 **FLENA** C-VOC-02 EPA 8260

 $\mu g/g$ = micrograms per gram (parts per million) and is equal to mg/Kg

F1 C6-C10 hydrocarbons in $\mu g/g$, (F1-btex if requested)

F2 C10-C16 hydrocarbons in $\mu g/g$, (F2-napth if requested)

F3 C16-C34 hydrocarbons in µg/g, (F3-pah if requested)

F4 C34-C50 hydrocarbons in µg/g

This method complies with the Reference Method for the CWS PHC and is $% \left(1\right) =\left(1\right) \left(1\right) +\left(1\right) \left(1\right) \left(1\right) +\left(1\right) \left(1\right) \left($

validated for use in the laboratory.

Any deviations from the method are noted and reported for any particular sample.

2023-Apr-22

nC6 and nC10 response factor is within 30% of response factor for toluene:

nC10.nC16 and nC34 response factors within 10% of each other:

C50 response factors within 70% of nC10+nC16+nC34 average:

Linearity is within 15%:

All results expressed on a dry weight basis.

Unless otherwise noted all chromatograms returned to baseline by the retention

time of nC50.

R.L. = Reporting Limit

NC = Not Calculated

Test methods may be modified from specified reference method unless indicated by an $\,^\star$

Unless otherwise noted all extraction, analysis, QC requirements and limits for holding time were met. If analyzed for F4 and F4G they are not to be summed but the greater of the two numbers are to be used in application to the CWS PHC

CADUCEON Environmental Laboratories

112 Commerce Park Dr Unit L

CUSTOMER PROJECT:

Barrie, ON L4N 8W8

QC will be made available upon request.

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
Parameter	Units	R.L.	Limits	Sample I.D. Date Collected Reg 153 - Liquid	23-008175-1 2023-Apr-21
Acetone	μg/L	30	2700	T1GW	<30
Benzene	μg/L	0.5	0.5	T1GW	<0.5
Bromodichloromethane	μg/L	2	2	T1GW	<2
Bromoform	μg/L	5	5	T1GW	<5
Bromomethane	μg/L	0.5	0.89	T1GW	<0.5
Carbon Tetrachloride	μg/L	0.2	0.2	T1GW	<0.2
Chlorobenzene	μg/L	0.5	0.5	T1GW	<0.5
Chloroform	μg/L	1	2	T1GW	<1
Dibromochloromethane	μg/L	2	2	T1GW	<2
Ethylene Dibromide	μg/L	0.2	0.2	T1GW	<0.2
Dichlorobenzene,1,2-	μg/L	0.5	0.5	T1GW	<0.5
Dichlorobenzene,1,3-	μg/L	0.5	0.5	T1GW	<0.5
Dichlorobenzene,1,4-	μg/L	0.5	0.5	T1GW	<0.5
Dichlorodifluoromethane (Freon 12)	μg/L	2	590	T1GW	<2
Dichloroethane,1,1-	μg/L	0.5	0.5	T1GW	<0.5
Dichloroethane,1,2-	μg/L	0.5	0.5	T1GW	<0.5
Dichloroethylene,1,1-	μg/L	0.5	0.5	T1GW	<0.5
Dichloroethylene,1,2-cis-	μg/L	0.5	1.6	T1GW	<0.5
Dichloroethylene,1,2-trans-	μg/L	0.5	1.6	T1GW	<0.5
Dichloropropane,1,2-	μg/L	0.5	0.5	T1GW	<0.5
Dichloropropene,1,3-cis-	μg/L	0.5			<0.5

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
Parameter	Units	R.L.	Limits	Date Collected Reg 153 - Liquid	2023-Apr-21
Dichloropropene,1,3-cis+trans- (Calculated)	µg/L	0.5	0.5	T1GW	<0.5
Dichloropropene,1,3-trans-	μg/L	0.5			<0.5
Ethylbenzene	μg/L	0.5	0.5	T1GW	<0.5
Hexane	μg/L	5	5	T1GW	<5
Dichloromethane (Methylene Chloride)	μg/L	5	5	T1GW	<5
Methyl Ethyl Ketone	μg/L	20	400	T1GW	<20
Methyl Isobutyl Ketone	μg/L	20	640	T1GW	<20
Methyl tert-Butyl Ether (MTBE)	μg/L	2	15	T1GW	<2
Styrene	μg/L	0.5	0.5	T1GW	<0.5
Tetrachloroethane,1,1,1,2-	μg/L	0.5	1.1	T1GW	<0.5
Tetrachloroethane,1,1,2,2-	μg/L	0.5	0.5	T1GW	<0.5
Tetrachloroethylene	μg/L	0.5	0.5	T1GW	<0.5
Toluene	μg/L	0.5	0.8	T1GW	<0.5
Trichloroethane,1,1,1-	μg/L	0.5	0.5	T1GW	<0.5
Trichloroethane,1,1,2-	μg/L	0.5	0.5	T1GW	<0.5
Trichloroethylene	μg/L	0.5	0.5	T1GW	<0.5
Trichlorofluoromethane (Freon 11)	μg/L	5	150	T1GW	<5
Vinyl Chloride	μg/L	0.2	0.5	T1GW	<0.2
Xylene, m,p-	μg/L	1			<1
Xylene, m,p,o-	μg/L	1.1	72	T1GW	<1.1
Xylene, o-	μg/L	0.5			<0.5

REPORT No: 23-008175 - Rev. 0

				Client I.D.	BH/MW 25
				Sample I.D.	23-008175-1
				Date Collected	2023-Apr-21
Parameter	Units	R.L.	Limits	Reg 153 - Liquid	-
PHC F1 (C6-C10)	μg/L	25	420	T1GW	<25
PHC F2 (>C10-C16)	μg/L	50	150	T1GW	<50
PHC F3 (>C16-C34)	μg/L	400	500	T1GW	<400
PHC F4 (>C34-C50)	μg/L	400	500	T1GW	<400

Reg 153 - Liquid: Reg 153 - Liquid T1GW: R153 Tbl. 1 - GW

GENERAL SAMPLE SUBMISSION FORM	SAMPLES SUBMITTE	D TO:			TE	STIN	G REC	QUIRE	MENTS	3						RE	PORT NUM	IBER (Lab Us	e)
CADUCE N ENVIRONMENTAL LABORATORIES Citent committed. Quelty assured. Proudly Canadian.	Kingston Ottawa Richmond Hill Barrie Windsor	×	X	O'Reg 153/04 O'Reg 406/19 RPI Coarse MISA Other:	Table	(1-9) (1-9.1 X		PWQ			P Table	Agricu O'Reg Landfi	558 TCL II Monito		7	3-1	00 S	817	S
Are any samples to be submitted intended for Human	Consumption under any	Drinking V	Vater Regulations	s?		Yes			No	(f yes, s	ubmit a	II Drink	ing Wat	er Sam	oles on a C		er Chain of Cu	
Organization: Tatham Engineering Address:	King St.	Invoicing	Address (if different):						YSES R	EQUES	TED						OUND SERVICED (see back page)	
ontrembley@tathameng.com Tol: a kimber by @tathameng.com Ba	rrie, ON.	Project Na	ame or#:		Pwao metals	153/04	PHCs		men Sund Septerion						Suspected Highly Contaminated		*Must be and Platinum* Gold* Silver Bronze	100% 50% S	Surcharge Surcharge Surcharge Surcharge
Kgardner@tathameng.com	Q3091_Tatham	1213 ^d Additiona	87 - 9th A	ME	180	49	2	5	Š						ected Hi	×	Standard Specific D	5-7 da	_
Additional Int (email, coll, etc): iniller & tothameng.com Sample Matrix Lege	nd: WW=Waste Water, SW=Su	0	wen Souno			lid Sluc			9	iment, P	C=Paint	Chins	F=Filter	Oil = Oi	.0.7] Specific D	ite.	
Lab Sample mauta Lege	S.P.L.	Sample	Date Collected	Time		iid Olde		Inc	icate Te	st For Ea	ch Sam	ole		OII = OI	x		ield	# Bottles/	Field Filtered
No. Sample Source and/or Sample Identification	(Watertrax)	Matrix *	(yy-mm-dd)	Collected	~	·				Mark In	The Box	Provide	d	T		pН	Temp.	Sample	Y/N
BH/MW 25		GW	23.04.21	13.30	^	X	Х	X	Λ									20	
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gen cherr(f) + +/g(f) + metals																	20170044	05.000.00	
SAMPLE SUBMISSION INFORMATION	SHIPPING IP Courier (Client account)	NFORMATIO		REPORT Report by Fax	ING /	INVOIC	ING		Receive	ed By (p						Signature:	DRATORY U	B3	
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Appendix F: Water Taking Estimates



Phase 1

$$Q = Kx \frac{H^2 - h^2}{L_0}$$

-0				
Ground Elevation		247.3	m asl	BH/MW23
Highest Groundwater Elevation		247.4	m asl	BH/MW23 on 04/21/2023
Lowest Proposed Excavation		244.8	m asl	Assume 2.5 m inverts
Target Water Level		243.8	m asl	Assume 1 m of drawdown
Aquifer Bottom		243.8	m asl	
Hydraulic Conductivity	K	1.50E-06	m/s	
Length of Excavation	X	650	m	
Width of Excavation	а	4	m	
Calculated Parameters				
Water level above aquifer bottom	Н	3.6	m	
Target water level above aquifer bottom	h	0	m	
Radius of Influence	R_0	13	m	
Length of Influence ($L_0=R_0/2$)	Lo	7	m	
Precipitation		26,000	L/day	
Construction Dewatering Flow Rate - Steady State	Q	165,100	L/day	
Maximum Construction Dewatering Flow Rate (safety				
factor of 2)	2Q	330,200	L/day	
Maximum Construction Dewatering Flow Rate (safety				
factor of 2) with 10 mm rainfall event	2Q	356,200	L/day	
Maximum Construction Dewatering Flow Rate (safety				
factor of 2) with 10 mm rainfall event per 100 m of				
trench	2Q	54,800	L/day/100 m	



Phase 2

$$Q = Kx \frac{H^2 - h^2}{L_0}$$

	248.8	m asl	BH/MW14
	248.2	m asl	BH/MW14 on 02/13/2023
	246.3	m asl	Assume 2.5 m inverts
	245.3	m asl	Assume 1 m of drawdown
	245.3	m asl	
K	1.50E-06	m/s	
Χ	860	m	
а	4	m	
Н	2.9	m	
h	0	m	
R_0	11	m	
Lo	5	m	
	34,400	L/day	
Q	175,900	L/day	
2Q	351,800	L/day	
2Q	386,200	L/day	
2Q	44,900	L/day/100 m	
	x a a H h R ₀ L ₀ Q 2Q 2Q	248.2 246.3 245.3 X 245.3 K 1.50E-06 X 860 a 4 H 2.9 h 0 R ₀ 11 L ₀ 5 34,400 Q 175,900 2Q 351,800 2Q 386,200	x 860 m a 4 m H 2.9 m h 0 m R ₀ 11 m L ₀ 5 m 34,400 L/day Q 175,900 L/day 2Q 351,800 L/day 2Q 386,200 L/day



Phase 3

$$Q = Kx \frac{H^2 - h^2}{L_0}$$

	237.7	m asl	BH/MW9
	235.5	m asl	BH/MW9 on 02/13/2023
	234.2	m asl	Assume 3.5 m inverts
	233.2	m asl	Assume 1 m of drawdown
	233.2	m asl	
K	1.50E-06	m/s	
Χ	1000	m	
а	4	m	
Н	2.3	m	
h	0	m	
R_0	8	m	
Lo	4	m	
	40,000	L/day	
Q	162,300	L/day	
2Q	324,600	L/day	
2Q	364,600	L/day	
2Q	36,460	L/day/100 m	
	X a H h R ₀ L ₀ Q 2Q 2Q	H 2.3 h 0 R ₀ 8 L ₀ 40,000 Q 324,600 2Q 364,600	x 1000 m a 4 m H 2.3 m h 0 m R ₀ 8 m L ₀ 4 m 40,000 L/day Q 162,300 L/day 2Q 324,600 L/day 2Q 364,600 L/day

Appendix G: Water Taking Plan

Water Taking Plan

CONSTRUCTION DEWATERING DISCHARGE RATE AND ZONE OF INFLUENCE

The Radius of Influence (ROI) and temporary dewatering discharge rates were calculated in Section 5.1 and the details are summarized below:

ZONE	DESCRIPTION	ROI (m)	CONSTRUCTION DEWATERING FLOW RATE (L/day)	CONSTRUCTION DEWATERING FLOW RATE INLCUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT (L/day)	CONSTRUCTION DEWATERING FLOW RATE INCLUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT PER 100 m LENGTH TRENCH (L/day/100 m)
1	Phase 1	13	165,100	356,200	54,800
2	Phase 2	11	175,900	386,200	44,900
3	Phase 3	8	162,300	364,600	36,460

POTENTIAL SETTLEMENT AND MONITORING

Portion of the site is surrounded by residential, industrial and/or commercial structures. Some structure may lie within the dewatering ROI; therefore, there is the potential for settlement related impacts. Prior to construction dewatering, a settlement analysis is to be completed by the geotechnical engineer, to provide input on the recommended monitoring and/or mitigative actions (if any).

Another cause of significant dewatering related settlement is due to pumping of fines through the system. It is imperative any dewatering systems shall be designed and installed adequately to ensure no soil is conveyed through the system. Sufficient filtering techniques should be incorporated at the entry point to avoid migration of fines in the pumping and/or dewatering system. The turbidity of pumped water should be monitored daily to ensure the minimal fines are being conveyed.

POTENTIAL IMPACT ON OTHER WATER USERS

Temporary dewatering activities are not anticipated to impact any water well users as municipal water is available to the nearest neighboring properties, and the proposed development consists of relatively shallow works.

REDUCTION OF GROUNDWATER FLOW TO WATERBODIES

Given the short duration of the proposed construction dewatering and that the water removed will be returned back to the same watershed, dewatering activities are not anticipated to have negative impacts to the nearest waterbody.

WATER QUANTITY, QUALITY AND GROUNDWATER LEVEL MONITORING PROGRAM

Based on baseline groundwater quality analysis, elevated concentrations of Total Suspended Solids (TSS) and iron were noted with respect to the Owen Sound Sewer Use Bylaw Criteria and Provincial Water Quality Objectives (PWQO), respectively. As such the dewatering discharge can only be directed to the storm sewer and/or surface provided that a filtration system allows groundwater quality to meet the Owen Sound Sewer By-Law Criteria, Provincial Water Quality Objectives (PWQO), and the applicable O.Reg.153/04, as amended, Site Condition Standards.

It is recommended that discharge be treated by a sediment control facility such as sediment/filtration bags or a decantation tank.

If water quality parameters exceed the City of Owen Sound Sewer By-Law Criteria and/or PWQO during construction dewatering, standard treatment options should be evaluated and/or the system should be shut down.

WATER QUALITY MONITORING AND POTENTIAL TREATMENT PLAN

The discharge and monitoring plan are detailed in Table G-1, below.

GROUNDWATER LEVEL MONITORING PROGRAM

The ground water level monitoring program is detailed in Table G-1, below.

DISCHARGE RATE MONITORING

Daily groundwater takings are to be measured and recorded using a flow measuring device during construction dewatering by the contractor, in accordance with O.Reg. 63/16. The total daily takings shall be recorded for the duration of the EASR and be submitted through the MECP online reporting system.

SUMMARY OF QUALIFICATIONS

Alicia Kimberley is a licensed professional geoscientist with a Bachelors and Masters degree in Earth Sciences from McMaster University and the University of Waterloo, respectively. She has twelve years of professional experience with geoenvironmental and hydrogeological assessments.

Her experiences include the design and execution of aquifer testing, in-situ groundwater sampling, groundwater modelling, and preparation of hydrogeological reports to support EASR registry.

Kimberly Gardner obtains a bachelor's degree in Environmental Engineering from the University of Guelph and is a registered Engineering Intern with PEO. She has over three years' experience with environmental and hydrogeological assessments. Her experiences include the completion of Phase One and Two Site Assessments and excess soil programs, field investigations (soil and groundwater sampling) and preparation of a variety of environmental/hydrogeological reports.

DATE OF PLAN PREPARATION

This plan was prepared on May 10, 2023.

Table G-1: Water Quality Monitoring Plan for Dewatering Discharge to Surface

PERIOD	MONITORING LOCATION	PARAMETERS	MONITORING FREQUENCY	TRIGGIER FOR MITIGATION	MITIGATION MEASURES/COMMENTS	
Trial Dewatering	Dewatering Discharge	City of Owen Sound Sewer By-Law Criteria and PWQO Metals	Once during trial dewatering	Exceeds the City of Owen Sound Sewer By-Law Criteria and/or PWQO	Modify treatment method and/or shut down.	
During Construction	Dewatering Discharge	City of Owen Sound Sewer By-Law Criteria and PWQO Metals	Weekly, then every four weeks after three consecutive weekly compliant samples	City of Owen Sound Sewer By- Law Criteria and/or PWQO	Modify/change treatment method and/or shut down.	
		Turbidity	Daily until stable, then weekly. Minimum of five samples	Exceeds 15 NTU	_	
	Discharge Point	Impact Assessment	At each sampling event	Sedimentation, erosion	Reduce pumping and/or improve sediment/erosion control measures	
	On-site monitoring wells	Water level meter	Every two weeks	Water level to be no more than 1 m lower than proposed depth of excavation	Reduce pumping	

PERIOD	MONITORING LOCATION	PARAMETERS	MONITORING FREQUENCY	TRIGGIER FOR MITIGATION	MITIGATION MEASURES/COMMENTS
During Construction (cont'd)	Structures closest to the excavations 9 th Avenue East	Settlement	Weekly (if needed)	Assessment by geotechnical engineer and/or structural engineer	Minimize the dewatering scope by reducing and/or staging the excavation or by installing a barrier. Alternatively other potential causes should be minimized.
Post Construction	On-site monitoring wells	Water level meter	Every two weeks for four weeks, then every four weeks until 90% recovery	Water level recovery less than 90% of baseline level	Continue monitoring

Appendix H: Discharge Taking Plan

Discharge Taking Plan

CONSTRUCTION DEWATERING DISCHARGE RATE AND ZONE OF INFLUENCE

The Radius of Influence (ROI) and temporary dewatering discharge rates were calculated in Section 5.1 and the details are summarized below:

ZONE	DESCRIPTION	ROI (m)	CONSTRUCTION DEWATERING FLOW RATE (L/day)	CONSTRUCTION DEWATERING FLOW RATE INLCUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT (L/day)	CONSTRUCTION DEWATERING FLOW RATE INCLUDING SAFETY FACTOR OF 2 AND A 10 mm RAIN EVENT PER 100 m LENGTH TRENCH (L/day/100 m)
1	Phase 1	13	165,100	356,200	54,800
2	Phase 2	11	175,900	386,200	44,900
3	Phase 3	8	162,300	364,600	36,460

PROPOSED DISCHARGE METHOD AND LOCATION

The preferred discharge location is the storm sewer and/or ground surface. The dewatering discharge will be transported by a hose and/or pipe to the treatment system. Following treatment at a filtration/silt bag or similar and/or sediment tank, the dewatering discharge will be transported by a hose/pipe to the preferred discharge location.

If significant rainfall events occur (including a 100-year storm event), the on-site excavation shall shutdown until storm water infiltration is reduced and the dewatering system can operate efficiently and accurately.

EROSION AND SEDIMENT CONTROL MEASURES

Sediment and erosion control measures will be setup on-site according to typical best management practices.

STATEMENTS

The Water Taking Plan included in Appendix G, including the water quantity and quality monitoring program shall be implemented at the site. No adverse effects on the environment is expected if the plan is adhered to.

SUMMARY OF QUALIFICATIONS

Alicia Kimberley is a licensed professional geoscientist with a Bachelors and Masters degree in Earth Sciences from McMaster University and the University of Waterloo, respectively. She has twelve years of professional experience with geoenvironmental and hydrogeological assessments.

Her experiences include the design and execution of aquifer testing, in-situ groundwater sampling, groundwater modelling, and preparation of hydrogeological reports to support EASR registry.

Kimberly Gardner obtains a bachelor's degree in Environmental Engineering from the University of Guelph and is a registered Engineering Intern with PEO. She has over three years' experience with environmental and hydrogeological assessments. Her experiences include the completion of Phase One and Two Site Assessments and excess soil programs, field investigations (soil and groundwater sampling) and preparation of a variety of environmental/hydrogeological reports.

DATE OF PLAN PREPARATION

This plan was prepared on May 10, 2023.

Appendix G: Property Owner Consultation





File 121387

June 7, 2022

Priya Siya Incorporated 485 9th Avenue East Owen Sound, Ontario N4K 3E2

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100 metres south of Superior Street to 100 metres north of 9th Street
 East:
- storm sewer system between Superior Street and 9th Street East;
- sanitary sewer system between 7th Street East and 8th Street East;
- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

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File 121387

June 7, 2022

Grey Bruce Health Services 1800 8th Street East Owen Sound, Ontario N4K 6M9

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.







File 121387

June 7, 2022

Flato Owen Sound Community 3621 Highway 7 East, Suite 503 Markham, Ontario L3R 0G6

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

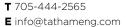
Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

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File 121387

June 7, 2022

Canada Bread Company Limited c/o Corporate Foods Limited 10 Four Seasons Place Etobicoke, Ontario M9B 6H7

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.





File 121387

May 25, 2022

Yusheng Zhao & Amy Yongmei Guo 1150 Superior Street Owen Sound, Ontario N4K 5N8

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.

The purpose of this letter is to initiate dialogue with key property owners and provide more information on the next steps in the Class EA process (refer also to the attached Notice of Study Commencement). We are beginning Phase 2 of the Class EA process, the intent of which is to identify and evaluate alternative solutions to address the noted deficiencies. While most of the alternative solutions will be contained within existing municipal road allowances, one solution for the water distribution system is to implement a looping watermain between 8th Street East and Superior Street (watermain loops provide necessary redundancy in case of system issues) which may require watermain to be installed on private property within dedicated easements.

To appropriately identify and evaluate any potential environmental impacts to the affected properties (which includes 1150 Superior Street) it is necessary to undertake a site investigation to document and characterize the existing field conditions (eg. topography, flora and fauna, wildlife, natural features and





habitat, etc.) which will be considered in the subsequent evaluation. The site investigation will include 2 to 3 site visits/walks (corresponding to spring, summer and/or fall seasons) undertaken by a natural environment scientist to facilitate the necessary observations – there will be no need for vehicle access, disturbance to existing conditions, etc.

To complete the investigation, we will require access to your property and thus would appreciate confirmation of same. Please contact the undersigned via email at abrownridge@tathameng.com to confirm access and coordinate the necessary investigations accordingly. We welcome any further questions, comments or concerns that you may have at this time and note that a formal Public Information Centre (PIC) will be hosted in the future (for which a separate notification will be provided).

Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh

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File 121387

May 25, 2022

White Owl Properties Limited 180 Renfrew Drive Unit 120 Markham, Ontario L3R 9Z2

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.

The purpose of this letter is to initiate dialogue with key property owners and provide more information on the next steps in the Class EA process (refer also to the attached Notice of Study Commencement). We are beginning Phase 2 of the Class EA process, the intent of which is to identify and evaluate alternative solutions to address the noted deficiencies. While most of the alternative solutions will be contained within existing municipal road allowances, one solution for the water distribution system is to implement a looping watermain between 8th Street East and Superior Street (watermain loops provide necessary redundancy in case of system issues) which may require watermain to be installed on private property within dedicated easements.

To appropriately identify and evaluate any potential environmental impacts to the affected properties (which includes 405 9th Avenue East) it is necessary to undertake a site investigation to document and characterize the existing field conditions (eg. topography, flora and fauna, wildlife, natural features and





habitat, etc.) which will be considered in the subsequent evaluation. The site investigation will include 2 to 3 site visits/walks (corresponding to spring, summer and/or fall seasons) undertaken by a natural environment scientist to facilitate the necessary observations - there will be no need for vehicle access, disturbance to existing conditions, etc.

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Yours truly,

Tatham Engineering Limited

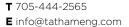
Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

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File 121387

May 25, 2022

Hydro One Networks Incorporated Assessment & Taxation Real Estate 185 Clegg Road Markham, Ontario L6G 1B7

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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The purpose of this letter is to initiate dialogue with key property owners and provide more information on the next steps in the Class EA process (refer also to the attached Notice of Study Commencement). We are beginning Phase 2 of the Class EA process, the intent of which is to identify and evaluate alternative solutions to address the noted deficiencies. While most of the alternative solutions will be contained within existing municipal road allowances, one solution for the water distribution system is to implement a looping watermain between 8th Street East and Superior Street (watermain loops provide necessary redundancy in case of system issues) which may require watermain to be installed on private property within dedicated easements.

To appropriately identify and evaluate any potential environmental impacts to the affected properties (which includes 1025 6th Street East) it is necessary to undertake a site investigation to document and characterize the existing field conditions (eg. topography, flora and fauna, wildlife, natural features and





habitat, etc.) which will be considered in the subsequent evaluation. The site investigation will include 2 to 3 site visits/walks (corresponding to spring, summer and/or fall seasons) undertaken by a natural environment scientist to facilitate the necessary observations – there will be no need for vehicle access, disturbance to existing conditions, etc.

To complete the investigation, we will require access to your property and thus would appreciate confirmation of same. Please contact the undersigned via email at abrownridge@tathameng.com to confirm access and coordinate the necessary investigations accordingly. We welcome any further questions, comments or concerns that you may have at this time and note that a formal Public Information Centre (PIC) will be hosted in the future (for which a separate notification will be provided).

Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

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File 121387

May 25, 2022

Grey County c/o County Clerk 595 9th Avenue East Owen Sound, Ontario N4K 3E3

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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To appropriately identify and evaluate any potential environmental impacts to the affected properties (which includes 595 9th Avenue East) it is necessary to undertake a site investigation to document and characterize the existing field conditions (eg. topography, flora and fauna, wildlife, natural features and





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Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh

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File 121387

June 7, 2022

Great Lakes Management Incorporated 8 Automatic Road Brampton, Ontario L6S 5N4

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

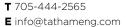
Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

 $\label{thm:consultation} I:\ 2021\ Projects\ 121387\ -\ 9th\ Avenue\ East\ Reconstruction,\ Owen\ Sound\ Documents\ Stakeholder\ Consultation\ Property\ Owner\ Consultation\ L-\ Great\ Lakes\ -\ Property\ Owner\ Consultation\ docx$







File 121387

June 7, 2022

Ashlar Holdings Incorporated 300 Raglan Street Collingwood, Ontario L9Y 3Z1

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100 metres south of Superior Street to 100 metres north of 9th Street
 East;
- storm sewer system between Superior Street and 9th Street East;
- sanitary sewer system between 7th Street East and 8th Street East;
- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

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File 121387

May 25, 2022

2779300 Ontario Incorporated 159 Galbraith Crescent Markham, Ontario L3S 1H5

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100 metres south of Superior Street to 100 metres north of 9th Street
 East:
- storm sewer system between Superior Street and 9th Street East;
- sanitary sewer system between 7th Street East and 8th Street East;
- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.

The purpose of this letter is to initiate dialogue with key property owners and provide more information on the next steps in the Class EA process (refer also to the attached Notice of Study Commencement). We are beginning Phase 2 of the Class EA process, the intent of which is to identify and evaluate alternative solutions to address the noted deficiencies. While most of the alternative solutions will be contained within existing municipal road allowances, one solution for the water distribution system is to implement a looping watermain between 8th Street East and Superior Street (watermain loops provide necessary redundancy in case of system issues) which may require watermain to be installed on private property within dedicated easements.

To appropriately identify and evaluate any potential environmental impacts to the affected properties (which includes 1000 & 1010 Superior Street) it is necessary to undertake a site investigation to document and characterize the existing field conditions (eg. topography, flora and fauna, wildlife, natural features





and habitat, etc.) which will be considered in the subsequent evaluation. The site investigation will include 2 to 3 site visits/walks (corresponding to spring, summer and/or fall seasons) undertaken by a natural environment scientist to facilitate the necessary observations – there will be no need for vehicle access, disturbance to existing conditions, etc.

To complete the investigation, we will require access to your property and thus would appreciate confirmation of same. Please contact the undersigned via email at abrownridge@tathameng.com to confirm access and coordinate the necessary investigations accordingly. We welcome any further questions, comments or concerns that you may have at this time and note that a formal Public Information Centre (PIC) will be hosted in the future (for which a separate notification will be provided).

Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh

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File 121387

June 7, 2022

2736003 Ontario Incorporated 250 10th Street West Owen Sound, Ontario N4K 3R3

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

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File 121387

June 7, 2022

1828915 Ontario Incorporated 23 Locksley Place Brampton, Ontario L6S 2P6

Re: 9th Avenue East Class Environmental Assessment, City of Owen Sound Consultation with Key Property Owners

To Whom It May Concern:

The City of Owen Sound has initiated a Municipal Class Environmental Assessment (Class EA) to address infrastructure, road and sidewalk needs and deficiencies within the 9th Avenue East corridor. It is expected that the deficiencies will require repair, replacement and/or improvements to the following (subject to confirmation following engineering investigations and/or condition assessments):

- water distribution system from 100 metres south of Superior Street to 100 metres north of 9th Street
 East:
- storm sewer system between Superior Street and 9th Street East;
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- road system within the above noted limits; and
- sidewalk system within the above noted limits, including provision of new sidewalk on the west side of 9th Avenue East from 6th Street East to 8th Street East.





Yours truly,

Tatham Engineering Limited

Allan Brownridge, B.E.Sc., P.Eng.

Director, Manager - Municipal Engineering

MJF:rlh Encl.

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Appendix H: Operations Committee Presentation









OPERATIONS COMMITTEE PROJECT UPDATE





AGENDA

- Project Contacts
- Project Objective
- Project Limits
- Phase 1
- Phase 2
- Phase 3
- Questions

Project Contacts







Chris Webb, P.Eng.

Mgr of Engineering Services City of Owen Sound (519) 376-1440, ext. 3300 cwebb@owensound.ca

Mark Figueroa, EIT

Project Manager
Tatham Engineering Limited
(705) 444-2565, ext. 2142
mfigueroa@tathameng.com

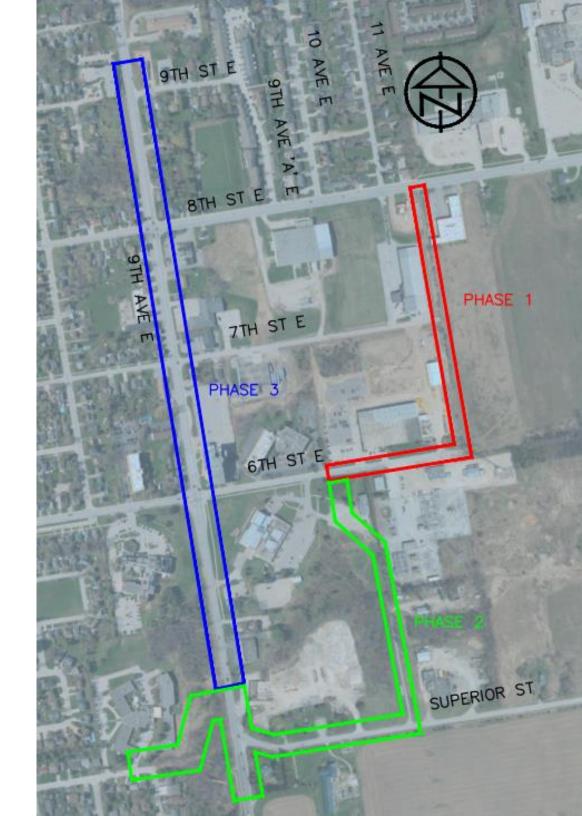
Project Objective



- Address existing needs and deficiencies in the project area in relation to:
 - Underground infrastructure
 - Road
 - Sidewalks

 Improve the overall reliability of the City's water distribution system

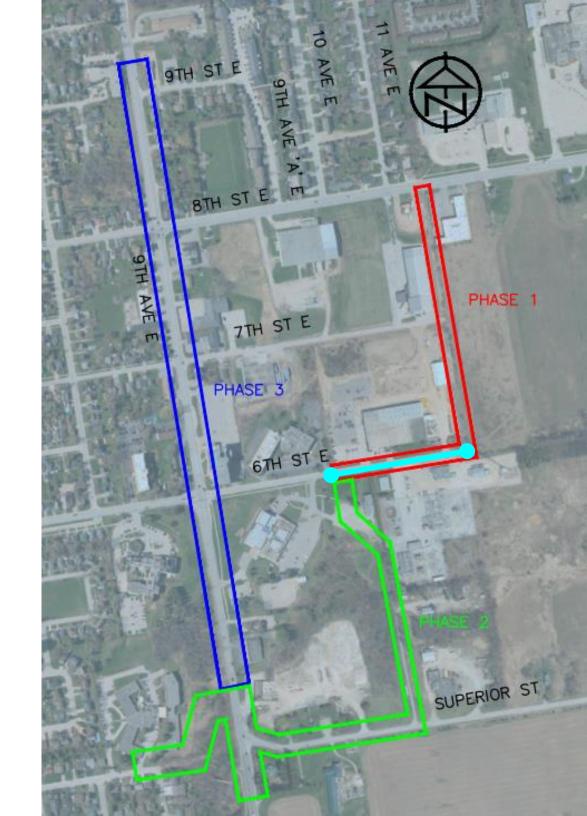
Project Limits



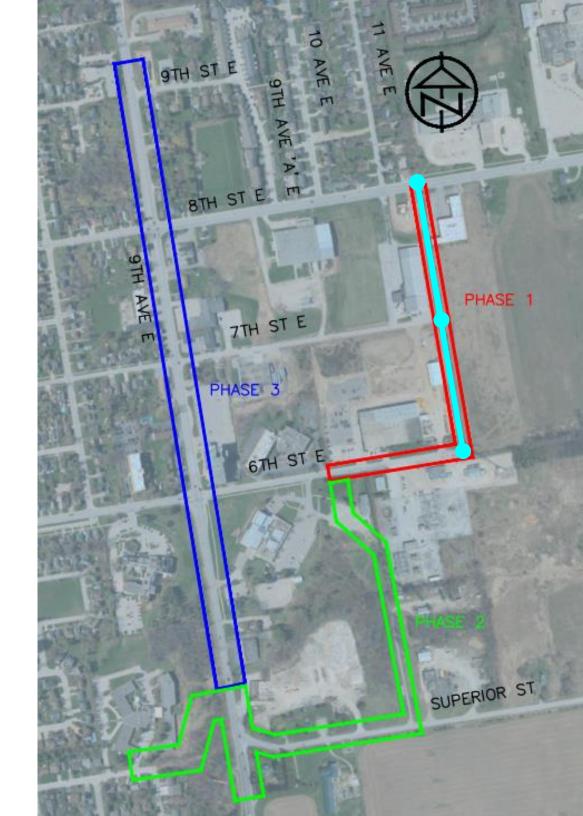
Phase 1

Scope of Work

- REPLACE deteriorated watermain on 6th Street East
 - from dead end
 - to future south looping watermain connection
 - length: 200 metres



- NEW watermain in Cityowned utility corridor
 - from 6th Street East
 - to 8th Street East
 - connection to 7th
 Street East dead end
 - length: 420 metres



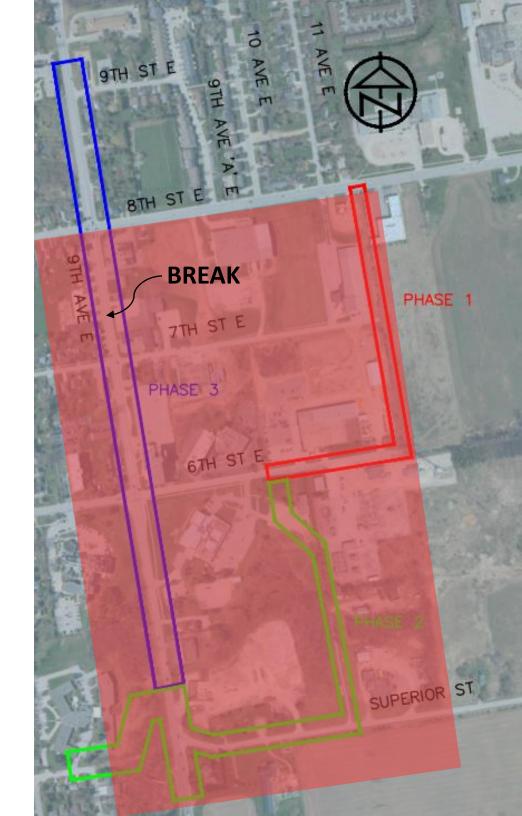
What does this accomplish?

- Improves reliability of water supply on 9th Avenue East
- Limits outages to several hotels, commercial and institutional buildings on 9th Avenue East



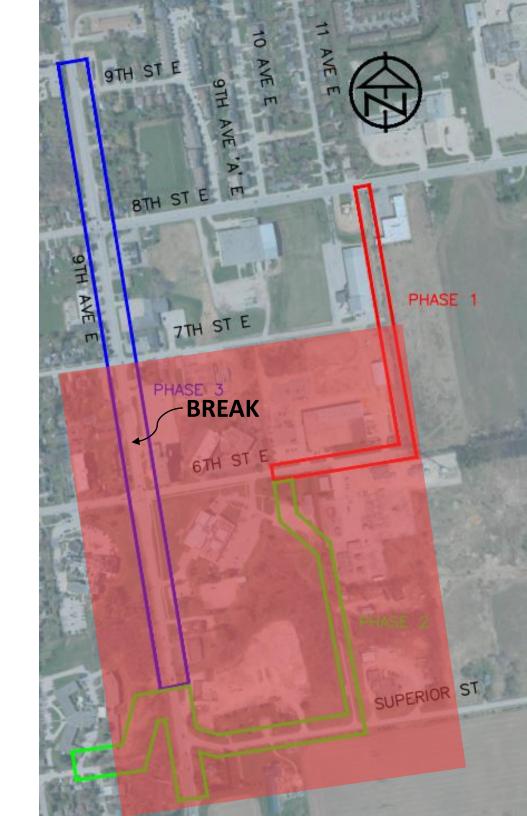
What does this accomplish?

With the current system, a watermain break on 9th
 Avenue East south of 8th
 Street East will interrupt water service for all properties south of the break



What does this accomplish?

With the current system, a watermain break on 9th
 Avenue East south of 8th
 Street East will interrupt water service for all properties south of the break



What does this accomplish?

With the current system, a watermain break on 9th
 Avenue East south of 8th
 Street East will interrupt water service for all properties south of the break



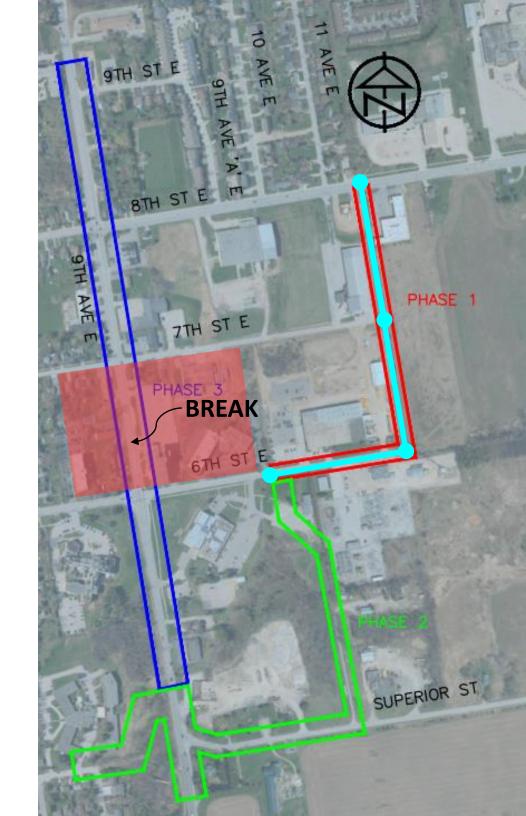
What does this accomplish?

With the Phase 1 loop, only properties in the block with the break will experience water service interruptions



What does this accomplish?

With the Phase 1 loop, only properties in the block with the break will experience water service interruptions



What does this accomplish?

With the Phase 1 loop, only properties in the block with the break will experience water service interruptions





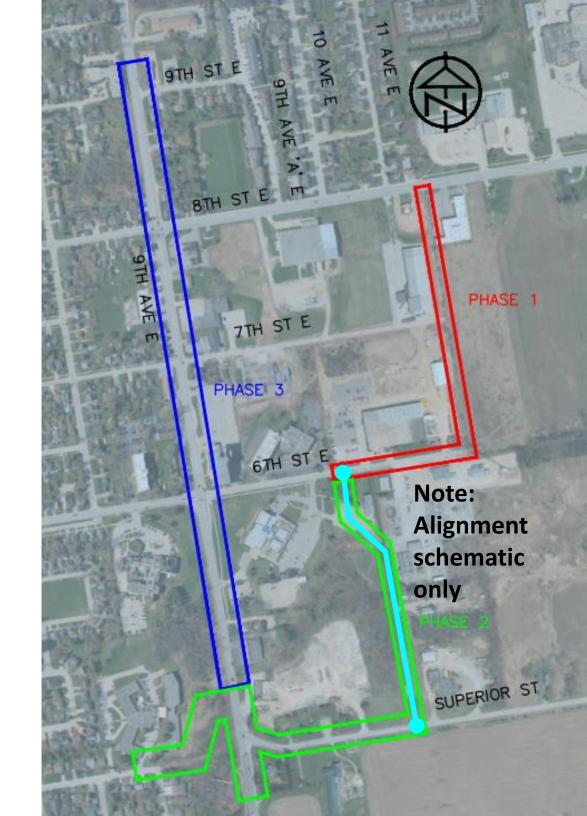
Schedule



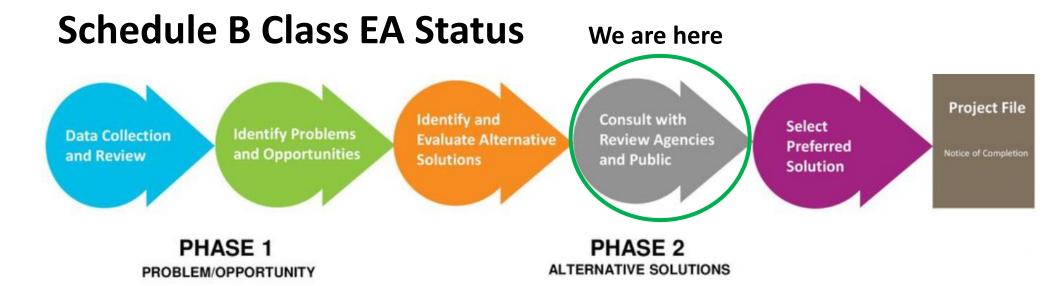
Construction Cost

Engineer's estimate available from City staff

- NEW watermain loop to complete the loop
 - from 6th Street East
 - to Superior Street
 - length: 420 metres
- Undertake a Schedule B Class EA
 - new alignment
 - to be located on non-City owned property



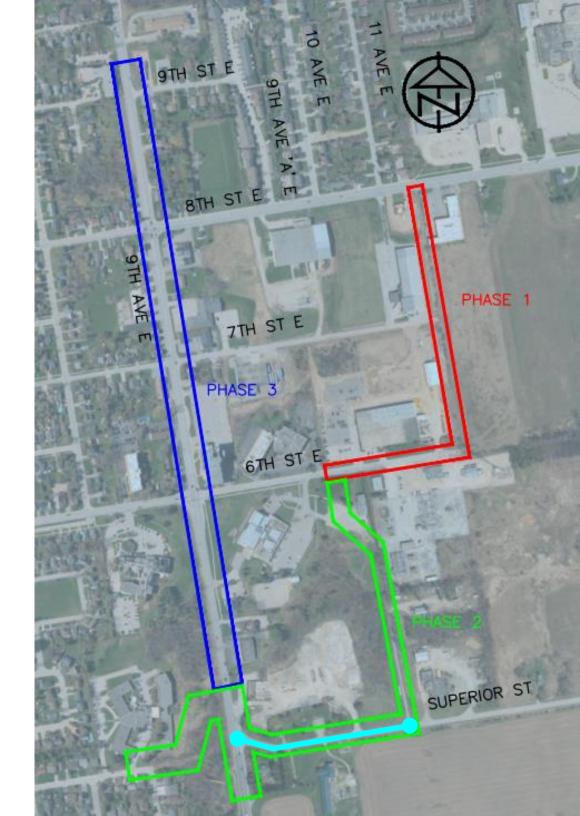




- Background info collected
 - topographic survey
 - geotechnical investigation
 - Environmental Impact Study
- Reviewing 5 potential alignments

- City in discussions with property owners for easements
 - 595 9th Avenue East
 - 1010 Superior Street

- REPLACE and UPSIZE watermain on Superior Street
 - from dead end
 - to 9th Avenue East
 - length: 280 metres



- ABANDON watermain on private property
 - 143006 Superior Street
- NEW connection
 - to 9th Avenue East



- REPLACE and UPSIZE watermain
 - from 9th Avenue East
 - to 8th Avenue 'B'
 East/4th Street East
 - length: 160 metres





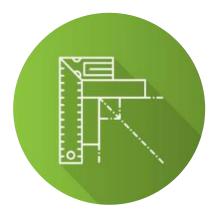
Schedule

Public Consultation



Summer 2023

Engineering Design



Fall 2023

Tender Period



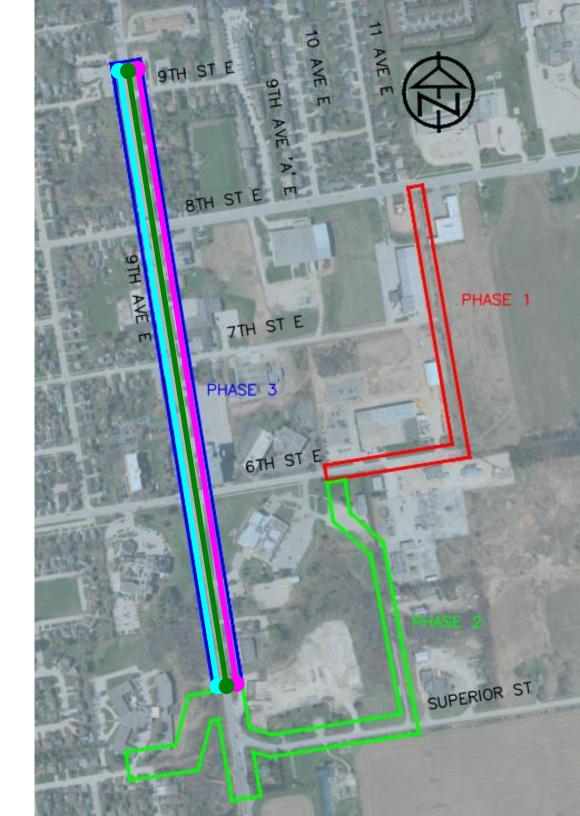
Winter 2024

Construction Period

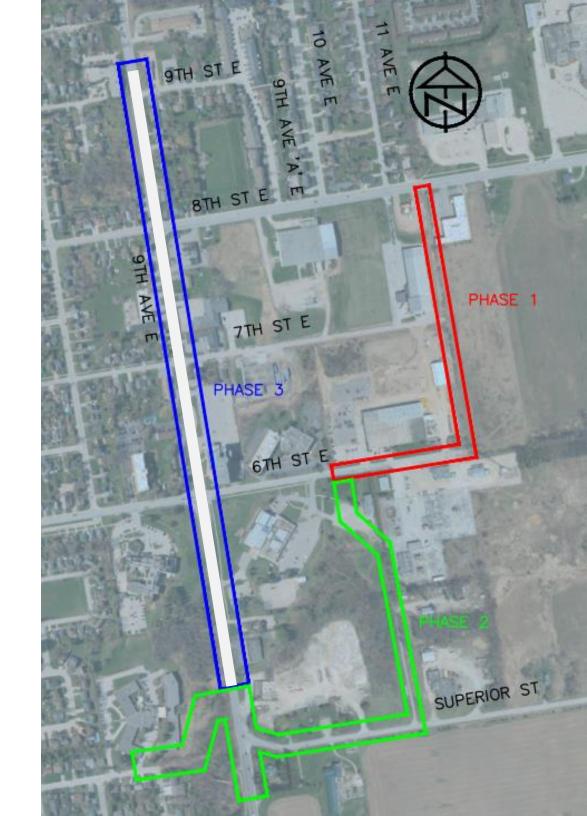


Summer 2024

- REPLACE distribution watermain
- REPLACE or RELINE sanitary sewer (localized areas only)
- REPLACE all water and sanitary services
- REPLACE storm sewer



- REPLACE road asphalt
- REPLACE guiderail
- REPLACE sidewalk (localized areas only)





Schedule



Note: Tender and construction periods subject to MTO Connecting Link funding



QUESTIONS

Appendix I: Public Information Centre Presentation







9TH AVENUE EAST LOOPING WATERMAIN

SCHEDULE B CLASS EA - PUBLIC INFORMATION CENTRE





AGENDA

- Project Contacts
- Study Area
- Class EA Overview
- Problem/Opportunity Statement
- Class EA Schedules
- Background Studies/Investigations
- Alternative Solutions
- Implementation Schedule
- Questions

Project Contacts







Chris Webb, P.Eng.

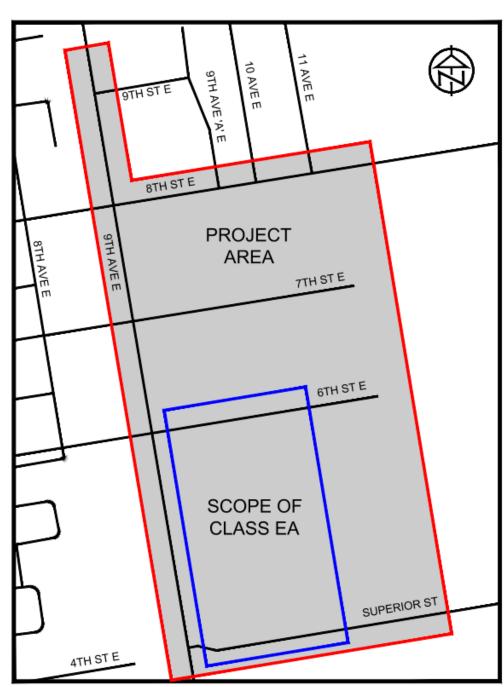
Mgr of Engineering Services
City of Owen Sound
(519) 376-1440 ext. 3300
cwebb@owensound.ca

Mark Figueroa, P.Eng.

Project Manager
Tatham Engineering Limited
(705) 444-2565 ext. 2142
mfigueroa@tathameng.com

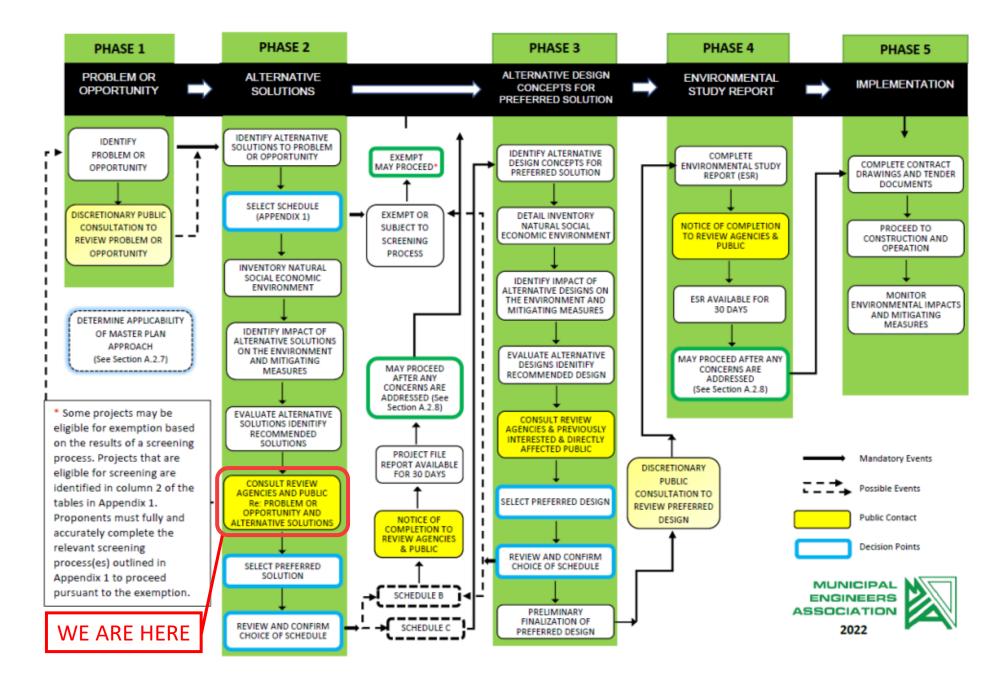
Study Area





Class EA Overview

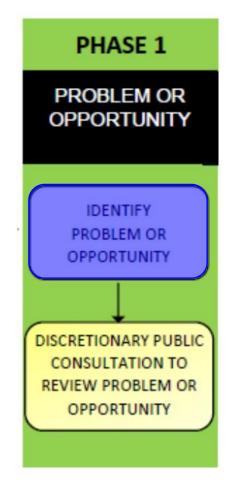




Problem/Opportunity Statement



"That existing infrastructure, road and sidewalk needs and deficiencies within the subject length of 9th Avenue East (100 metres south of Superior Street to 100 metres north of 9th Street East) be addressed in an environmentally sound manner, in consideration of City standards and policies, infrastructure requirements and active transportation opportunities, with the objective of providing safe and reliable service to the people of Owen Sound."



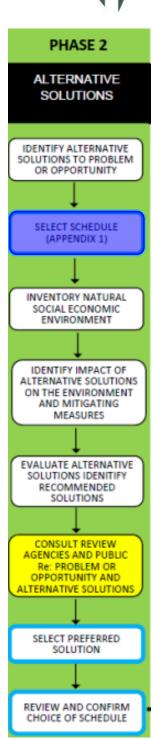


Exempt Activities (formerly Schedule A/A+)

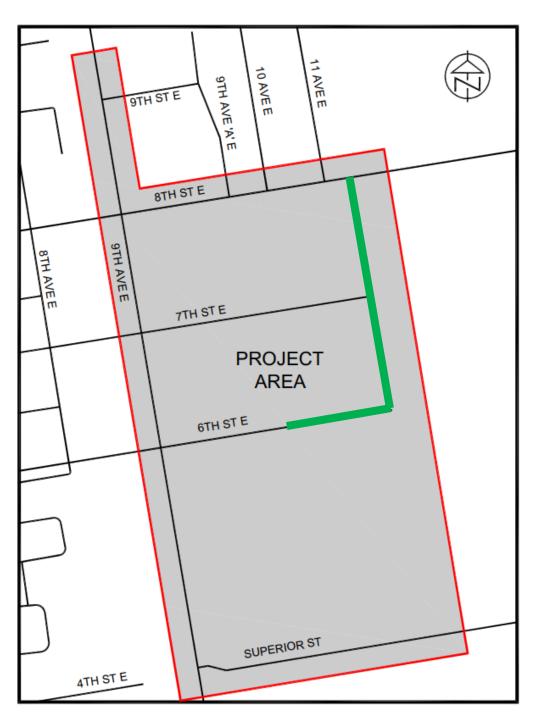
- Watermain and sewer replacements or extensions within an existing City owned road allowance or utility corridor
- Reconstruction of an existing road where number of lanes does not increase
- Sidewalk replacements or extensions
- Guiderail installation

Schedule B Activities

 Watermain and sewer replacements or extensions not located within an existing City owned road allowance or utility corridor

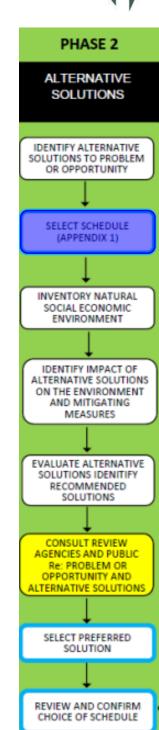




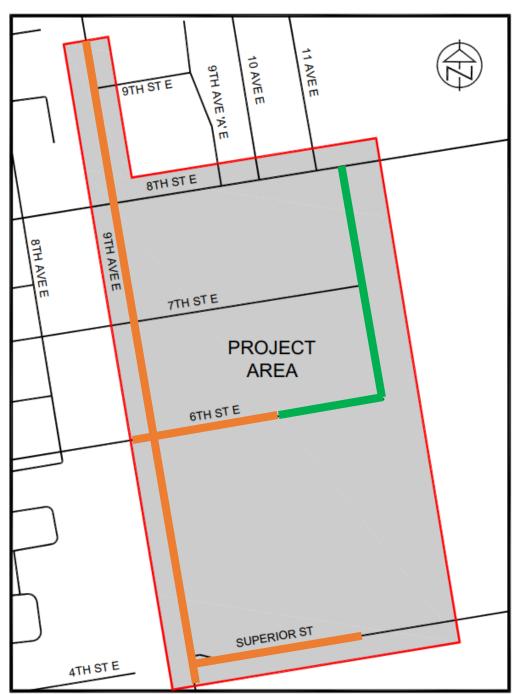


Previously complete
"Exempt" activities
(2023)

 Phase 1 looping watermain in utility corridor & 6th Street East



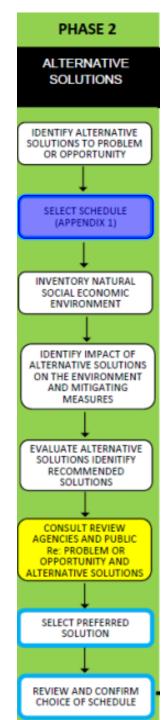




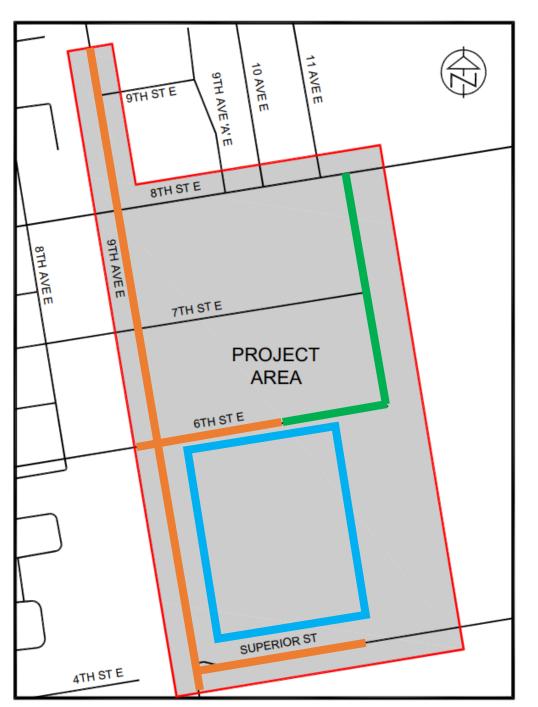
Previously complete
"Exempt" activities
(2023)

Future "Exempt"
activities
(Timeline TBD)

- Watermain replacement
- Storm sewer replacement on 9th Avenue East
- Localized sanitary sewer replacements
- Road reconstruction
- Localized sidewalk extensions and improvements
- Guiderail replacement





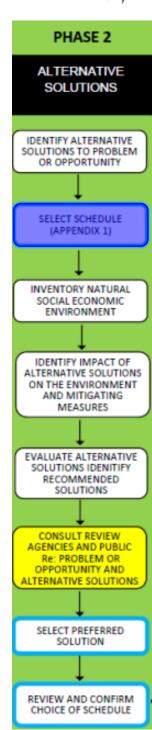


Previously complete
"Exempt" activities
(2023)

Future "Exempt"
activities
(Timeline TBD)

Future Schedule B activities (2024)

- Complete watermain loop from Superior Street to 6th Street East
- No road allowances or City owned utility corridors available



Background Studies/Investigations



Topographic Survey

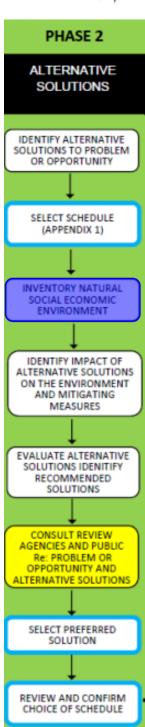
- Collect location and elevation of all surface features
- Forms basis for planning and design

Geotechnical Investigation

- Determine subsurface conditions (soil types, presence/depth of bedrock)
- Collect and analyze soil samples for contaminants and identify options for reuse of excess soil generated during construction
- Provides specifications for road and pipe construction

Hydrogeological Study

- Determine groundwater table elevation
- Identify dewatering requirements during construction
- Forms basis for required dewatering permits from MECP

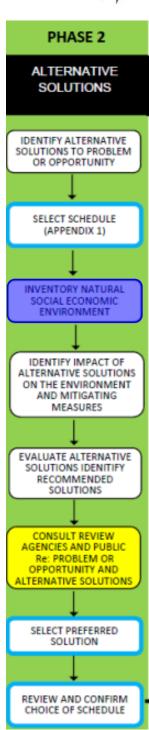


Background Studies/Investigations



Environmental Impact Study

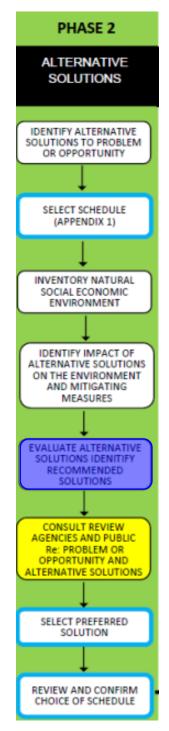
- Collected and reviewed background records from:
 - Grey County
 - Ministry of Natural Resources and Forestry
 - Ministry of the Environment, Conservation and Parks records
- Conducted field surveys:
 - 2 vascular plant inventories (spring and summer 2022)
 - 2 dawn breeding bird surveys
- Completed a Species at Risk habitat assessment through desktop reviews and fieldwork
- Assessed the potential direct and indirect impacts of the project on Natural Heritage Features and Functions in the study area



Alternative 0 – Do Nothing

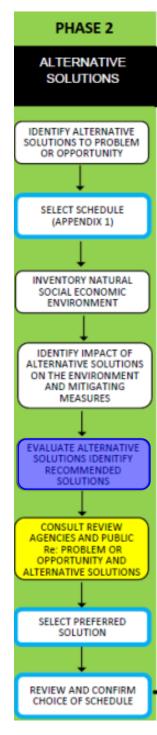


Criteria	Comments			
Technical (Water Operations)	- Operational needs not addressed			
Social Environment	 No easements required Watermain break results in detrimental impacts to commercial and institutional properties 			
Natural Environment	- No adverse impacts			
Heritage Archaeological Cultural Impacts	- No adverse impacts	5		
Cost	No capital costMaintenance costs remain (flushing, fixing breaks)			
	TOTAL:	13		



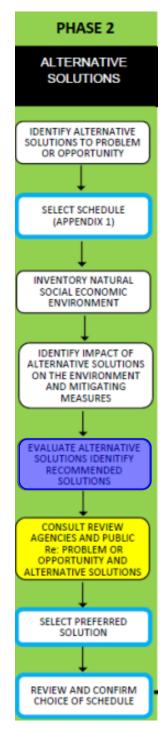






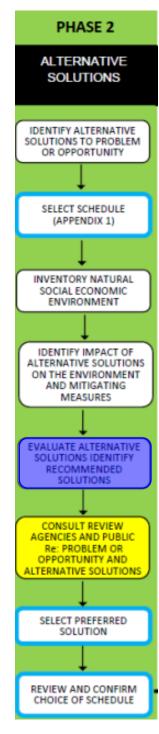


Criteria	Comments			
Technical (Water Operations)	Operational needs addressedRelatively straight alignment			
Social Environment	 New easements required on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 			
Natural Environment	- Fragments woodland in south half- Encroaches on potential SAR bat habitat			
Heritage Archaeological Cultural Impacts	No adverse impactsPreviously disturbed area in north half			
Cost	Lowest capital cost (shortest length)Reduces maintenance costs (flushing, fixing breaks)			
	TOTAL:	19		



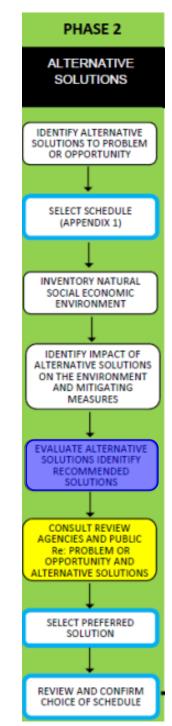






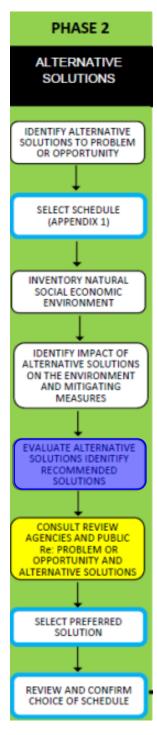


Criteria	Comments			
Technical (Water Operations)	Operational needs addressedRelatively straight alignment			
Social Environment	 New easement required on 1 property Widen existing easement on 1 property Significantly reduces impacts of watermain breaks (less customers affected) 			
Natural Environment	- Minimal impacts (limited tree removals)			
Heritage Archaeological Cultural Impacts	No adverse impactsAll areas previously disturbed			
Cost	 Lowest capital cost (shortest length) Reduces maintenance costs (flushing, fixing breaks) 			
	TOTAL:	23		



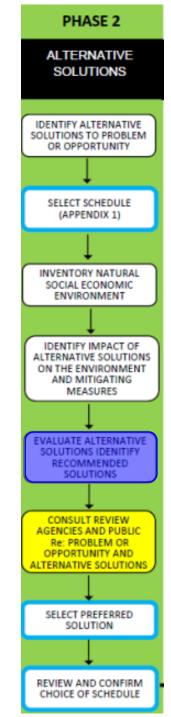






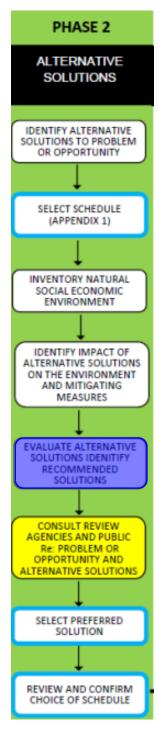


Criteria	Comments				
Technical (Water Operations)	Operational needs addressedStraight alignment				
Social Environment	 Widen existing easements on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 				
Natural Environment	- Minimal impacts (limited tree removals)	4			
Heritage Archaeological Cultural Impacts	No adverse impactsAll areas previously disturbed				
Cost	- Lowest watermain capital cost (shortest length) but must relocate building on Grey Cost County property - Reduces maintenance costs (flushing, fixing breaks)				
	TOTAL:	19			



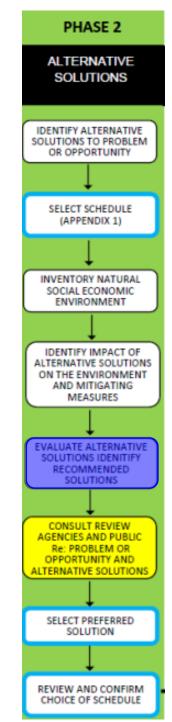






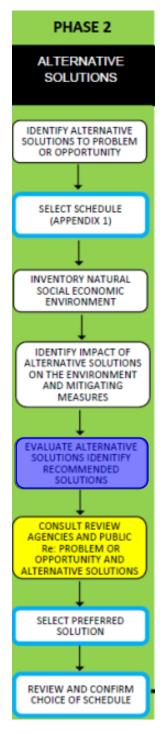


Criteria	Comments				
Technical (Water Operations)	Operational needs addressedSeveral bends in alignment, longer length				
Social Environment	 Widen existing easements on 2 properties New easements required on 2 properties Significantly reduces impacts of watermain breaks (less customers affected) 				
Natural Environment	- Limited tree removals- Will encroach into wetlands				
Heritage Archaeological Cultural Impacts	No adverse impactsAll areas previously disturbed				
- Largest watermain capital cost (longest length) - Reduces maintenance costs (flushing, fixing breaks)		1			
	TOTAL:	15			



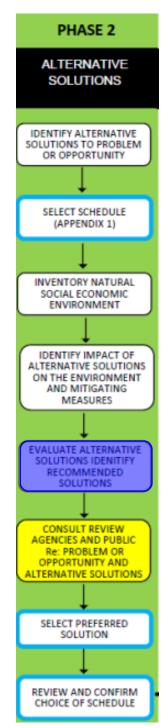








Criteria	Comments				
Technical (Water Operations)	Operational needs addressedSeveral bends in alignment, longer length				
Social Environment	 New easements required on 3 properties Hydro One won't allow infrastructure or easements through high voltage area Significantly reduces impacts of watermain breaks (less customers affected) 				
Natural Environment	Limited tree removalsWill encroach into wetlands				
Heritage Archaeological Cultural Impacts	No adverse impactsAll areas previously disturbed	5			
- Largest watermain capital cost (longest length) - Reduces maintenance costs (flushing, fixing breaks)		1			
	TOTAL:	12			

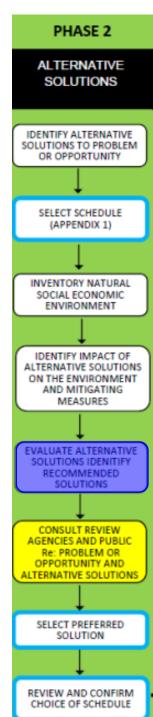


Recommended Alternative



Criteria	Do Nothing	1	2	3	4	5
Technical (Water Operations)	0	5	5	5	4	4
Social Environment	1	3	4	4	3	0
Natural Environment	5	1	4	4	2	2
Heritage Archaeological Cultural Impacts	5	5	5	5	5	5
Cost	2	5	5	1	1	1
Total Score	13	19	23	19	15	12

RECOMMENDED ALTERNATIVE



Implementation Schedule



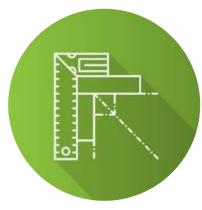
Public Consultation



Fall 2023

Legal Survey &

Engineering Design



Winter/Spring 2024

Tender Period



Spring/Summer 2024

Construction Period



Summer/Fall 2024



QUESTIONS